## Low-Cost Improvements to Express-Highway Bottleneck Locations



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The preparation of this document was supported by the Federal Highway Administration through MPO 3C PL contract \#95411.
MPO 3C PL contract \#101725
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Planning Organization. The MPO is composed of state and regional agencies and authorities, and local governments.

January 2018


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## Abstract

The purpose of the Low-Cost Improvements to Express-Highway Bottleneck Locations study is to identify low-cost improvements that will help reduce congestion at freeway bottleneck locations in the Boston Metropolitan Planning Organization (MPO) region. Bottlenecks in the freeway network can occur where geometric elements such as ramps or lane drops restrict traffic flow, and are a major contributor to recurring congestion. This study was undertaken in cooperation with the Massachusetts Department of Transportation (MassDOT) Highway Division and the Federal Highway Administration (FHWA) Massachusetts Division and is part of federal fiscal year (FFY) 2017.

Candidate locations were selected based on input from the MassDOT Highway Division as well as Congestion Management Process (CMP) data. The screening process yielded four locations that had the potential to respond to low-cost improvement measures. These locations included:

- Interstate-95 northbound between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) in Lexington
- Interstate-93 southbound between Exit 37C (Commerce Way) and Exit 37B (I-95) in Woburn and Reading
- Route 24 northbound between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton
- Route 24 southbound between Exit 21 (I-93) and Exit 20 (Route 139) in Randolph, Canton, and Stoughton

All locations regularly experience poor level of service (LOS) as a result of one or more freeway bottlenecks during peak travel periods.

The MPO staff developed one or more low-cost improvement proposals to address each bottleneck. If implemented, the modifications would result in capacity and safety improvements on these four high-volume facilities. Some recommendations of three previous low-cost bottleneck studies have already been implemented with positive results.

This report summarizes the analyses and recommendations from the study. The report is divided into multiple chapters, with four chapters covering each study location. Each location chapter summarizes existing conditions, proposes various low-cost measures to address the bottlenecks, and evaluates the efficacy of the proposed alternatives using methodology from the Highway Capacity Manual (HCM). The report concludes with a summary of the recommendations, followed by figures that illustrate features of the proposed improvements. The report also includes technical appendices that cite the methods used and the data applied.

## TABLE OF CONTENTS

PAGE
Abstract ..... 3
Chapter 1—Introduction ..... 11
1.1 Introduction ..... 11
1.2 Background ..... 11
1.3 Purpose of Study ..... 12
Chapter 2—Selection of Study Locations ..... 13
2.1 Screening Criteria ..... 14
2.2 Study Locations ..... 14
Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) in Lexington ..... 15
Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95) in Woburn and Reading ..... 15
Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton ..... 15
Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139) in Randolph, Canton, and Stoughton ..... 16
2.3 Rationale for Not Selecting Location 9 for Study ..... 16
Chapter 3-Data Collection ..... 17
3.1 Traffic Volume Data ..... 17
3.2 Classification Data ..... 17
3.3 Crash Data ..... 17
3.4 Speed Data ..... 17
3.4 Freeway Components ..... 17
3.4.1 Basic Freeway Segment ..... 17
3.4.2 Entrance Ramp. ..... 18
3.4.3 Exit Ramp ..... 18
3.4.4 Weaving Segment ..... 18
3.4.5 Major Merge and Diverge Areas. ..... 18
3.5 Level-of-service Criteria for Analyses ..... 18
Chapter 4—Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) in Lexington ..... 20
4.1 Existing Freeway Characteristics ..... 20
4.1.1 Basic Freeway Section ..... 20
4.1.2 Entrance Ramp. ..... 20
4.1.3 Exit Ramp ..... 21
4.2 Problems ..... 21
4.3 Causes ..... 21
4.3.1 High Volume of Traffic ..... 21
4.3.2 Short Acceleration Lane ..... 22
4.4 Impacts ..... 22
4.4.1 Crashes ..... 22
4.4.2 Travel Speed ..... 23
4.4.3 Level of Service ..... 24
4.5 Improvement Alternatives ..... 25
4.5.1 Alternative 1: Lengthen the Acceleration Lane at the On-Ramp from Route 2 ..... 25
4.5.2 Alternative 2: Create an Auxiliary Lane for Merging and Diverging Traffic ..... 26
4.5.3 Alternative 3: Signage Improvements for Exit 30 ..... 27
4.6 Effectiveness and Cost of the Improvements ..... 27
4.6.1 Effectiveness and Cost of Alternative 1 ..... 28
4.6.2 Effectiveness and Cost of Alternative 2 ..... 29
4.6.3 Effectiveness and Cost of Alternative 3 ..... 29
4.7 Recommendations ..... 30
Chapter 5—Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95) in Woburn and Reading ..... 31
5.1 Existing Freeway Characteristics ..... 31
5.1.1 Basic Freeway Section ..... 31
5.1.2 Entrance Ramps ..... 31
5.1.3 Exit Ramps ..... 32
5.2 Problems ..... 32
5.3 Causes ..... 32
5.3.1 High Volume of Traffic ..... 33
5.3.2 Insufficient Queueing Space ..... 33
5.4 Impacts ..... 33
5.4.1 Crashes ..... 33
5.4.2 Travel Speed ..... 35
5.4.3 Level of Service ..... 35
5.5 Improvement Alternatives ..... 37
5.5.1 Alternative 1: Create an Auxiliary Lane for Merging and Diverging Traffic at Exit 37B ..... 37
5.5.2 Alternative 2: Lengthen the Acceleration Lane at the Merge from Commerce Way ..... 38
5.5.3 Alternative 3: Use a Two-Lane Ramp at Exit 37B. ..... 38
5.6 Effectiveness and Cost of the Improvements ..... 39
5.6.1 Effectiveness and Cost of Alternative 1 ..... 40
5.6.2 Effectiveness and Cost of Alternative 2 ..... 41
5.6.3 Effectiveness and Cost of Alternative 3. ..... 41
5.7 Long-Term Plan for I-93/I-95 Interchange ..... 41
5.8 Recommendations ..... 42
Chapter 6—Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton ..... 43
6.1 Existing Freeway Characteristics ..... 43
6.1.1 Basic Freeway Section ..... 43
6.1.2 Major Diverge Area ..... 43
6.1.3 Merge Areas ..... 44
6.2 Problems ..... 44
6.3 Causes ..... 44
6.3.1 High Volume of Traffic ..... 44
6.3.2 Short Widening Distance at Major Diverge ..... 45
6.3.3 Merge to Single Lane on I-93 Southbound Ramp. ..... 45
6.3.4 Geometry at I-93 Northbound Merge ..... 45
6.4 Impacts ..... 46
6.4.1 Crashes ..... 46
6.4.2 Travel Speed ..... 47
6.4.3 Level of Service ..... 48
6.5 Improvement Alternatives ..... 49
6.5.1 Alternative 1: Widen Route 24 Northbound to Four Lanes between I-93 and Horse Bridge ..... 50
6.5.2 Alternative 2: Widen Route 24 Northbound to Four Lanes between I-93 and Canton Street ..... 50
6.5.3 Alternative 3: Remove the Merge on the Ramp to I-93 Southbound ..... 51
6.6 Effectiveness and Cost of the Improvements ..... 52
6.6.1 Effectiveness and Cost of Alternative 1 ..... 52
6.6.2 Effectiveness and Cost of Alternative 2 ..... 53
6.6.3 Effectiveness and Cost of Alternative 3 ..... 53
6.7 Recommendations ..... 54
Chapter 7—Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139) in Randolph, Canton, and Stoughton. ..... 55
7.1 Existing Freeway Characteristics ..... 55
7.1.1 Major Diverge Areas ..... 55
7.1.2 Major Merge Area ..... 55
7.1.3 Basic Freeway Section ..... 56
7.2 Problems ..... 56
7.3 Causes ..... 56
7.3.1 High Volume of Traffic ..... 56
7.3.2 Geometry at the Major Merge. ..... 56
7.4 Impacts ..... 57
7.4.1 Crashes ..... 57
7.4.2 Travel Speed ..... 58
7.4.3 Level of Service ..... 59
7.5 Improvement Alternative ..... 60
7.5.1 Alternative 1: Lengthen the Merge Distance at the Ramp Junction ..... 60
7.6 Effectiveness and Cost of the Improvement ..... 60
7.6.1 Effectiveness and Cost of Alternative 1 ..... 61
7.7 Recommendations ..... 61
Chapter 8-Conclusion and Next Steps ..... 62
TABLES AND FIGURES PAGE
TABLE 1. Inventory of Express-Highway Bottleneck Locations for Screening ..... 13
TABLE 2. LOS Criteria for Basic Freeway, Ramp Merge/Diverge, and Weaving Segments ..... 19
TABLE 3. Crash Summary (2010-14): Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) ..... 22
TABLE 4. LOS Analysis-Existing Conditions: Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) ..... 24
TABLE 5. LOS Analysis-Improvement Alternatives: Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) ..... 28
TABLE 6. Crash Summary (2010-14): Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95) ..... 34
TABLE 7. LOS Analysis-Existing Conditions: Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95) ..... 36
TABLE 8. LOS Analysis-Improvement Alternatives: Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95) ..... 39
TABLE 9. Crash Summary (2010-14): Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93) ..... 46
TABLE 10. LOS Analysis-Existing Conditions: Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93) ..... 49
TABLE 11. LOS Analysis-Improvement Alternatives: Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93) ..... 52
TABLE 12. Crash Summary (2010-14): Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139) ..... 57
TABLE 13. LOS Analysis-Existing Conditions: Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139) ..... 59
TABLE 14. LOS Analysis-Improvement Alternatives: Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139) ..... 61
FIGURE 1. Regional Map of Study Areas ..... 63
FIGURE 2. Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza): Peak Period Traffic Volumes ..... 64
FIGURE 3. Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza): Location and Number of Crashes ..... 65
FIGURE 4. Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza): Congestion Scan ..... 66
FIGURE 5. Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza): Alternative 1-Lengthen Acceleration Lane at Exit 29 ..... 67
FIGURE 6. Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza): Alternative 2-Create an Auxiliary Lane ..... 68
FIGURE 7. Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95): Peak Period Traffic Volumes ..... 69
FIGURE 8. Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95): Location and Number of Crashes ..... 70
FIGURE 9. Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95): Congestion Scan ..... 71
FIGURE 10. Location 2: I-95 Southbound Segment between Exit 38 (Route 28) and Lowell MBTA Line: Congestion Scan ..... 72
FIGURE 11. Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95): Alternative 1-Create an Auxiliary Lane on I-93 Southbound ..... 73
FIGURE 12. Location 2: I-95 Southbound Segment between Exit 38 (Route 28) and Lowell MBTA Line: Alternative 2-Lengthen the Acceleration Lane at I-95 Southbound Exit 36 ..... 74
FIGURE 13. Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95): Alternative 3-Two-Lane Ramp at Exit 37B ..... 75
FIGURE 14. Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93): Peak Period Traffic Volumes ..... 76
FIGURE 15. Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93): Location and Number of Crashes ..... 77
FIGURE 16. Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93): Congestion Scan ..... 78
FIGURE 17. Location 3: I-93 Northbound Segment between Exit 2 (Route 138) and Exit 5 (Route 28): Congestion Scan ..... 79
FIGURE 18. Location 3: I-93 Southbound Segment between Exit 5 (Route 28) and Exit 2 (Route 138): Congestion Scan ..... 80
FIGURE 19. Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93): Alternative 1-Widen to Four Lanes After Horse Bridge ..... 81
FIGURE 20. Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93): Alternative 2-Widen to Four Lanes After Canton Street Bridge ..... 82
FIGURE 21. Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93): Alternative 3-Remove Merge in Ramp to I-93 Southbound83
FIGURE 22. Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139): Peak Period Traffic Volumes ..... 84
FIGURE 23. Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139): Location and Number of Crashes ..... 85
FIGURE 24. Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139): Congestion Scan ..... 86
FIGURE 25. Location 4: Route 24 Southbound Segment between Exit 21 (I-93)and Exit 20 (Route 139): Alternative 1-Lengthen Merge Distance at RampJunction87

APPENDIXES

Appendix A: Review Comments and Selection Process
Appendix B: ATR and Classification Data
Appendix C: Crash Tables
Appendix D: HCS Printouts

## Chapter 1-Introduction

### 1.1 INTRODUCTION

This report summarizes the results of the analyses and improvement alternatives considered in the federal fiscal year (FFY) 2017 Low-Cost Improvements to Express-Highway Bottleneck Locations study. The report opens with background information and describes the purpose of the study, followed by the selection of study locations, an assessment of the safety and operational problems, and a discussion of the potential improvement strategies. The final section presents study recommendations. The report concludes with technical appendices, which cite the study methods and describe how the data were applied, including detailed reports from the freeway merge and diverge analyses. If implemented, the report's recommendations are expected to result in improvements on the freeway facilities; they would improve traffic safety, make traffic operations more efficient, and reduce congestion at the bottlenecks.

### 1.2 BACKGROUND

According to the Federal Highway Administration (FHWA), "Much of recurring congestion is due to physical bottlenecks—potentially correctible points on the highway system where traffic flow is restricted. While many of the nation's bottlenecks can only be addressed through costly major construction projects, there is a significant opportunity for the application of operational and low-cost infrastructure solutions to bring about relief at these chokepoints." ${ }^{1}$ To be consistent with this guidance, the FHWA Massachusetts Division has recommended, as part of its comments on the Unified Planning Work Program process, that the Boston Region Metropolitan Planning Organization (MPO) identify the worst bottlenecks in the region that can be mitigated with low-cost countermeasures and develop recommendations for such countermeasures at these locations.

In general, recurring bottlenecks, the subject of this study, are influenced by the design or operation present at the point where the bottleneck begins (for example, merges, diverges, lane drops, traffic weaving, and abrupt changes in highway alignment). Previously, MPO staff analyzed several express-highway bottleneck locations in three consecutive studies, Low-Cost Improvements to Bottlenecks Phase I (FFY 2011), Phase II (FFY 2012), and Phase III (FFY 2015),

[^0]which were well received by the Massachusetts Department of Transportation (MassDOT) and the FHWA. ${ }^{2,3,4}$ Previous study locations included sections of Interstate 95 in Burlington, Lexington, and Weston; sections of Interstate 93 in Woburn; and sections of Route 3 in Braintree.

Many of the recommendations from those studies have been implemented, and the FHWA has interviewed MPO staff about these successful implementations, including:

- Restriping lanes to serve traffic demand better on I-95 northbound at Interchange 24 in Weston
- Restriping lanes to serve traffic demand better on I-95 southbound at Interchange 24 in Weston
- Providing two-lane exit for traffic exiting I-95 northbound to Route 3 northbound and the Middlesex Turnpike at Interchange 32 in Lexington and Burlington
- Providing two-lane exit for traffic exiting I-95 southbound to Route 3 northbound and the Middlesex Turnpike at Interchange 32 in Burlington


### 1.3 PURPOSE OF STUDY

The purpose of this study is twofold:

- Identify two or more bottleneck segments or points where low-cost mitigation improvements seem applicable
- Recommend low-cost mitigation improvements based on analysis of geometric design, traffic volumes and other data, and projected service performance associated with the improvements at each location

The MPO has been conducting these studies in the Boston region to identify lowcost methods to reduce congestion, increase safety, and improve traffic operations. In the current study, the MPO staff will rely on their technical expertise regarding the nature of bottlenecks and will seek input from MassDOT Highway Division staff, who are familiar with the region's express-highway system operations, to develop and evaluate a comprehensive list of potential improvements at the bottleneck locations.

[^1]
## Chapter 2-Selection of Study Locations

The selection of study locations included the inventorying and screening of candidate locations. ${ }^{5}$ MPO staff developed an initial list of candidate locations in the MPO region based on the following parameters:

- Consultations with the MassDOT Highway Division
- Review of Congestion Management Process (CMP) monitoring data and recent MPO and other planning studies
- Staff knowledge of bottleneck locations in the Boston MPO region

The inventory process yielded nine bottleneck locations in the Boston Region MPO area for screening, which are presented in Table 1.

TABLE 1.
Inventory of Express-Highway Bottleneck Locations for Screening


* = locations selected for analysis

Source: Central Transportation Planning Staff.

[^2]
### 2.1 SCREENING CRITERIA

MPO staff used the following three criteria to screen the bottleneck locations:

1. Does the location qualify as a bottleneck? A repetitive, long-traffic queue upstream trailing free-flowing traffic downstream usually characterizes the location as a bottleneck. In other words, the location experiences routine and predictable congestion because traffic volume exceeds the available capacity at that location.
2. Is a physical design constraint or operational conflict inherent in the location the cause of the bottleneck? Examples of these include the following constraints or conflicts:
a. Lane drop: one or more travel lanes end, requiring traffic to merge
b. Weaving area: drivers must merge across one or more lanes to access an entry or exit ramp
c. Merge area: on-ramp traffic merges with mainline traffic to enter the freeway
d. Major interchanges: high-volume traffic is directed from one freeway to another
3. Can the bottleneck be fixed with low-cost operational and geometric improvements? These exclude costly long-term solutions such as expansion or widening of the roadway. Examples of low-cost operational and geometric improvements include the following:
a. Using a short section of shoulder as an additional travel lane or for lengthening an acceleration or deceleration lane
b. Restriping merge and diverge areas to better serve traffic demand
c. Providing all-purpose reversible lanes
d. Changing or adding signs and striping

Each location must meet these criteria for it to be selected for study. In addition, the number of locations selected for study is also dependent on funding allocated for the study.

### 2.2 STUDY LOCATIONS

Based on the screening criteria and consultations with MassDOT Highway Division officials, MPO staff selected locations 1, 2, 3, and 4 for study. Figure 1 shows the study locations, which are described below. Although locations 5, 6, 7, and 8 met the screening criteria, they were not selected for study in this round of bottleneck study because of funding-these locations would be considered for the next round of bottleneck study. Appendix A contains comments about the study from the MassDOT Highway Division and a memorandum to the MPO that describes the selection process in detail. (All figures are included at the end of the report.)

Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) in Lexington
This bottleneck is located on I-95 northbound between the Route 2 and Route 2A interchanges, and is present during AM and PM peak periods. The I-95 northbound mainline can carry up to 7,600 vehicles per hour, while up to 1,500 vehicles per hour merge from Route 2 westbound and up to 1,300 exit to Route 2A and the service plaza. The merging and diverging activities of these vehicles slow down traffic on the freeway upstream of the Route 2A interchange, making it difficult to enter the freeway from Route 2. The existing conditions analyses, problem identification, and the improvements proposed to this bottleneck location are described in Chapter 4.

## Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (l-95) in Woburn and Reading

This bottleneck is located on I-93 southbound upstream from the point where traffic begins to diverge onto I-95 southbound. During the AM peak period, traffic going to I-95 southbound backs up on the ramp and spills onto the I-93 mainline, thus impacting flow on the right most low-speed southbound lane. As a result, motorists attempt to get into the breakdown lane as soon as possible to stay clear of the low-speed lane. But usually vehicles are still queuing on the lowspeed lane, compounding the problems. The other three southbound lanes are almost in free flow conditions (that is, uncongested conditions with drivers traveling at posted speeds) during this period. In the segment, the four I-93 southbound lanes carry up to 7,500 vehicles per hour, of which approximately 2,000 vehicles exit to I-95 southbound. The existing conditions analyses, problem identification, and the improvements proposed to this bottleneck location are described in Chapter 5.

## Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton

This bottleneck is located on Route 24 northbound at the point where traffic diverges onto I-93 northbound and southbound. Bottleneck conditions emerge primarily during the AM peak period and extend south from I-93 in Randolph as far as Route 27 in Brockton, or approximately seven miles. During this period, Route 24 northbound carries approximately 4,600 vehicles per hour, with volumes of 2,300 vehicles heading northbound on I-93 and approximately 2,300 vehicles heading to l-93 southbound. These volumes are low because of the bottleneck, and they do not reflect actual traffic demand or traffic capacity of Route 24 mainline or connector ramps. The merging activity of these vehicles on I-93 slows down traffic on the Route 24 connector ramps and causes traffic to back up on Route 24. The existing conditions analyses, problem identification,
and the improvements proposed to this bottleneck location are described in Chapter 6.

## Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139) in Randolph, Canton, and Stoughton

This bottleneck is located on Route 24 southbound at the point where traffic from the I-93 connector ramps merges onto Route 24 southbound. Bottleneck conditions emerge primarily during the PM peak period. During this period, Route 24 southbound carries approximately 5,300 vehicles per hour, of which approximately 2,700 vehicles enter from I-93 northbound and another 2,600 from $\mathrm{I}-93$ southbound. The merging activity of these vehicles creates a bottleneck that causes a one-mile-long traffic queue to extend from the Canton Street Bridge under Route 24 onto the I-93 northbound and southbound lanes. The existing conditions analyses, problem identification, and the improvements proposed to this bottleneck location are described in Chapter 7.

### 2.3 RATIONALE FOR NOT SELECTING LOCATION 9 FOR STUDY

MPO staff did not select Location 9: I-95 Northbound between Exit 37 (I-93) and Exit 38 (Route 28) in Reading for the study. This section of highway frequently is congested because of a lane drop, intensive weaving, and merging and diverging activities, which slow down mainline traffic, especially during the PM peak period. During that time, the I-95 northbound mainline carries approximately 6,000 vehicles per hour, and the Exit 37 off- and on-ramps carry approximately 3,000 and 2,600 vehicles per hour, respectively. Adding an auxiliary lane northbound on I-95 would provide more room for the merging and diverging activities and reduce disturbance to mainline traffic. Staff did not select this location because the weave problem at Exit 37 could not be corrected in a low-cost manner and an auxiliary lane would need to be extended for a long distance (three to four interchanges downstream) to reduce congestion and the queue, which could be expensive.

## Chapter 3-Data Collection

### 3.1 TRAFFIC VOLUME DATA

The MassDOT Highway Division's Traffic Data Collection Program conducted automatic traffic recorder (ATR) counts for the ramps and freeways at the locations selected for study. The ATR counts traffic continuously for at least 48 hours. These counts are used to determine the average weekday daily traffic of a highway. The traffic volume data are included in Appendix B.

### 3.2 CLASSIFICATION DATA

Although the ATR data that MassDOT collected for this study did not include vehicle classification, other count methods can capture this information. MPO staff used the MassDOT traffic count database to access classification data collected during previous traffic counts inside the study areas. The heavy vehicle percentages present in these counts were used to estimate truck traffic for the freeway analyses. All the counts used in this way were taken between 2014 and 2017. They are included in Appendix B.

### 3.3 CRASH DATA

MPO staff used crash data from January 2010 through December 2014 from the MassDOT's Registry of Motor Vehicles database to evaluate safety for motorists. Crash data are included in Appendix C.

### 3.4 SPEED DATA

MPO staff used speed data from spring 2015 and fall 2015 for average weekday from the MPO's CMP. The CMP maintains average speed data on expresshighway systems in the MPO region with use of the INRIX historical traffic speed data archive.

### 3.4 FREEWAY COMPONENTS

### 3.4.1 Basic Freeway Segment

Basic freeway segments are outside of the influence area of ramps or weaving areas of the freeway. The flow in such segments occurs more smoothly than segments with merging, diverging, or weaving. The exact point at where basic freeway segments begin or end-the area where the influence of merging, diverging, or weaving has dissipated-depends on local conditions, particularly the level of service (LOS) operating at the time. If traffic flow is light, the influence
may be negligible, whereas under congested conditions, queues may be extensive.

### 3.4.2 Entrance Ramp

An entrance ramp is a one-way roadway that allows traffic to enter a freeway from other crossing highways. Sufficient acceleration distance is needed to allow a vehicle to enter the freeway mainline safely and comfortably; drivers on the entrance ramp need to be able to see a sufficient distance upstream from the entrance to locate the gaps in the traffic stream within which to merge.

### 3.4.3 Exit Ramp

An exit ramp is a one-way roadway that allows traffic to exit from the freeway and provide access to other crossing highways. Sufficient deceleration distance is needed to allow a vehicle to leave the freeway mainline safely and comfortably.

### 3.4.4 Weaving Segment

Weaving segments are formed when a freeway merge is followed by a freeway diverge within one-half mile. This geometry creates an area of intense lane changing as the two streams of traffic travel in conflicting directions. Weaving length, or the distance between merge and diverge points, must be sufficient to allow drivers to make the required lane changes safely and comfortably.

### 3.4.5 Major Merge and Diverge Areas

A major merge occurs when two multilane freeway segments combine to form a single freeway segment with three or more lanes. Likewise, a major diverge occurs when a freeway segment with three or more lanes splits into two multilane basic freeway segments. While these locations can create turbulence in the traffic flow, they are less restrictive than freeway ramps because speed differences are smaller and lane changes are often unnecessary.

### 3.5 LEVEL-OF-SERVICE CRITERIA FOR ANALYSES

LOS is a quality measure describing operational conditions within a traffic stream, generally in terms of such service measures as speed and travel time, freedom to maneuver, traffic interruptions, and comfort and convenience. Factors influencing LOS are volume, lane width, lateral obstructions, traffic composition, grade, and speed. The Highway Capacity Manual (HCM) methodology demonstrates driving conditions on freeways in terms of LOS ratings from $A$
through F. ${ }^{6}$ The LOS criteria characterize freeway performance measures in terms of density (passenger cars per lane mile, [pc/lane mile]). Table 2 shows the LOS criteria for basic freeway and ramp merge/diverge and weaving segments.

TABLE 2.
LOS Criteria for Basic Freeway, Ramp Merge/Diverge, and Weaving Segments

|  | Basic Freeway Segment | Ramp Merge/Diverge and <br> Weaving Segments |
| :--- | :--- | :--- |
| LOS | Density (pc/lane mile) | Density (pc/lane mile) |
| A | $\leq 11$ | $\leq 10$ |
| B | $>11-18$ | $>10-20$ |
| C | $>18-26$ | $>20-28$ |
| D | $>26-35$ | $>28-35$ |
| E | $>35-45$ | $>35$ |
| F | $>45$, Demand exceeds | Demand exceeds capacity |
|  | capacity |  |

pc/lane mile = passenger cars per lane mile
Source: Highway Capacity Manual 2010.
LOS A represents the best operating conditions (unrestricted operations), while LOS F represents the worst operating conditions (queuing on the freeway and/or ramp). LOS A through LOS D represent acceptable operating conditions. LOS E represents operating conditions at capacity. LOS F represents failing conditions (demand exceeds capacity).

MPO staff conducted traffic operations analyses consistent with HCM methodologies. Using the data collected, MPO staff built traffic analysis networks for the AM and PM peak hours with the 2010 Highway Capacity Software (HCS) to assess the capacity and quality of traffic flow at the bottleneck area. Detailed reports generated by the HCS software are included in Appendix D. ${ }^{7}$

[^3]
# Chapter 4-Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) in Lexington 

Location 1 is a stretch of Interstate 95/Route 128 northbound in Lexington. Figure 1 shows the location of the bottleneck within the MPO region. The northbound on- and off-ramps connect to and from Route 2 (Concord Turnpike), Route 2A (Merrett Road), and a service plaza. The bottleneck conditions form primarily during the PM peak period, when high volumes of rush hour traffic heads northbound on I-95. This interchange and the roadways are under the jurisdiction of MassDOT Highway Division, and they are located in District 4.

### 4.1 EXISTING FREEWAY CHARACTERISTICS

Operations at this bottleneck are associated with the freeway components described below.

### 4.1.1 Basic Freeway Section

The basic freeway section of l-95 northbound has four 12 -foot travel lanes, a 10foot right shoulder, and a 10 - to 11 -foot left shoulder. This section carries approximately 7,500 vehicles per hour during both the AM and PM peak periods. ${ }^{8}$ The posted speed limit is 65 miles per hour (mph). Freeway exit signs are posted at one-mile and one-half-mile intervals to guide drivers to Routes 2 and 2A. As a result of recent resurfacing, neither side of I-95 northbound at this location is equipped with a rumble strip.

### 4.1.2 Entrance Ramp

The entrance ramp from Route 2 westbound to I-95 northbound is a one-lane, one-way roadway. It carries as many as 1,500 vehicles per hour during the AM peak period and 1,100 vehicles per hour during the PM peak period. The length of the acceleration lane for traffic entering the section from Route 2 westbound is approximately 500 feet long, ${ }^{9}$ and the posted speed limit on the entrance ramp is 25 mph . Based on highway design and entrance ramp curve design speeds, the length of the acceleration lane does not meet MassDOT's standards. The

[^4]MassDOT Highway Division's current Project Development and Design Guide specifies a minimum acceleration lane of 1,220 feet for a freeway facility with a design speed of 65 mph , an entrance ramp curve design speed of 25 mph , and a grade of two percent or less.

### 4.1.3 Exit Ramp

The exit ramp from I-95 northbound to Route 2A is a one-way, one-lane roadway that leads to a connector-distributor road approximately 4,000 feet long. Traffic bound for Route 2A westbound, eastbound, and the Lexington service plaza all use Exit 30. Combined, these three destinations produce flows of 1,300 vehicles per hour on the ramp during peak hours. The length of the deceleration lane is approximately 740 feet long, and the posted speed limit on the exit ramp is 30 mph. Based on highway design and exit ramp curve design speeds, the length of the deceleration lane meets MassDOT's standards. The MassDOT Highway Division's current Project Development and Design Guide specifies a minimum deceleration length of 440 feet for a freeway facility with a design speed of 65 mph , an exit ramp curve design speed of 35 mph , and a grade of two percent or less. The MassDOT design guide recommends using parallel type deceleration lanes instead of the taper type that is used on Exit 30, although in this case the presence of a nearby bridge (over Lincoln Street) might make a parallel design difficult.

### 4.2 PROBLEMS

The existing bottleneck creates intense interruption of traffic flow primarily during PM peak travel periods, experienced by virtually all drivers in the section. It reduces travel speeds on the freeway mainline to 35 mph or less during the PM peak period. In addition, the bottleneck causes many crashes in this area and results in poor operating LOS, especially at the diverge area connecting the exit ramp to Route 2A eastbound.

### 4.3 CAUSES

MPO staff identified two factors that contribute to form the bottleneck:

- A high volume of traffic during peak hours
- A short acceleration lane at the ramp from Route 2


### 4.3.1 High Volume of Traffic

Figure 2 shows the traffic flows during the AM and PM peak periods. The merging and diverging activities of vehicles using the ramps slow down traffic on the freeway upstream of the Route 2A interchange, creating a bottleneck and making it difficult to enter the freeway from Route 2.

Although ATR data show similar ramp and mainline volumes in the two peaks, vehicle speed data indicate that the worst congestion occurs during the PM peak (see Section 4.4.2). During this period of time, traffic slows considerably and queues extend for miles down I-95. This observation suggests that the actual demand on the facility is greater than the number of vehicles it is able to serve. True demand is nearly 8,800 vehicles per hour, which is the theoretical capacity of a four-lane freeway operating in uncongested conditions.

### 4.3.2 Short Acceleration Lane

A short acceleration lane for the high-volume traffic entering I-95 northbound from Route 2 westbound forces drivers to merge quickly and does not give them the distance needed to reach safe freeway speeds. The intense merging maneuvers slow down traffic, causing a bottleneck upstream from the merge location.

### 4.4 IMPACTS

### 4.4.1 Crashes

A summary of the crashes in this segment is presented in Table 3. There were 108 crashes in this area between 2010 and 2014 (Appendix C). Figure 3 shows the location of these crashes. The majority ( 98 crashes) occurred in the vicinity of the off-ramp at Exit 30.

TABLE 3.
Crash Summary (2010-14):
Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza)

|  | Number of Crashes |  |  |
| :--- | :---: | :---: | :---: |
| Crash Variable | At Merge | At Diverge | Total |
| Crash severity |  |  |  |
| Fatal injury | 0 | 0 | 0 |
| Nonfatal injury | 4 | 20 | 24 |
| Property damage only | 6 | 75 | 81 |
| Not reported/unknown | 0 | 3 | 3 |
| Manner of collision |  |  |  |
| Angle | 0 | 9 | 9 |
| Rear-end | 5 | 49 | 54 |
| Rear-to-rear | 0 | 2 | 2 |
| Sideswipe, same direction | 2 | 7 | 9 |
| Single-vehicle crash | 3 | 28 | 31 |
| Not reported/unknown | 0 | 3 | 3 |


| Road surface conditions |  |  |  |
| :--- | :---: | :---: | :---: |
| Dry | 8 | 68 | 76 |
| Wet | 2 | 6 | 8 |
| Snow | 0 | 24 | 24 |
| Ambient light conditions |  |  |  |
| Daylight | 5 | 58 | 63 |
| Dark: lighted roadway | 1 | 11 | 12 |
| Dark: nonlighted roadway | 4 | 22 | 26 |
| Dawn | 0 | 3 | 3 |
| Dusk | 0 | 4 | 4 |
| Weather conditions |  |  |  |
| Clear | 7 | 59 | 66 |
| Cloudy | 1 | 17 | 18 |
| Rain | 2 | 11 | 13 |
| Snow | 0 | 6 | 6 |
| Not reported/unknown | 0 | 5 | 5 |
| Travel period | 5 |  |  |
| Peak | 5 | 60 | 65 |
| Off-peak | 10 | 38 | 43 |
| Total crashes | 2 | 98 | 108 |
| Five-year average (rounded) |  | 20 |  |

Below is a summary of the crashes in this segment:

- 22 percent of the crashes resulted in injury
- 50 percent of the crashes were rear-end collisions, the largest share among collision types
- 60 percent of the crashes occurred during peak travel periods
- 42 percent of the crashes occurred outside daylight conditions
- 70 percent of the crashes occurred under dry roadway conditions


### 4.4.2 Travel Speed

Figure 4 is a congestion scan that shows the average travel speeds on I-95 northbound at the bottleneck location between Route 2 and Route 2A. The bottleneck reduces travel speeds less than 25 mph between 3:00 PM and 5:00 PM. Vehicle speeds this far below free-flow correlate with LOS F conditions on the freeway. Travel speed during the AM peak is less affected and remains more than 50 mph .

### 4.4.3 Level of Service

MPO staff conducted traffic operations analyses consistent with HCM methodologies. Using data from MassDOT, MPO staff built traffic analysis networks for the AM and PM peak hours with the HCS suite to assess the capacity and quality of traffic flow at the bottleneck area. ${ }^{10}$ Full HCS reports are included in Appendix D.

Table 4 presents the results of the LOS analyses for existing conditions at Location 1. The primary bottleneck is located at the merge from Route 2 westbound. Some simplifications were necessary to fit the HCS model more closely with observed conditions and are stated in the table notes.

TABLE 4.
LOS Analysis-Existing Conditions:
Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza)

| Location | Peak Period | Density (pc/lane mile) | $\begin{aligned} & \text { Speed } \\ & (\mathrm{mph})^{\text {a }} \end{aligned}$ | VIC <br> Ratio | LOS ${ }^{\text {b }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| HCM Analysis Type: Basic Freeway Segment |  |  |  |  |  |
| I-95 northbound between | AM | 32.9 | 59.1 | 0.84 | D |
| Exit 29 and Exit 30 | PM | 41.7 | 53.7 | 0.96 | E |
| HCM Analysis Type: Merge Area ${ }^{\text {d }}$ |  |  |  |  |  |
| Ramp from Route 2 | AM | 34.5 | 53.3 | 0.83 | D |
| westbound | PM | N/A ${ }^{\text {e }}$ | N/A | 1.05 | F |
| HCM Analysis Type: Diverge Area |  |  |  |  |  |
| Exit 30 to Route 2A and | AM | 33.4 | 51.3 | 0.83 | D |
| service plaza | PM | 38.8 | 51.1 | 0.95 | E |
| HCM Analysis Type: Weaving Segment ${ }^{t}$ |  |  |  |  |  |
| I-95 northbound between | AM | N/A | N/A | 1.10 | F |
| Exit 29 and Exit 30 | PM | 41.8 | 42.8 | 0.89 | E |

${ }^{\text {a }}$ Refers to ramp influence area speed for merge/diverge areas.
${ }^{\mathrm{b}}$ LOS A through LOS D represent acceptable operating conditions; LOS E represents operating conditions at capacity; and LOS F represents failing conditions (demand exceeds capacity).
${ }^{c}$ Estimated demand flow rate of 8,800 vph used for all PM existing condition analyses (see Section 4.3.1)
${ }^{\text {d }}$ In HCM merge and diverge analyses, acceleration and deceleration lanes are measured from the tip of the painted gore to the end of the taper. This may differ from the AASHTO length.
${ }^{e}$ HCM does not provide density and speed data for scenarios that result in LOS F.
${ }^{f}$ Uses a weaving segment of five lanes so limiting factor is weaving behavior and not mainline capacity. (HCM weaving analysis assumes a lane drop after the merge.) HCM = Highway Capacity Manual; LOS = level of service; mph = miles per hour; pc/lane mile = passenger cars per lane mile; V/C = volume-to-capacity; vph = vehicles per hour

[^5]Table 4 shows that most facilities operate at LOS D during the AM peak and LOS E during the PM peak. The two exceptions are the PM merge from Route 2 and the AM weaving segment analysis, both of which reach LOS F.

The high combined-ramp volume during the AM peak (2,600 entering and exiting vehicles per hour) also causes the weaving analysis to fail during this period. This means that the formulas in the HCM predict that not all vehicles using the ramps during the AM peak will be able to successfully merge within the available 1,720 feet. However, this does not fit with observed conditions. One possible explanation is that this and other bottlenecks along I-95 reduce speed on the northbound mainline below free-flow speed, giving vehicles more time to execute a lane change. Driver behavior may also be misrepresented in the formulas. At any rate, the fact that weaving fails during the AM peak period when congestion is not a big problem suggests that weaving analysis is not well suited to this bottleneck location.

### 4.5 IMPROVEMENT ALTERNATIVES

MPO staff developed the following improvements to address safety and operational issues at the bottleneck:

- Alternative 1: Lengthen the acceleration lane at the on-ramp from Route 2 westbound (Figure 5).
- Alternative 2: Create an auxiliary lane for merging and diverging traffic (Figure 6).
- Alternative 3: Add new signage at Exit 30 to help clarify the location of the three destinations served by this ramp.

The alternatives were analyzed using projected year 2030 traffic volumes. MPO staff estimated a five percent total background growth from 2017 to 2030.

### 4.5.1 Alternative 1: Lengthen the Acceleration Lane at the On-Ramp from Route 2

The existing acceleration lane is short; it does not meet MassDOT's standards and contributes to poor traffic operations. MPO staff recommends lengthening the acceleration lane from the Route 2 westbound on-ramp.

Figure 5 shows the following improvements recommended in Alternative 1:

- Extend the acceleration lane for the on-ramp from Route 2 westbound. The current ramp features a 500-foot full-width acceleration lane followed by a 540-foot taper. Alternative 1 would extend the full-width lane as far as permitted by the existing right-hand paved shoulder, which would bring the new length to approximately 1,030 feet. While still not quite in line with the

1,220-foot acceleration lane that the MassDOT standards recommend, the additional length would improve system operations and safety while leaving enough of a buffer before the subsequent ramp. The taper would be reduced from 540 feet to 300 feet, leaving 300 feet before the beginning of the taper for Exit 30. Right-hand shoulder width would be reduced to a minimum of two feet to provide space for the acceleration lane.

### 4.5.2 Alternative 2: Create an Auxiliary Lane for Merging and Diverging Traffic

An auxiliary lane is defined as the portion of the roadway adjoining the traveled freeway for speed change, merging, diverging, weaving, and other purposes supplementary to through-traffic movement. Alternative 2 would create an auxiliary lane between the on-ramp at Exit 29 and the off-ramp at Exit 30. This lane would extend the distance available for merging or diverging traffic maneuvers and would provide sufficient distance to accommodate speed changes and vehicle weaving. The auxiliary lane would also upgrade the acceleration lane to meet MassDOT's standards.

Figure 6 shows the following improvements recommended in Alternative 2:

- Restripe I-95 northbound between Exit 29 and Exit 30 (about one-third of a mile) to accommodate a fifth 12-foot auxiliary lane on the right. This would bring the total lane width to 60 feet along this distance. Use the existing paved area on both the left and right shoulders to provide the required additional width. The highway alignment would need to be shifted to the left by approximately four feet to accomplish this. Alternative 2 would reduce the left shoulder to approximately 6 feet and the right shoulder to a minimum of 2 feet.
- Relocate existing guide signs or install new guide signs and pavement markings to direct drivers to merge onto the mainline or to use Exit 30.
- Modify pavement markings to delineate the auxiliary lane from the mainline travel lanes.

Alternative 2 does present some design difficulties. First, an existing bridge carries l-95 northbound over Lincoln Street in Lexington only 200 feet from the beginning of the gore area at Exit 30. Currently the taper for the Exit 30 ramp extends onto the bridge, and creating an auxiliary lane in this area would require expanding this taper to a full-width lane. The bridge looks to be approximately 64 to 66 feet wide, providing space for five 12-foot lanes and a two- to three-foot offset on each side. These less-than-minimal shoulders would require a Design Exception Report (DER). Second, while the paved shoulder along this stretch of highway is wide enough to accommodate an extra travel lane, it is not wide
enough to fit an additional emergency pullover or stopping area. Any such area would require additional paving and possibly significant grading work because of a moderate slope to the right of the roadway.

### 4.5.3 Alternative 3: Signage Improvements for Exit 30

Because of the high frequency of crashes observed in the vicinity of Exit 30, some signage modifications are recommended. The following improvements are recommended as part of Alternative 3:

- Add a sign for the service plaza at each location where there is a sign for Exit 30A or 30B, to reinforce that this ramp serves all three movements.
- Use a more prominent arrow sign for the service plaza right at the exit.
- Use "Next right" or "Second right" on all signs, or consider using a lane diagram.
- Move the speed limit sign closer to the beginning of the ramp to remind drivers to slow down.

These signage modifications are safety-oriented and do not result in operational improvements.

While signage is a factor, the underlying design of the Route 2A interchange may also play a role in the frequency of crashes observed here. The ramp at Exit 30 leads to a connector-distributor road that serves a high-speed off-ramp, then a service plaza, and then the remaining three legs of the cloverleaf interchange before rejoining the I-95 mainline. The placement of a service plaza in the midst of a high-speed interchange is an unusual design not seen elsewhere in the northeast and may confuse drivers, especially visiting drivers using the service plaza. This confusion could contribute to the high crash rate. However, redesigning the Route 2A interchange would be a high-cost project and is beyond the scope of this report.

### 4.6 EFFECTIVENESS AND COST OF THE IMPROVEMENTS

Table 5 presents the 2030 future LOS analyses compiled using the HCS software. Results for the no-build scenario are compared against Alternative 1 and Alternative 2 for all facilities where modifications affect system operations. All scenarios use a uniform five percent growth for 2030 traffic volumes. Alternative 3 does not affect LOS and is not included in Table 5. Approximations made as part of the HCM analysis are given where applicable.

TABLE 5.
LOS Analysis-Improvement Alternatives:
Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza)

|  | Peak |  | Density <br> (pc/lane <br> mile) | Speed <br> $(\mathrm{mph})$ | VIC <br> Ratio | LOS |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- |

HCM Analysis Type: Basic Freeway Segment

| I-95 northbound | AM | No-Build | 35.5 | 57.6 | 0.88 | E |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| between Exit 29 |  | Alt 2 | 26.6 | 61.4 | 0.71 | D |
|  | ${ }^{*}$ and Exit 30 | No-Build | 41.7 | 53.7 | 0.96 | E |
|  |  | PM $^{2}$ | Alt 2 | 29.6 | 60.5 | 0.77 |
|  |  |  | D |  |  |  |

HCM Analysis Type: Merge Area ${ }^{\text {b }}$

|  |  | No-Build | 36.7 | 52.2 | 0.87 | D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ramp from Route 2 | Alt 1 | 36.6 | 52.5 | 0.87 | D |  |
|  |  | Alt 2 | 36.4 | 53.2 | 0.87 | D |
|  |  | No-Build | N/A | N/A | 1.05 | F |
|  |  | Alt 1 | N/A | N/A | 1.05 | F |
|  |  | Alt 2 | N/A | N/A | 1.05 | F |

HCM Analysis Type: Diverge Area

|  | Exit 30 to Route 2A | No-Build | 35.2 | 51.2 | 0.87 | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| And <br> and service plaza |  | 35.2 | 51.2 | 0.87 | C |  |
|  | PM | No-Build | 38.9 | 51.0 | 0.95 | E |
|  |  | Alt 2 | 38.9 | 51.0 | 0.95 | D |

HCM Analysis Type: Weaving Segment ${ }^{d}$

| I-95 northbound between Exit 29 and Exit 30 | AM | No-Build | N/A | N/A | 1.16 | F |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Alt 2 | N/A | N/A | 1.16 | F |
|  | PM | No-Build | 42.4 | 42.2 | 0.94 | E |
|  |  | Alt 2 | 42.4 | 42.2 | 0.94 | E |

${ }^{2}$ Estimated demand flow rate of 8,800 vph was used as the PM peak volume for all 2030 analyses. It did not develop from existing conditions. The roadway is at capacity and peak spreading is likely to occur when this is the case.
${ }^{\mathrm{b}}$ Uses an acceleration lane of 1,500 feet as an approximation for a full auxiliary lane in the Alternative 2 merge and diverge models.
${ }^{\text {c }}$ HCM does not provide density and speed data for scenarios that result in LOS F.
${ }^{\text {d }}$ Uses a weaving segment of five lanes for No-Build and six lanes for Alt 2 to approximate the effect of an added lane.
HCM = Highway Capacity Manual; LOS = level of service; mph = miles per hour; pc/lane mile = passenger cars per lane mile; V/C = volume-to-capacity; vph = vehicles per hour

### 4.6.1 Effectiveness and Cost of Alternative 1

A Crash Modification Factor (CMF) is an estimate of the change in crashes expected after implementation of a countermeasure. Using CMFs from the Highway Safety Manual (HSM) and the CMF Clearinghouse for lengthening an acceleration lane show that Alternative 1 would reduce crashes at the merge
area by 10 to 20 percent. ${ }^{11,12}$ In addition, Alternative 1 would have a positive, albeit small, effect on traffic operations in the bottleneck. Alternative 1 would not improve the diverge maneuver at Exit 30, the basic freeway capacity, or weaving operations.

Implementing the changes in Alternative 1 would only require restriping the existing Exit 29 ramp area. No right-of-way acquisition, pavement widening, or alignment changes would be required. Alternative 1 is estimated to cost between $\$ 10,000$ and $\$ 20,000$ to construct and would require restriping lanes and lengthening the acceleration lane on I-95 northbound.

### 4.6.2 Effectiveness and Cost of Alternative 2

Using CMFs from the Clearinghouse show that adding continuous auxiliary lane for weaving between entrance ramp and exit ramp would reduce crashes by 20 to 25 percent. Alternative 2 would significantly improve performance in this area, particularly at the Route 2A off-ramp. The LOS for Exit 30 would improve from E to $C$ during the AM peak and from E to D during the PM peak. However, the merge from Route 2 would remain at LOS D in the AM peak and LOS F in the PM peak.

As with Alternative 1, weaving is the limiting factor with the lowest LOS. Alternative 2 does improve LOS for PM weaving from E to D, although according to the model the segment is still over its weaving capacity for the AM peak.

Implementing the changes in Alternative 2 would require restriping to shift the northbound highway alignment to the left by approximately four feet, beginning at Exit 29 and extending through Exit 30. No right-of-way acquisition, pavement widening, or alignment changes should be required. Alternative 2 is estimated to cost between $\$ 50,000$ and $\$ 75,000$ to construct and would require restriping lanes, pavement widening, relocating existing guide signs or installing new guide signs, and pavement markings.

### 4.6.3 Effectiveness and Cost of Alternative 3

Using CMF from the Clearinghouse, Alternative 3 is expected to reduce crashes by up to 20 percent. Alternative 3 would significantly improve safety but would have limited effect on traffic operations in the bottleneck. Alternative 3 is estimated to cost between $\$ 10,000$ and $\$ 20,000$ to construct. This estimate

[^6]includes the cost of installing new signs on overhead gantries, retrofitting existing sign assemblies, and relocating signs.

### 4.7 RECOMMENDATIONS

MPO staff recommends Alternative 2 in conjunction with Alternative 3 because of their beneficial effects on safety and operational efficiency. Alternative 2 removes entering and exiting traffic from the mainline travel lanes to the auxiliary lane. On the other hand, Alternative 1 forces traffic to merge onto the mainline as well as diverge from the mainline to exit the freeway, interrupting traffic flow.

# Chapter 5-Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95) in Woburn and Reading 

Location 2 is on the I-93 southbound barrel before the l-95 interchange in Woburn. Figure 1 shows the location of the bottleneck within the MPO region. The affected section, approximately one-mile long, extends from the beginning of Commerce Way to Exit 37B (I-95 southbound). The interchange and roadways are under the jurisdiction of MassDOT Highway Division, which are located in District 4.

### 5.1 EXISTING FREEWAY CHARACTERISTICS

Operations at this bottleneck are associated with the freeway components described below.

### 5.1.1 BASIC FREEWAY SECTION

The basic freeway section on I-93 southbound has four 12-foot travel lanes, a two- to three-foot left shoulder, and an 11- to 12 -foot right shoulder. During the AM peak period, I-93 southbound carries as many as 7,500 vehicles per hour upstream of the section under study. ${ }^{13}$ The posted speed limit is 65 mph . As a result of recent resurfacing, neither side of I-93 southbound at this location is equipped with a rumble strip.

The basic freeway section on the adjacent I-95 southbound has three 12 -foot travel lanes in the interchange that increase to four lanes after the merge from Exit 37B. It carries up to 6,800 vehicles per hour during the AM peak period and has a posted speed limit of 55 mph . The paved shoulder between ramps is about 10 feet wide.

### 5.1.2 Entrance Ramps

There are two merge facilities relevant to congestion at this bottleneck location. The ramp following Exit 37C on I-93 southbound is an on-ramp with access from Commerce Way. It is a one-way, one-lane roadway with a generous 1,100 -foot

[^7]acceleration lane. ${ }^{14}$ During the peak period, however, it only carries a merging volume of 150 vehicles per hour. Even though the percentage of heavy vehicles is high ( 10.9 percent), the demand at this ramp is too small to affect operations at the bottleneck.

The ramp following Exit 36 on I-95 southbound is an on-ramp that connects to the southern end of Commerce Way. It has a 730 -foot acceleration lane, a posted speed limit of 30 mph , and a peak volume of 1,200 vehicles per hour. It is considered as part of this analysis because of the high peak volume and because the widespread congestion near the I-93/I-95 interchange is likely the result of several interconnected bottlenecks.

### 5.1.3 Exit Ramps

At Exit 37B, the exit ramp to I-95 southbound is a one-way, one-lane roadway. It carries as many as 1,900 vehicles per hour during the AM peak period. The length of the deceleration lane is 980 feet. Based on the highway design and exit ramp curve design speeds, the length of the deceleration lane meets MassDOT's standards. The posted speed limit on the exit ramp curve to $\mathrm{I}-93$ is 30 mph .

Exit 36 on I-95 southbound is a low-volume ramp ( 600 vehicles per hour) that directly follows the merge from I-93 southbound. While the volume makes it unlikely to contribute to bottleneck conditions, it is important to note that recent restriping, which removed a lane upstream from this exit, means drivers now have to execute two lane changes within 1,500 feet to access this exit.

### 5.2 PROBLEMS

The high volume of traffic using Exit 37B during the AM peak period causes queues of exiting vehicles that stretch one-half mile or longer up the rightmost lanes of I-93 southbound. These queues frequently exceed the length of the deceleration lane. As a result of this, some drivers cross the rumble strip and queue in the right side shoulder. Other drivers stay in the main travel lanes and attempt to merge into the queue closer to the exit, either because of the lack of familiarity with the queues or the desire to cut ahead. This behavior interrupts the flow of through traffic on the southbound barrel.

### 5.3 CAUSES

MPO staff identified two factors that contribute to the bottleneck:

[^8]- A high volume of traffic using Exit 37B to I-95 southbound during the AM peak period
- Insufficient queueing space for the ramp for Exit 37B


### 5.3.1 High Volume of Traffic

Figure 7 shows the traffic flows during the AM peak period. MassDOT ATR counts indicate that as many as 1,900 vehicles per hour are served by the Exit 37B ramp. However, vehicle speed data (see Section 5.4.2) and field observations show that there are significant queues present at this ramp during morning hours. This suggests that demand for the facility is likely greater than the capacity of the ramp. MPO staff estimates that the presence of a queue in this location adds 200 vehicles per hour to the peak value, bringing total peak ramp demand to 2,100 vehicles per hour. ${ }^{15}$

In addition to disrupting traffic on I-93 southbound, the high volume of traffic using Exit 37B also affects motorists on I-95 southbound. Merging vehicles interrupt the through traffic on I-95 southbound and force drivers to switch out of the right lane.

### 5.3.2 Insufficient Queueing Space

While the 980 -foot deceleration lane is adequate for safe braking, it can only accommodate a queue of about 50 vehicles. Longer queues typically develop during the AM peak period, causing stopped traffic to spill into the breakdown or through lanes. This stopped traffic both interrupts smooth southbound flow and creates a safety hazard.

### 5.4 IMPACTS

### 5.4.1 Crashes

A summary of the crashes is presented in Table 6. There were 47 crashes in this section between 2010 and 2014 (Appendix C). Figure 8 shows the location of these crashes. The majority, 43 of the crashes, occurred in the vicinity of the diverge area at Exit 37B.

[^9]TABLE 6.
Crash Summary (2010-14):
Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95)

| Crash Variable | Number of Crashes |  |  |
| :---: | :---: | :---: | :---: |
|  | At Merge | At Diverge | Total |
| Crash severity |  |  |  |
| Fatal injury | 0 | 0 | 0 |
| Nonfatal injury | 0 | 13 | 13 |
| Property damage only | 3 | 29 | 32 |
| Not reported/unknown | 1 | 1 | 2 |
| Manner of collision |  |  |  |
| Angle | 2 | 4 | 6 |
| Rear-end | 0 | 23 | 23 |
| Sideswipe, same direction | 1 | 9 | 10 |
| Single-vehicle crash | 1 | 7 | 8 |
| Road surface conditions |  |  |  |
| Dry | 3 | 38 | 41 |
| Wet | 0 | 2 | 2 |
| Snow | 1 | 1 | 2 |
| Ice | 0 | 1 | 1 |
| Other | 0 | 1 | 1 |
| Ambient light conditions |  |  |  |
| Daylight | 0 | 34 | 34 |
| Dark: lighted roadway | 1 | 4 | 5 |
| Dark: nonlighted roadway | 3 | 4 | 7 |
| Dark: unknown roadway lighting | 0 | 1 | 1 |
| Weather conditions |  |  |  |
| Clear | 1 | 28 | 29 |
| Cloudy | 1 | 4 | 5 |
| Rain | 0 | 3 | 3 |
| Snow | 1 | 1 | 2 |
| Not reported/unknown | 1 | 7 | 8 |
| Travel period |  |  |  |
| Peak | 2 | 33 | 35 |
| Off-peak | 2 | 10 | 12 |
| Total crashes | 4 | 43 | 47 |
| Five-year average (rounded) | 1 | 9 | 9 |

Below is a summary of the crashes in this segment:

- 28 percent of the crashes resulted in injury
- 49 percent of the crashes were rear-end collisions, the largest share among collision types
- 87 percent of the crashes occurred under dry roadway conditions
- 28 percent of the crashes occurred outside daylight conditions
- 74 percent of the crashes occurred at peak travel periods

MPO staff believes that many of the rear-end and sideswipe crashes were caused by drivers slowing down to exit the freeway to l-95 or by drivers changing lanes. It appears that the short deceleration lane at this location may be contributing to poor traffic operations and the high number of crashes.

### 5.4.2 Travel Speed

Figure 9 is a congestion scan that shows the average travel speeds on I-93 southbound at the bottleneck location ahead of Exit 37B. The bottleneck present at the I-95 interchange reduces travel speeds to less than 35 mph between the hours of 6 AM and 7 AM. Vehicle speeds this far below free-flow correlate with LOS F conditions on the freeway. Speeds can fall to less than 25 mph for up to half an hour at a time.

Figure 10 is a congestion scan that shows average travel speeds on I-95 southbound, which runs adjacent to the bottleneck at location 2. Conditions during the AM peak period are even worse on I-95 southbound, falling less than 25 mph between the hours of 7 AM and 9 AM . Importantly, the congestion scan shows that slowdowns worsen further down I-95 southbound. This suggests that the I-93 interchange is not the main cause of the congestion and that more issues are present further downstream on I-95.

### 5.4.3 Level of Service

MPO staff conducted traffic operations analyses consistent with HCM methodologies. Using the MassDOT data, MPO staff built traffic analysis networks for the AM peak hours with the HCS suite to assess the capacity and quality of traffic flow at the bottleneck area. ${ }^{16}$ Full HCS reports are included in Appendix D.

Table 7 presents the results of the LOS analyses for existing conditions at the bottleneck on I-93 southbound. The primary bottleneck is located at the diverge area at Exit 37B, but operations at nearby facilities are also included in Table 7.

[^10]In addition, components of I-95 southbound were considered as part of the analysis as they affect merge conditions at the end of the Exit 37B ramp. Some simplifications were necessary to fit the HCS model more closely with observed conditions and are stated in the table notes.

TABLE 7. LOS Analysis-Existing Conditions:
Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95)

| Location | Density (pc/lane mile) | Speed (mph) ${ }^{\text {a }}$ | VIC <br> Ratio | LOS ${ }^{\text {b }}$ |
| :---: | :---: | :---: | :---: | :---: |
| HCM Analysis Type: Basic Freeway Segment |  |  |  |  |
| I-93 southbound: Between Exit 37C and Exit 37 B | 32.7 | 59.3 | 0.84 | D |
| I-95 southbound: Between Exit 37 and Exit 36 | 29.5 | 51.3 | 0.68 | D |
| HCM Analysis Type: Merge Area ${ }^{\text {c }}$ |  |  |  |  |
| I-93 southbound: Ramp from Commerce Way | 33.5 | 57.2 | 0.83 | C |
| I-95 southbound: Ramp from I-93 southbound ${ }^{\text {de }}$ | $\mathrm{N} / \mathrm{A}^{\dagger}$ | N/A | 0.74 | F |
| I-95 southbound: Ramp from Commerce Way | 36.6 | 49.4 | 0.81 | D |

HCM Analysis Type: Diverge Area I-93 southbound: Exit 37B to I-95 southbound

N/A
N/A
0.83

F
I-95 southbound: Exit 36 to Commerce Way
31.7
47.9
0.79

C
HCM Analysis Type: Weaving Segment
I-95 southbound: Between Exit 37
N/A N/A
1.13

F and Exit $36^{9}$
${ }^{\text {a }}$ Refers to ramp influence area speed for merge/diverge areas.
${ }^{\mathrm{b}}$ LOS A through LOS D represent acceptable operating conditions; LOS E represents operating conditions at capacity; and LOS F represents failing conditions (demand exceeds capacity).
${ }^{\mathrm{c}}$ In HCM merge and diverge analyses, acceleration and deceleration lanes are measured from the tip of the painted gore to the end of the taper. This may differ from the AASHTO length.
${ }^{\text {d }}$ Uses maximum acceleration lane length of 1,500 feet to approximate a lane addition at this merge.
${ }^{e}$ Estimated demand flow rate of 2,100 vph used for Exit 37B ramp volumes in all existing condition analyses (see Section 5.3.1).
${ }^{\dagger} \mathrm{HCM}$ does not provide density and speed data for scenarios that result in LOS F.
${ }^{9}$ Uses a weaving segment of five lanes; therefore, limiting factor is weaving behavior and not mainline capacity. (HCM weaving analysis assumes a lane drop after the merge.)
HCM = Highway Capacity Manual; LOS = level of service; mph = miles per hour; pc/lane mile = passenger cars per lane mile; V/C = volume-to-capacity; vph = vehicles per hour

Table 7 shows that the Exit 37B ramp from I-93 southbound operates at LOS F at both ends (the diverge on I-93 and the merge on I-95). However, the volume-tocapacity (V/C) ratio for both of these facilities is well below 1.0, indicating that the capacity to serve merging and diverging maneuvers is not exceeded. The reason these facilities fail is because the ramp itself is over capacity: the ramp roadway has a V/C ratio of 1.14, meaning the volume experienced on this ramp is 14 percent above the theoretical maximum throughput of a ramp with the given characteristics. (Any V/C ratio above 1.0 causes LOS F operations.) All other facilities operate at LOS D or above.

### 5.5 IMPROVEMENT ALTERNATIVES

MPO staff developed the following improvements to address safety and operational issues at the bottleneck:

- Alternative 1: On I-93 southbound, create an auxiliary lane for merging and diverging traffic at Exit 37B (Figure 11)
- Alternative 2: On I-95 southbound, lengthen the acceleration lane at the merge from Commerce Way (Figure 12)
- Alternative 3: On the ramp connecting Exit 37B to I-95 southbound: consider employing a two-lane exit ramp (Figure 13)

The alternatives were analyzed using projected year 2030 traffic volumes. MPO staff estimated a five percent total background growth from 2017 to 2030.

### 5.5.1 Alternative 1: Create an Auxiliary Lane for Merging and Diverging Traffic at Exit 37B

Alternative 1 would extend the deceleration lane and create a full-width auxiliary lane between the on- and off-ramps. This lane would provide drivers with ample distance to decelerate safely and comfortably enter and exit the freeway. More importantly, it would also increase the available space for vehicles queueing for Exit 37B, keeping them sheltered from the high-speed traffic on the main southbound barrel.

Figure 11 shows the improvements recommended in Alternative 1:

- Add a 12-foot auxiliary lane in the southbound direction for a distance of approximately one mile between Exit 37C and Exit 37B. Use the available 12 -foot shoulder for this auxiliary lane, and add an additional one- to twofeet of pavement widening where necessary to provide for a minimum twofoot shoulder.
- Relocate existing guide signs or install new guide signs and pavement markings to direct drivers to merge onto the mainline or to use Exit 37B.
- Modify pavement markings to delineate the auxiliary lane from the mainline travel lanes.

Because widening will not be possible on the bridge over West Street, a minor leftward shift (one to two feet) of the highway alignment may be necessary in this area if the right shoulder cannot provide enough width. There is plenty of clearance on the left shoulder on the bridge to allow for this shift.

### 5.5.2 Alternative 2: Lengthen the Acceleration Lane at the Merge from Commerce Way

I-95 southbound experiences chronic congestion during the AM peak period. While the merge from Commerce Way is not directly adjacent to the problem area, it is possible that it contributes to congested conditions on I-95, which may in turn reduce the capacity of the Exit 37B ramp.

While the existing acceleration lane is adequate according to MassDOT design standards, the ramp serves a high volume of traffic (1,200 vehicles per hour) during the AM peak. Extending the acceleration lane would help this traffic merge onto the I-95 mainline safely and efficiently.

Figure 12 shows the improvements recommended in Alternative 2:

- Extend the full-width acceleration lane at the Exit 36 on-ramp by 460 feet, lengthening it from 700 feet to 1,160 feet. Use the existing right-hand shoulder width (about 10 feet) and shift the highway alignment to the left by up to four feet where necessary to yield space for the 12-foot acceleration lane extension and two-foot shoulder. Shift the alignment into the existing 10 -foot left shoulder where necessary.
- Modify pavement markings in accordance with the new acceleration lane geometry.


### 5.5.3 Alternative 3: Use a Two-Lane Ramp at Exit 37B

Because the demand flow rate at Exit 37B (2,100 vehicles per hour) exceeds the capacity for a single-lane roadway, it is likely that the ramp itself is the limiting factor at this interchange. For this reason, the MPO staff decided to compare the advantages of this higher-cost alternative that would have the potential to increase capacity on the exit ramp.

Using a two-lane ramp at Exit 37B would require significant geometric changes on both I-93 southbound and I-95 southbound. Figure 13 shows the improvements recommended in Alternative 3:

- Create an auxiliary lane as in Alternative 1 on I-93 southbound
- Use a two-lane exit consisting of two exit-only lanes: the abovementioned auxiliary lane and the fourth lane (second from right)
- Drop the rightmost lane for the bridge over I-95, and re-add the lane at the merge from I-95 southbound
- Use existing shoulder space to widen the freeway to five lanes between exits 37 and 36 on 1-95 southbound, establishing lane balance in this stretch. The right-most lane would become an exit-only lane and would be dropped at Exit 36

While all of the other modifications mentioned above would be relatively minor in scale, the expansion of the ramp would require construction and, possibly, land takings, both at significant cost. The existing ramp is tightly spaced: directly abutting it to the left is the on-ramp from I-95 southbound, while the nearest property line is only approximately 50 feet from the edge of the pavement. There is also a fairly significant downgrade in this direction, meaning adding a lane on the right side of the ramp would probably require fill, and the resulting embankment could extend beyond the existing right-of-way.

### 5.6 EFFECTIVENESS AND COST OF THE IMPROVEMENTS

Table 8 presents the 2030 future LOS analyses compiled using the HCS software. Results for the no-build scenario are compared against Alternative 1, Alternative 2, and Alternative 3 for all facilities where modifications affect system operations. All scenarios use a uniform five percent growth for 2030 traffic volumes. Approximations made as part of the HCM analysis are given where applicable.

TABLE 8.
LOS Analysis-Improvement Alternatives:
Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95)

| Location | Scenario | Density (pc/lane mile) | Speed (mph) | VIC Ratio | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| HCM Analysis Type: Basic Freeway Segment |  |  |  |  |  |
| I-93 southbound: Between Exit 37C and Exit 37B | No-Build | 35.2 | 57.8 | 0.88 | E |
|  | Alt 1 | 26.3 | 62.0 | 0.70 | D |
| I-93 southbound: After Exit 37B | No-Build | 24.4 | 62.2 | 0.65 | C |
|  | Alt 3 | 35.0 | 57.9 | 0.87 | D |
| I-95 southbound: Between <br> Exit 37 and Exit 36 | No-Build | 34.0 | 51.3 | 0.79 | D |
|  | Alt 3 | 27.6 | 50.7 | 0.63 | D |
| HCM Analysis Type: Merge Area |  |  |  |  |  |
| I-93 southbound: Ramp from | No-Build | 35.5 | 56.8 | 0.87 | C |
| Commerce Way ${ }^{\text {a }}$ | Alt 1 | 35.3 | 57.4 | 0.87 | C |
| I-95 southbound: Ramp from | No-Build | 38.8 | 49.0 | 0.85 | D |


| Commerce Way | Alt 2 | 38.6 | 49.4 | 0.85 | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| I-95 southbound: Ramp from | No-Build | N/A ${ }^{\text {b }}$ | N/A | 0.78 | F |
| I-93 southbound | Alt 3 | 34.0 | 51.2 | 0.78 | A |
| HCM Analysis Type: Diverge Area |  |  |  |  |  |
| I-93 southbound: Exit 37B to | No-Build | N/A | N/A | 0.87 | F |
| I-95 southbound | Alt 1 | N/A | N/A | 0.87 | F |
|  | Alt $3^{\text {c }}$ | 35.7 | 48.9 | 0.87 | A |
| I-95 southbound: Exit 36 to | No-Build | 33.5 | 47.8 | 0.83 | D |
| Commerce Way | Alt 3 | 35.2 | 47.8 | 0.87 | C |
| HCM Analysis Type: Weaving Segment ${ }^{\text {d }}$ |  |  |  |  |  |
| I-95 southbound: Between | No-Build | N/A | N/A | 1.19 | F |
|  | Alt 3 | N/A | N/A | 1.19 | F |

[^11]
### 5.6.1 Effectiveness and Cost of Alternative 1

CMF from HSM and the CMF Clearinghouse shows that adding a continuous auxiliary lane for weaving between entrance ramp and exit ramp would reduce crashes by 20 to 25 percent. Alternative 1 was able to improve the LOS of the basic freeway segment on I-93 southbound from LOS E to LOS D, meaning capacity of the facility was significantly improved.

The LOS experienced by motorists using Exit 37B remains unchanged at LOS F because the ramp capacity is unaffected. The V/C ratio of the Exit 37B ramp roadway increases from 1.14 to 1.20 under 2030 no-build conditions, resulting in LOS F performance for both the diverge at Exit 37B and the merge with I-93 southbound at the end of the ramp. However, these metrics do not take into account the safety and driver comfort provided by the additional queue space present under Alternative 1.

Alternative 1 is estimated to cost between $\$ 100,000$ to $\$ 200,000$ to construct. This estimate includes preparing the shoulder for a travel lane, restriping travel lanes, relocation and installation of signs, new rumble strips, and pavement markings. New paving may be required if an emergency pullover area is necessary.

### 5.6.2 Effectiveness and Cost of Alternative 2

CMF from HSM and the CMF Clearinghouse shows that lengthening an acceleration lane would reduce crashes by 10 to 20 percent. Alternative 2 was able to increase LOS at the on-ramp at Exit 36 (from Commerce Way to I-95 southbound) from $D$ to $C$, even though the speed and density at this merge were essentially unchanged. This may lead to an improvement, albeit small, in the overall capacity of I-95 southbound in this area. While this may also lead to improved operations at the I-93 interchange and consequently at the bottleneck on I-93 southbound, HCM analysis methods are unable to directly correlate these two outcomes.

Alternative 2 is estimated to cost between \$50,000 and \$75,000 to construct and would require lengthening the acceleration lane, restriping travel lanes, minor paving, and relocating rumble strips.

### 5.6.3 Effectiveness and Cost of Alternative 3

CMF for converting a single-lane exit into a two-lane exit shows that Alternative 2 would reduce crashes at Exit 37B by up to 30 percent. Alternative 3 was the only option able to improve the LOS on the facilities at Exit 37B. Both the merge and diverge area change from LOS F to LOS A when the ramp is widened to two lanes. Accordingly, the V/C ratio for the ramp roadway is cut in half, improving from 1.20 to 0.60 . This configuration required removing a lane on I-93 southbound downstream from the exit, which lowered the LOS in this area from C to D

While the projected LOS improvements under Alternative 3 are significant, in reality induced demand as direct result of the improvements could lower the LOS from A to B or C. Alternative 3 is estimated to cost approximately \$ 1.0million, which would include widening on the ramp to two lanes, reconfiguring travel lanes on both I-93 and I-95, installing new signs, preparing the shoulder on I-95 southbound for a travel lane, and new paving and rumble strips.

### 5.7 LONG-TERM PLAN FOR I-93/I-95 INTERCHANGE

The Massachusetts Office of Transportation Planning has a long-range plan for the I-93/I-95 interchange because of its chronic problems. ${ }^{17}$ Conceptual alternatives for this plan are focused around adding flyovers or underpasses for some of the ramps at the interchange. Although it would keep all ramps with a single lane, this design would reduce the number of merge areas and make all

[^12]ramps high speed, both of which would greatly increase overall capacity at the interchange. The new configuration would also reduce traffic noise experienced in neighboring residential communities by increasing clearance and adding noise barriers. The potential major investment planned at this interchange should be taken into account when deciding on short-term solutions.

### 5.8 RECOMMENDATIONS

MPO staff recommends Alternatives 1 and 2, both of which are low-cost solutions. Together, they would produce maximum operational benefits as Alternative 2 would reduce a downstream bottleneck and allow the auxiliary lane to function well. Because the I-93 and I-95 interchange already has a long-term improvement planned for it, the low-cost improvements identified in Alternatives 1 and 2 align with the objectives and vision for the interchange. Although Alternative 3 improves the LOS on the exit ramp, it is costly and will affect the abutting properties, and must be considered while taking into account the longterm plans for the interchange.

# Chapter 6-Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton 

Location 3 is a stretch of Route 24 northbound leading up to its northern terminus at the interchange with Interstate 93 (Route 24, Exit 21). Figure 1 shows the location of the bottleneck within the MPO region. The high volumes at this merge are the main cause for poor operating conditions. During the AM peak period, congestion can extend south for more than five miles, all the way into Avon. ${ }^{18}$ The segment in question begins in Stoughton, which is in MassDOT Highway Division, District 5, and continues north through Canton and Randolph, which are both in MassDOT Highway Division, District 6.

### 6.1 EXISTING FREEWAY CHARACTERISTICS

Operations at this bottleneck are associated with the freeway components described below.

### 6.1.1 BASIC FREEWAY SECTION

Route 24 northbound is a freeway segment with three 12-foot travel lanes, a 12to 13 -foot right shoulder, and a two- to three-foot left shoulder. This segment carries volumes of up to 4,600 vehicles per hour during the AM peak because of the severe bottleneck at the interchange with I-93, with trucks comprising a not insignificant amount of the volume at approximately five percent. The posted speed limit is 65 mph on the Route 24 northbound mainline and decreases to 50 mph at the ramps. Rumble strips are present on the right side of the northbound barrel.

### 6.1.2 Major Diverge Area

A major diverge occurs when a basic freeway segment with three or more lanes splits into two multilane roadways. This is the case at the end of Route 24 northbound, where the main barrel splits into two two-lane, high-speed ramp segments that connect to I-93 northbound and southbound. The speed limit decreases from 65 mph to 50 mph at the connector ramps.

[^13]
### 6.1.3 Merge Areas

The right branch of Route 24 northbound merges with I-93 northbound at a major merge area. Figure 14 shows the lane configuration at this location. Here, the two-lane ramp merges into the right side of the three-lane main barrel. These five total lanes become a four-lane freeway by combining the two center lanes. This ramp serves approximately 2,300 vehicles per hour during the AM peak period.

The left branch of Route 24 northbound merges with I-93 southbound on the lefthand side, and continues in its own lane as shown in Figure 15. Approximately 1,200 feet before the merge with I-93, however, the two-lane traffic on the ramp is forced to merge into a single travel lane. This is the result of restriping that took place between 2010 and 2013. ${ }^{19}$ This ramp serves approximately 2,300 vehicles per hour during the AM peak period.

### 6.2 PROBLEMS

The existing bottleneck creates intense interruption of traffic flow during the AM peak travel period. During these hours, queues of up to five miles long form as drivers wait to merge onto l-93 southbound. These waiting drivers back up onto the Route 24 northbound mainline and prevent vehicles from accessing the otherwise uncongested ramp to l-93 northbound. This scenario results in slow speeds and low LOS that affect virtually all drivers using the facility. The bottleneck also likely contributes to crashes in this area.

### 6.3 CAUSES

MPO staff identified four primary factors contributing to this bottleneck:

- A high volume of traffic using Exit 21 to I-93 during the AM peak period
- A short diverge length where the two ramps split at the I-93 interchange
- The forced merge to a single lane on the I-93 southbound ramp
- A short merge length at the I-93 northbound ramp


### 6.3.1 High Volume of Traffic

Figure 14 shows the hourly traffic flow during the AM peak period. Usage of both the I-93 ramps is very high, especially in the AM peak as traffic flows north towards Boston and the business areas located along Route 128. The merging and diverging maneuvers of these vehicles interrupt traffic flow and reduce capacity, resulting in a traffic bottleneck.

[^14]
### 6.3.2 Short Widening Distance at Major Diverge

The three-lane Route 24 northbound barrel begins to widen to four lanes only approximately 190 feet ahead of the painted gore nose at the I-93 ramps. The short maneuvering distance available causes sudden maneuvers, reducing speeds and producing unsafe conditions.

### 6.3.3 Merge to Single Lane on I-93 Southbound Ramp

The ramp to I-93 southbound serves up to 2,300 vehicles per hour during the AM peak. On most mornings there is also a queue of vehicles waiting to use the ramp that can extend for up to five miles down Route 24. MPO staff estimate that the presence of a queue in this location adds 700 vehicles per hour to the peak value, bringing total peak demand for the I-93 southbound ramp to 3,000 vehicles per hour. ${ }^{20}$

According to the HCM, the capacity for a single lane ramp roadway segment with a free-flow speed of 50 mph is 2,200 vehicles per hour. ${ }^{21}$ Therefore the practical capacity of this ramp is exceeded even before queued vehicles are considered. This leads to severe congestion and is the largest contributor to bottleneck conditions at this location.

### 6.3.4 Geometry at I-93 Northbound Merge

At major merge locations with lane drops, MassDOT design standards recommend that only the rightmost lanes be forced to merge. This is not the case at the I-93 northbound merge, where the middle lanes merge. Merging these lanes instead of the exterior lanes causes safety issues because of the higher vehicle speeds, and also may lead to confusion regarding who has the right of way. The merge also begins only 90 feet from the end of the gore area, forcing drivers to make very rapid maneuvers.

Because of the proximity to the next off-ramp (the ramp to Route 28 southbound begins to diverge only 1,450 feet downstream from the Route 24 merge), the only option for changing the geometry at this merge is to add an auxiliary lane covering the full distance between the two ramps. The existing shoulder along this stretch is not adequate to accommodate a fifth travel lane; creating an auxiliary lane would require extensive paving and fill, making this a high-cost option and, therefore, outside of the scope of this report. An analysis of an auxiliary lane on this segment of I-93 northbound can be found in the Boston

[^15]MPO's 2007 memorandum "Safety and Operational Improvements for the I93/Route 24 Interchange." ${ }^{22}$

### 6.4 IMPACTS

### 6.4.1 Crashes

A summary of the crashes in this segment is presented in Table 9. There were 96 crashes in this area between 2010 and 2014 (Appendix C). Figure 15 shows the location of these crashes. The majority ( 63 crashes) occurred leading up to the diverge at the l-93 interchange.

TABLE 9.
Crash Summary (2010-14):
Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93)

|  | Number of Crashes |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Rte. 24 NB <br> Exit 21 <br> (Diverge) | Merge <br> with I-93 <br> NB | Merge <br> with I-93 |  |
| Crash Variable |  |  |  | Total |
| Crash severity | 1 | 0 | 0 | 1 |
| Fatal injury | 22 | 7 | 4 | 33 |
| Non-fatal injury | 32 | 10 | 10 | 52 |
| Property damage only | 8 | 1 | 1 | 10 |
| Not reported |  |  |  |  |
| Manner of collision | 1 | 3 | 1 | 5 |
| Angle | 0 | 0 | 1 | 1 |
| Head-on | 24 | 9 | 4 | 37 |
| Rear-end | 10 | 2 | 2 | 14 |
| Sideswipe, same direction | 28 | 4 | 7 | 39 |
| Single-vehicle crash | 52 | 13 | 10 | 75 |
| Road surface conditions | 3 | 0 | 1 | 4 |
| Dry | 8 | 5 | 4 | 17 |
| Snow |  |  |  |  |
| Wet | 3 | 1 | 0 | 4 |
| Ambient light conditions | 38 | 11 | 12 | 61 |
| Dawn | 2 | 1 | 1 | 4 |
| Daylight |  |  |  |  |
| Dusk |  |  |  |  |

[^16]| Dark: lighted roadway | 3 | 2 | 1 | 6 |
| :--- | :---: | :---: | :---: | :---: |
| Dark: roadway not lighted | 16 | 3 | 1 | 20 |
| Dark: unknown lighting | 1 | 0 | 0 | 1 |
| Weather conditions |  |  |  |  |
| Clear | 41 | 11 | 7 | 59 |
| Cloudy | 10 | 0 | 3 | 13 |
| Rain | 1 | 3 | 2 | 6 |
| Snow | 4 | 0 | 1 | 5 |
| Not reported | 7 | 4 | 2 | 13 |
| Travel period | 27 | 7 | 8 | 42 |
| Peak | 36 | 11 | 7 | 54 |
| Off-peak | 63 | 18 | 15 | 96 |
| Total crashes | 13 | 4 | 3 | 19 |
| Five-year average <br> (rounded) |  |  |  |  |

Below is a summary of the crashes in this area:

- 35 percent of the crashes resulted in injury, including one fatal injury
- 41 percent of the crashes were single-vehicle collisions, the largest share among collision types
- 44 percent of the crashes occurred during the peak travel period
- 28 percent of the crashes occurred outside daylight conditions
- 78 percent of the crashes occurred under dry roadway conditions


### 6.4.2 Travel Speed

Figure 16 is a congestion scan that shows the average travel speeds on Route 24 northbound ahead of the bottleneck at the I-93 interchange. Congestion at this location reduces travel speeds to less than 35 mph between the hours of 6 AM and 9 AM . Vehicle speeds this far below free-flow correlate with a freeway LOS of $F$. Speeds on this segment can fall to less than 25 mph for up to 45 minutes at a time. Varying levels of congestion extend for more than six miles down Route 24. One notable feature of the congestion scan is that speeds begin to improve slightly approximately one-half mile ahead of the interchange. This is the result of traffic headed to I-93 northbound finally being able to pass the queue for I-93 southbound when they near the ramps. No congestion develops outside of AM peak hours.

Travel on I-93 is also affected by this bottleneck. Figure 17 shows a congestion scan for l-93 northbound near Route 24, and Figure 18 shows a congestion scan for I-93 southbound near Route 24. The congestion scans show moderate congestion on these roadways during the AM peak period. On I-93 northbound,
traffic near the Route 24 interchange slows less than 45 mph between the hours of 8 AM and 9 AM. However, the scan shows that this is the tail end of congestion that originates further north on I-93. On I-93 southbound, congestion present between 7 AM and 9 AM slows travel speeds to less than 45 mph . Unlike the congestion in the northbound direction, this slowdown peaks around the Route 24 interchanges and begins to dissipate soon afterwards, suggesting that this interchange is the cause.

### 6.4.3 Level of Service

MPO staff conducted traffic operations analyses consistent with HCM methodologies. Using the MassDOT data, MPO staff built traffic analysis networks for the AM peak hours with the HCS suite to assess the capacity and quality of traffic flow at the bottleneck area. ${ }^{23}$ Full HCS reports are included in Appendix D.

Unfortunately, the HCM is unable to model performance effectively for major merge or diverge areas. LOS can be approximated by checking capacities of each component segment as basic freeway segments. However, using a basic freeway segment tends to overestimate the capacity of merge or diverge areas because merging maneuvers are ignored and because traffic is assumed to be evenly distributed across all lanes. The results of the analysis are shown in Table 10.

[^17]

Table 10 shows that the merge to I-93 southbound operates at LOS F during the AM peak period. However, the V/C ratio for this facility is well below 1.0, indicating that its capacity to accommodate merge maneuvers is not exceeded. The reason the facility fails is because the ramp itself is over capacity: the ramp roadway has a V/C ratio of 1.16, meaning the volume experienced on this ramp is 16 percent above the theoretical maximum throughput of a ramp with the given characteristics. (Any V/C ratio above 1.0 causes LOS F operations.) The merge area operates at LOS C during the AM peak, although, as stated before, this model is an approximation that will generally predict a LOS better than that experienced by drivers.

### 6.5 IMPROVEMENT ALTERNATIVES

MPO staff developed the following improvements to address safety and operational issues at the bottleneck:

- Alternative 1: Widen Route 24 northbound to four lanes for a stretch of approximately 1,200 feet between the I-93 interchange and the horse bridge (Figure 19).
- Alternative 2: Widen Route 24 northbound to four lanes in a similar manner to Alternative 1, but continue the extra lane south until the Canton Street bridge for a total length of approximately 4,000 feet (Figure 20).
- Alternative 3: Remove the merge on the ramp to I-93 southbound (Figure 21).

The alternatives were analyzed using projected year 2030 traffic volumes. MPO staff estimated a five percent total background growth from 2017 to 2030.

### 6.5.1 Alternative 1: Widen Route 24 Northbound to Four Lanes between I-93 and Horse Bridge

The 36-foot, three-lane mainline of Route 24 northbound widens to a 48 -foot, four-lane diverge section only approximately 200 feet before the tip of the merge gore area. MPO staff recommends extending the four lanes present on the ramp for 1,200 feet down Route 24.

Figure 19 shows the improvements recommended in Alternative 1:

- Begin a taper shortly after the existing horse bridge that expands the righthand travel lane to two 12-foot lanes over a distance of 600 feet.
- Continue these four lanes for 1,200 feet up through the diverge at the I-93 ramps. There is adequate paved shoulder on the right-hand side to accommodate the extra travel lane and maintain a two-foot right shoulder along this distance.
- Switch to exit-only lanes one-half mile upstream from the diverge. Indicate this change using overhead signage and a wide dotted line between the middle two lanes, as can be seen at the diverge between l-93 northbound and Route 3 southbound at the Braintree split.
- Create one emergency pullover area using new paving to address incidents and safety concerns related to the use of the shoulder as a travel lane.


### 6.5.2 Alternative 2: Widen Route 24 Northbound to Four Lanes between I-93 and Canton Street

The modifications present in Alternative 1 help to address the vehicle slowdowns and safety risks that come as a result of turbulence ahead of the Exit 21 diverge. What is not addressed, however, is the fact that the queue for I-93 southbound inhibits vehicles from using the ramp to l-93 northbound. Since Alternative 1 only proposes a fourth lane across a distance of approximately one-quarter mile, any queues longer than this still have the potential to block access to the northbound ramp.

Alternative 2 would extend the fourth travel lane nearly one mile down to the bridge over Canton Street in Randolph. This would provide more room for approximately 400 vehicles to queue in the left two lanes for I-93 southbound without interrupting other traffic. While there is adequate right-hand side shoulder space for a fourth lane along almost this entire stretch, accommodating the horse
bridge that passes over Route 24 may require a slight shift to the left of the traveled way.

Figure 20 shows the improvements recommended in Alternative 2:

- Begin a taper shortly after the existing bridge over Canton Street that expands the right-hand travel lane to two 12-foot lanes over a distance of 600 feet.
- Continue these four travel lanes for 4,000 feet through the diverge at the I93 ramps. Use the existing right-hand side paved shoulder for this new lane, and maintain a two-foot right shoulder.
- Shift the highway alignment to the left slightly, starting 400 feet upstream from the horse bridge and ending 400 feet downstream from it. This shift is required because of decreased right-hand shoulder space near the bridge footing. The maximum shift would be two feet and would occur as Route 24 passes under the horse bridge. Use the existing left-hand side paved shoulder to accommodate this shift. Relocate the existing left guardrail.
- Switch to exit-only lanes one-half mile upstream from the diverge. Indicate this change using overhead signage and a wide dotted line between the middle two lanes, as can be seen at the diverge between l-93 northbound and Route 3 southbound at the Braintree split.


### 6.5.3 Alternative 3: Remove the Merge on the Ramp to I-93 Southbound

The ramp from Route 24 northbound to l-93 southbound is wide enough to accommodate two travel lanes and was previously striped in this way. MPO staff recommends returning to a two-lane ramp to better meet the demand during the AM peak period.

Figure 21 shows the improvements recommended in Alternative 3:

- Remove the merge on the ramp from Route 24 northbound to I-93 southbound. Use the hatched area on the right side of the ramp to continue the second ramp lane.
- Add a 1,000-foot acceleration lane for the leftmost ramp lane. This is the distance the MassDOT design guide recommends before forcing a lane drop at a major merge area. Shift the I-93 southbound highway alignment to the right along this distance to accommodate a fifth 12-foot travel lane. Use the existing paved area on both the left and right shoulders to provide the required additional width. The left shoulder would be reduced from 10 feet to two feet, and the right shoulder would be reduced as needed by up to three feet from approximately 10 feet to seven feet. Follow the acceleration lane with a 500-foot taper.
- Shift the left-hand and right-hand rumble strips along this stretch to match the new lane configuration.
- Add new guide signs and appropriate MUTCD-compliant pavement markings to direct drivers to merge right from the acceleration lane.

The length of the acceleration lane and subsequent taper may be limited by the culvert structure that carries the Blue Hill River.

### 6.6 EFFECTIVENESS AND COST OF THE IMPROVEMENTS

Table 11 presents the 2030 future LOS analyses compiled using the HCS software. Results for the no-build scenario are compared against Alternatives 1 and 2 combined and Alternative 3 for all facilities where modifications affect system operations. (The main difference between Alternative 1 and Alternative 2 is the queue length they can accommodate, and because this does not affect HCM analysis they are combined in Table 11.) All scenarios use a uniform five percent growth for 2030 traffic volumes. Approximations made as part of the HCM analysis are given where applicable.

TABLE 11.
LOS Analysis-Improvement Alternatives:
Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93)

| Density <br> (pc/lane <br> mile) | Speed <br> (mph) | VIC <br> Ratio | LOS |
| :---: | :---: | :---: | :---: |

HCM Analysis Type: Basic Freeway Segment

| Route 24 northbound at | No-Build | 27.4 | 62.0 | 0.73 | D |
| :--- | :---: | :--- | :--- | :--- | :--- |
| diverge | Alt 1 and 2 | 20.7 | 61.5 | 0.55 | C |
| I-93 southbound after merge | No-Build | 35.6 | 51.8 | 0.83 | E |

HCM Analysis Type: Merge Area ${ }^{a}$

| Merge with I-93 southbound | No-Build | N/A ${ }^{\text {b }}$ | N/A | 0.83 | F |
| :--- | :---: | :---: | :---: | :---: | :---: |
|  | Alt 3 | 36.6 | 51.0 | 0.83 | B |

${ }^{a}$ Uses maximum acceleration lane length of 1,500 feet and a four-lane mainline to approximate a lane addition at this merge.
${ }^{\mathrm{b}}$ HCM does not provide density and speed data for scenarios that result in LOS F.
HCM = Highway Capacity Manual; LOS = level of service; mph = miles per hour; pc/lane mile = passenger cars per lane mile; V/C = volume-to-capacity

### 6.6.1 Effectiveness and Cost of Alternative 1

A CMF is an estimate of the change in crashes expected after implementation of a countermeasure. Using CMFs from the CMF Clearinghouse for installing an additional lane for an urban freeway shows that Alternative 1 would reduce
crashes at the diverge area by up to 20 percent. ${ }^{24,25}$ As mentioned before, the only methodology HCM provides to study major diverge areas is to model them as basic freeway segments. Table 11 compares an analysis of a three-lane basic freeway segment at the diverge with a four-lane basic freeway segment. The additional lane improves LOS by one level over the no-build scenario, bringing it to LOS C from LOS D during the AM peak period.

The basic freeway segment analysis can be misleading because the real cause of the bottleneck is diverging vehicles and not the base capacity of the freeway. However, the analysis demonstrates that adding the lane significantly increases capacity. This increased capacity will help to offset the capacity reduction resulting from the diverge. The extra lanes will also help avoid driver confusion at the split lane, and allow traffic heading to I-93 northbound to bypass the queued traffic heading to I-93 southbound during the AM peak period.

Alternative 1 is estimated to cost between $\$ 100,000$ and $\$ 200,000$ to construct. This estimate includes preparing the shoulder for a travel lane, restriping travel lanes, relocation and installation of signs, and minor pavement markings. It may require a DER for using a less-than-minimal right shoulder. New paving may be required if an emergency pullover area is necessary.

### 6.6.2 Effectiveness and Cost of Alternative 2

Alternative 2 is expected to reduce crashes by the same percentage as in Alternative 1. Based on parameters that HCM methodology can measure, Alternative 2 performs the same as Alternative 1. However, the extended fourth travel lane will increase capacity on Route 24 over a longer distance and allow more drivers to use this extra lane to skip morning queues that develop in advance of the I-93 southbound merge. Alternative 2 is estimated to cost between $\$ 300,000$ and $\$ 400,000$ to construct. Similar to Alternative 1, Alternative 2 may require a DER for using a less-than-minimal right shoulder, and new paving may be required if an emergency pullover area is necessary.

### 6.6.3 Effectiveness and Cost of Alternative 3

Using CMFs from the HSM and the CMF Clearinghouse for lengthening an acceleration lane show that Alternative 3 would reduce crashes at the merge area by 10 to 20 percent. ${ }^{26,27}$ Using estimates for ramp roadway capacity, the

[^18]single lane I-93 southbound ramp will be at a V/C ratio of 1.21 under the 2030 no-build scenario. A V/C ratio higher than 1.0 indicates that not only is user experience very poor, but that the facility cannot meet demand and extensive queues will form. This may lead to problems on nearby facilities. With a two-lane ramp, the V/C ratio drops to 0.61 , demonstrating that two lanes are sufficient to meet the projected future demand.

The one- and two-lane ramps were also compared as traditional merge segments. Using this analysis, the two-lane ramp improved from LOS F to LOS B. However, the downstream basic freeway segment (after I-93 southbound returns to four travel lanes) has a LOS of E in 2030 and will not be changed by either proposed alternative. Therefore the downstream freeway segment is the limiting factor, meaning that only merging vehicles will see improved operations and through traffic will experience no change from Alternative 3.

Alternative 3 is estimated to cost between $\$ 100,000$ and $\$ 200,000$ to construct. This estimate consists of restriping the connector ramp, pavement markings, and preparing a short segment of shoulder on l-93 southbound to allow a two-lane entry from Route 24 northbound to l-93 southbound.

### 6.7 RECOMMENDATIONS

MPO staff recommends implementation of both Alternative 2 and Alternative 3 to improve operational efficiency for all traffic on Route 24 northbound. For a more in-depth discussion of alternatives affecting this bottleneck, including right-hand ramps and auxiliary lane additions, refer to the Boston MPO's 2007 report on this location. ${ }^{28}$

[^19]
# Chapter 7-Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139) in Randolph, Canton, and Stoughton 


#### Abstract

Location 4 is on Route 24 southbound after the Interstate 93 interchange. Figure 1 shows the location of the bottleneck within the MPO region. The high volumes at these ramps are the main cause of poor operating conditions. Heavy congestion is usually present on both the Route 24 southbound ramps for the entire duration of the PM peak period. ${ }^{29}$ The study area begins at the I-93 interchange in Randolph (I-93 Exit 4) and extends southward through Canton to the Route 139 ramp in Stoughton (Route 24 Exit 20). Randolph and Canton are part of MassDOT Highway Division, District 6 and Stoughton is part of District 5. This bottleneck parallels Location 3 in the southbound direction.


### 7.1 EXISTING FREEWAY CHARACTERISTICS

Operations at this bottleneck are associated with the freeway components described below.

### 7.1.1 Major Diverge Areas

A major diverge occurs when a basic freeway segment with three or more lanes splits into two multilane primary freeway segments. The off-ramps leading to Route 24 southbound are two-lane ramps splitting from a four-lane freeway, qualifying them as major diverge areas. Both geometries use a center lane that splits into two at the diverge, and both ramps have a speed limit of 50 mph . However, the ramp from l-93 southbound is a left-hand side diverge while the northbound ramp is a right-hand side diverge. Demand for these ramps is highest during the PM peak, with up to 2,700 vehicles per hour using the ramp from I-93 northbound and up to 2,600 vehicles per hour using the ramp from I-93 southbound.

### 7.1.2 Major Merge Area

The two Route 24 southbound ramps meet at a major merge area. The configuration at this location has two two-lane ramps merging to become the

[^20]three-lane Route 24 southbound barrel. Lane balance is achieved by combining the two center lanes. This junction serves 6,200 vehicles per hour during the PM peak period.

### 7.1.3 Basic Freeway Section

Route 24 southbound is a freeway segment with three 12 -foot travel lanes, a 12to 13 -foot right shoulder, and a two- to three-foot left shoulder. The posted speed limit is 65 mph on the Route 24 southbound mainline. Rumble strips are present on the right side of the southern barrel.

### 7.2 PROBLEMS

The existing bottleneck creates intense interruption of traffic flow during the PM peak travel period. During these hours, travel speeds are reduced and queues back up on both ramps leading to Route 24 southbound. These waiting drivers can spill onto both branches of I-93 and interfere with through traffic. In addition, the bottleneck likely contributes to crashes in this area.

### 7.3 CAUSES

MPO staff identified two primary factors contributing to this bottleneck:

- A generally high volume of traffic using I-93 Exit 4 to Route 24 during the PM peak period
- Suboptimal merge geometry at the start of Route 24 southbound


### 7.3.1 High Volume of Traffic

Figure 22 shows the hourly traffic flow during the PM peak periods. Usage of both the l-93 ramps is very high in the evening hours as traffic flows south out of Boston. The merging and diverging maneuvers of these vehicles interrupt traffic flow and reduce capacity, resulting in a traffic bottleneck.

### 7.3.2 Geometry at the Major Merge

The geometry where the ramps from I-93 merge is problematic for two reasons. First, the merge distance is very short. The 48 -foot width present where the four ramp lanes meet begins to narrow and merge into three lanes immediately after the end of the painted gore nose. Drivers using the two center lanes are forced to make merge decisions quickly as they negotiate for space with drivers in the opposite lane. This effect is amplified by the high-posted speed ( 50 mph ) present on the ramps. The result is sudden merge maneuvers that lead to braking, reduced speeds, and unsafe conditions.

Second, the practice of merging the two center lanes at a major merge is not recommended. Unlike with a left- or right-hand side merge where vehicles in the
merging lane must yield to through traffic, with a center merge neither movement has a clear right of way. Communication errors can lead to angle crashes when a driver refuses to yield and rear-end crashes when a driver yields unexpectedly. Where a lane drop at a major merge is necessary, the current MassDOT design guide recommends instead continuing all travel lanes for at least 1,000 feet and then merging the rightmost lane into the main barrel.

## $7.4 \quad$ IMPACTS

### 7.4.1 Crashes

A summary of the crashes in this segment is presented in Table 12. There were 238 crashes in this area between 2010 and 2014 (Appendix C). Figure 23 shows the location of these crashes. Crashes were very high at all three locations studied, with both I-93 exits registering almost 100 crashes each.

TABLE 12.
Crash Summary (2010-14):
Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139)

|  | Number of Crashes |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Rte. 24 <br> SB at <br> I-93 NB | I-93 SB <br> Exit 4 to <br> Exit 4 to |  |  |
| Crash Variable |  |  |  |  |
| Crash severity | 0 | 0 | 0 | 0 |
| Fatal injury | 14 | 25 | 25 | 64 |
| Non-fatal injury | 42 | 61 | 65 | 168 |
| Property damage only | 2 | 2 | 2 | 6 |
| Not reported |  |  |  |  |
| Manner of collision | 20 | 58 | 51 | 129 |
| Rear-end | 9 | 10 | 16 | 35 |
| Sideswipe, same direction | 23 | 14 | 19 | 56 |
| Single-vehicle crash | 5 | 4 | 4 | 13 |
| Angle | 0 | 1 | 1 | 2 |
| Head-on | 1 | 1 | 1 | 3 |
| Not reported |  |  |  |  |
| Road surface conditions | 0 | 1 | 0 | 1 |
| Snow | 13 | 13 | 26 | 52 |
| Wet | 45 | 74 | 64 | 183 |
| Dry | 0 | 0 | 2 | 2 |
| Not reported |  |  |  |  |
| Ambient light conditions | 0 | 0 | 3 | 3 |
| Dawn |  |  |  |  |


| Daylight | 31 | 50 | 58 | 139 |
| :--- | :---: | :---: | :---: | :---: |
| Dusk | 1 | 2 | 2 | 5 |
| Dark: lighted roadway | 18 | 27 | 20 | 65 |
| Dark: roadway not lighted | 7 | 9 | 8 | 24 |
| Dark: unknown lighting | 1 | 0 | 0 | 1 |
| Not reported | 0 | 0 | 1 | 1 |
| Weather conditions |  |  |  |  |
| Clear | 33 | 51 | 55 | 139 |
| Cloudy | 5 | 7 | 15 | 27 |
| Rain | 10 | 9 | 14 | 33 |
| Snow | 0 | 1 | 0 | 1 |
| Not reported | 10 | 20 | 8 | 38 |
| Travel period |  |  |  |  |
| Peak | 22 | 58 | 52 | 132 |
| Off-peak | 36 | 30 | 40 | 106 |
| Total crashes | 58 | 88 | 92 | 238 |
| Five-year average (rounded) | 12 | 18 | 18 | 48 |
| NB $=$ northbound; SB = southbound |  |  |  |  |

Below is a summary of the crashes in this segment:

- 27 percent of the crashes resulted in injury, including one fatal injury
- 54 percent of the crashes were rear end collisions, the largest share among collision types
- 55 percent of the crashes occurred during the peak travel period
- 38 percent of the crashes occurred outside daylight conditions
- 77 percent of the crashes occurred under dry roadway conditions


### 7.4.2 Travel Speed

Figure 24 is a congestion scan that shows the average travel speeds on Route 24 southbound at the bottleneck location. Congestion at this location reduces travel speeds near the merge to less than 50 mph between the hours of 4 PM and 5 PM. These vehicle speeds correspond to LOS E conditions. Congestion begins to dissipate rapidly once the merge is passed and is almost entirely cleared two miles south of the l-93 interchange.

Figure 17 and Figure 18 contain congestion scans for I-93 northbound and I-93 southbound respectively. These figures demonstrate that the evening traffic peak lasts much longer than the morning peak, as congestion is present near Route 24 on I-93 northbound and southbound between 4 PM and 7 PM. In both directions, travel speeds are decreased to less than 35 mph for three hours at a
time. However, traffic on I-93 begins to clear once Route 24 is passed and travel speeds rapidly return to free-flow speed, especially in the southbound direction.

### 7.4.3 Level of Service

MPO staff conducted traffic operations analyses consistent with HCM methodologies. Using the MassDOT data, MPO staff built traffic analysis networks for the PM peak hours with the HCS suite to assess the capacity and quality of traffic flow at the bottleneck area. ${ }^{30}$ Full HCS reports are included in Appendix D.

As mentioned in the previous chapter, the HCM is unable to model performance effectively for major merge or diverge areas. LOS can be approximated by checking capacities of each component segment as basic freeway segments. Using a basic freeway segment ignores merging maneuvers and distributes traffic evenly across all lanes, leading to an overstated capacity for these facilities. The results of the analysis are shown in Table 13.
$\left.\begin{array}{lllll} & \begin{array}{c}\text { TABLE } 13 .\end{array} \\ \text { LOS Analysis-Existing Conditions: }\end{array}\right]$

Table 13 shows LOS D for the merge segment, although as mentioned above this is an approximation. Speed data and field observations show much slower speeds indicative of LOS E or LOS F.

Unlike in Location 3, ramp roadway capacity is not a limiting factor at Route 24 southbound. Both of the ramps at this bottleneck location use a two-lane design that has a theoretical capacity of 4,400 vehicles per hour. ${ }^{31}$ This means that the

[^21]capacity of the ramp roadway facilities at Location 4 is well above the demand flow rate and does not become a limiting factor in system performance.

### 7.5 IMPROVEMENT ALTERNATIVE

MPO staff identified a low-cost improvement to address safety and operational issues at the bottleneck:

- Alternative 1: Lengthen the merge distance at the ramp junction (Figure 25).

The alternative was analyzed using projected year 2030 traffic volumes. MPO staff estimated a five percent total background growth from 2015 to 2030.

### 7.5.1 Alternative 1: Lengthen the Merge Distance at the Ramp J unction

The 48-foot width present where the ramps intersect begins to narrow almost immediately after the painted gore nose. The freeway becomes a 36 -foot, threelane segment within approximately 400 feet. MPO staff recommends bringing this merge in line with the MassDOT standards by extending the four lanes present on the ramps for approximately 1,000 feet down Route 24 and by using a righthand lane drop.

Figure 25 shows the improvements recommended in Alternative 1:

- Use the existing right-hand paved shoulder to add a fourth travel lane beginning at the merge and continuing 1,000 feet downstream. Continue the existing four ramp lanes down this stretch, and reduce the right shoulder width to two feet.
- Restripe the merge area with wide-dotted lines and add new signage after 500 feet to alert the travelers in the right-hand lane to merge left.
- Begin a 500-foot taper that drops the rightmost lane after 1,000 feet, leaving three southbound lanes.


### 7.6 EFFECTIVENESS AND COST OF THE IMPROVEMENT

Table 14 presents the 2030 future LOS analysis compiled using the HCS software. Results for the no-build scenario are compared against Alternative 1. Both scenarios use a uniform five percent growth for 2030 traffic volumes.

TABLE 14.
LOS Analysis-Improvement Alternatives:
Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139)

| Location | Scenario | Density (pc/lane mile) | Speed (mph) | VIC Ratio | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| HCM Analysis Type: Basic Freeway Segment |  |  |  |  |  |
| Route 24 southbound at | No-Build | 30.7 | 60.6 | 0.80 | D |
| merge | Alt 1 | 22.7 | 61.5 | 0.60 | C |

HCM = Highway Capacity Manual; LOS = level of service; mph = miles per hour; pc/lane mile = passenger cars per lane mile; V/C = volume-to-capacity

### 7.6.1 Effectiveness and Cost of Alternative 1

Using CMFs from the CMF Clearinghouse for installing an additional lane for an urban freeway shows that Alternative 3 would reduce crashes at the merge area by up to 20 percent. In addition, Table 14 compares an analysis of a three-lane basic freeway segment at the merge with a four-lane basic freeway segment. The additional lane improves LOS by one level over the no-build scenario, from LOS D to LOS C in the PM peak.

The basic freeway segment analysis can be misleading because the real cause of the bottleneck is merging maneuvers of vehicles and not the base capacity of the freeway. However, the HCM model does show that adding the lane increases capacity significantly. This increased capacity will help mitigate the capacity reduction resulting from merge maneuvers. Changing the center merge to an exterior merge will also improve safety and bring the geometry at the interchange in line with MassDOT standards.

Alternative 1 is estimated to cost between $\$ 100,000$ and $\$ 200,000$ to construct. This estimate includes preparing the shoulder for travel lane, restriping travel lanes, relocation and installation of signs, and minor pavement markings. New paving may be required if an emergency pullover area is found to be necessary.

### 7.7 RECOMMENDATIONS

MPO staff recommends implementation of Alternative 1 to improve operational efficiency and safety for all traffic headed to Route 24 southbound.

## Chapter 8-Conclusion and Next Steps

MPO staff, working in conjunction with the MassDOT Highway staff, identified, developed, and evaluated improvements for four bottleneck locations in the MPO region. The study provides the MassDOT Highway Division with an opportunity to begin identifying the needs at the four bottleneck locations and to start planning design and engineering efforts. If implemented, these low-cost, short-term improvements would increase traffic safety, make traffic operations more efficient, and reduce congestion at the bottlenecks. The study aligns with the MPO goals of managing capacity and improving mobility, and increasing safety on the region's highway system.


## BOSTON REGION MPO

Figure 1
Regional Map of Study Areas


Location 1: I-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza):



| BOSTON <br> REGION <br> MPO | Location 1: l-95 Northbound Segment between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza): |
| :--- | :--- | :--- |
| Congestion Scan |  |







| BOSTON REGION MPO | Figure 9 <br> Location 2: I-93 Southbound Segment between Exit 37C (Commerce Way) and Exit 37B (I-95): <br> Congestion Scan | Low-Cost Improvements to Express-Highway Bottleneck Locations |
| :---: | :---: | :---: |



| BOSTON REGION MPO | ${ }^{N}$ | Figure 10 <br> Location 2: I-95 Southbound Segment between Exit 38 (Route 28) and Lowell MBTA Line: Congestion Scan | Low-Cost Improvements to Express-Highway Bottleneck Locations |
| :---: | :---: | :---: | :---: |








| $\begin{aligned} & \text { BOSTON } \\ & \text { REGION } \\ & \text { MPO } \end{aligned}$ | z | Figure 16 <br> Location 3: Route 24 Northbound Segment between Exit 20 (Route 139) and Exit 21 (I-93): Congestion Scan | Low-Cost Improvements to Express-Highway Bottleneck Locations |
| :---: | :---: | :---: | :---: |



| BOSTON <br> REGION <br> MPO | Figure 17 <br> N | Low-Cost Improvements <br> to Express-Highway <br> Bottleneck Locations |
| :--- | :--- | :--- |



| BOSTON REGION MPO | $\wedge_{\mathbf{N}}$ | Figure 18 <br> Location 3: I-93 Southbound Segment between Exit 5 (Route 28) and Exit 2 (Route 138): Congestion Scan | Low-Cost Improvements to Express-Highway Bottleneck Locations |
| :---: | :---: | :---: | :---: |



$\square$





Figure 2
Location 4: Route 24 Southbound Segment between Exit 21 (I-93) and Exit 20 (Route 139):
Low-Cost Improvements to Express-Highway
Congestion Scan Bottleneck Locations

$<z$

## Appendixes

Appendix A: Review Comments and Selection Process
Appendix B: ATR and Classification Data
Appendix C: Crash Tables
Appendix D: HCS Printouts

## APPENDIX A

1. Review Comments
2. Selection Process
3. Review Comments

## Seth Asante

| From: | Raphael, Connie (DOT) |
| :--- | :--- |
| Sent: | Wednesday, November 29, 2017 3:45 PM |
| To: | Seth Asante |
| Cc: | Chen-Yuan Wang; Suszynski, Frank (DOT) |
| Subject: | FW: Low-Cost Improvements to Express-Highway Bottleneck Locations Study |

Hi Seth,
Here are some comments on this study from Brian Fallon, our Projects Engineer.
Below the comments I have sent an excerpt from our weekly report with a blurb on the I-95 NB to Route 3 NB exit work and a picture. Thought you would like to know how well your recommendations are working!

Location 1 - Lexington Auxiliary Lane from Route 2 on ramp to the Service area CD road
An auxiliary Lane in this area would improve the traffic flow.
The existing right shoulder in this area is approximately 10 feet wide.
There are stormwater improvement structures behind the guardrail just south of the Lincoln Street Bridge.
If the 12 foot auxiliary lane and 2 foot right shoulder (assumed cross section) are proposed, then the left shoulder would need to be reduced to avoid widening.

If the left shoulder reduction is proposed, then a highway alignment shift would be required.
If widening is proposed, there would be impacts to the stormwater structure (underground chambers) and possibly wetland impacts. The cost of the work would be higher.

Location 2 - Reading \& Woburn Auxiliary Lane from Commerce Way on ramp to the 195 Southbound On Ramp
An auxiliary Lane on 193 would improve the traffic flow.
The existing right shoulder in this area is approximately 12 feet wide.
If the 12 foot auxiliary lane and 2 foot right shoulder (assumed cross section) are proposed, then a minor one to two foot widening would be required for the majority of the auxiliary lane.

A reduced auxiliary lane would need to be proposed on the 193 over West Street Bridge.

## Location 2 -Woburn Extending the 195 Acceleration Iane from Commerce Way

A lengthened Acceleration Lane in this area would improve the traffic flow.
The existing right shoulder in this area is approximately 10 feet wide.
If the 12 foot auxiliary lane and 2 foot right shoulder (assumed cross section) are proposed, then the left shoulder would need to be reduced to avoid widening.

If the left shoulder reduction is proposed, then a highway alignment shift would be required.
If widening is proposed, there would be construction impacts due to the steep highway side slopes and possibly wetland impacts. The cost of the work would be higher.

Lexington/Burlington - Route I-95 resurfacing - as part of an Interstate Maintenance resurfacing contract covering this section of I-95, several of the ramps at the I-95/Route 3/Middlesex Turnpike interchange were widened to improve operations. The improvements were based on the results of a past CTPS study that evaluated regional bottleneck locations. Since the work was completed in mid-October, there has been a noticeable improvement in traffic operations and a significant reduction in vehicle queueing, particularly during the weekday afternoon peak period. The photo below shows the newly widened ramp on Route I-95 NB providing two formal exit lanes to Route 3 NB.


[^22]| From: | Lipton, Amitai (DOT) |
| :--- | :--- |
| Sent: | Thursday, December 7, 2017 10:19 AM |
| To: | Seth Asante |
| Cc: | Mark Abbott; Kulen, Raj (DOT); Patel, Hasmukh (DOT); Vatan, Geraldine (DOT); Polin, |
|  | Bonnie (DOT); Belanger, David (DOT) |
| Subject: | RE: Low-Cost Improvements to Express-Highway Bottleneck Locations Study |

Good morning Seth,
District 6 Traffic section would like to add a few comments:

- Consider evaluating the relative safety effects of the recommended alternatives, compared with the existing conditions.
- Section 1.2 - The term "subtract-a-lane" was only used internally.
- Section 2.2 (Location 3) \& Chapter 6 - Route 24 NB queue length is described inconsistently. It sometimes backs up as far as Brockton, well beyond Route 139. For some reason, the heaviest volumes on Route 24 NB are often found earlier in the morning than other locations along the 128 corridor, with queues forming as early as 5 AM and dissipating by 9 AM .
- Section 6.5.1 (3rd bullet) and 6.5.2 (4th bullet) - Replace term "distinct dash pattern" with "wide dotted line" per current MUTCD requirements. Also, please note that on recent projects, these pavement markings have started $1 / 2$ mile upstream of a split, rather than 3000 feet as described in the text and Figure 20, and 600 feet as described in Figure 19.
- Section 6.5.3-(Typo) Figure 21 shows the recommendations in Alternative 3, rather than Alternative 2.
- Section 6.6.3 - Alternative 3 costs should be roughly equivalent to Alternative 1 , since all existing rumble strips and pavement markings would need to be removed and replaced over similar distances.
- Section 7.5.1 (2nd bullet) - Replace term "distinct striping pattern" with "appropriate MUTCD-compliant pavement markings", since current requirements disallow use of a distinct striping pattern for this application. Revises Figures 21 and 25 for consistency (note that we've recently been using three arrows spaced at 120 feet to indicate a mainline lane reduction).
- Figure 14 - Some volumes on Route 24 ramps to I-93 NB and SB are inconsistent with those described in Chapter 6. Also, the volumes on Route 24 mainline do not equal the sum of the volumes on the ramps to I-93.
- Figures 17 \& 18 - Would it be possible to reverse the direction of these figures? E.g. on Figure 17, I-93 NB is actually heading easterly, so it might be more intuitive to have the direction of travel be from left-to-right.

Thank you,
Amitai

From: Vatan, Geraldine (DOT)
Sent: Thursday, December 7, 2017 08:19
To: Seth Asante

Cc: Mark Abbott; Boudreau, Neil (DOT); Danila, James (DOT); Raphael, Connie (DOT); Gregg, John (DOT); Timoner, Sara (DOT); Kulen, Raj (DOT); Lipton, Amitai (DOT); Patel, Hasmukh (DOT); Clark, Michael (DOT); Pounds, Bryan (DOT); Gascon, Cassandra (DOT); Paul, Andrew (DOT)
Subject: RE: Low-Cost Improvements to Express-Highway Bottleneck Locations Study

Hello Seth,
Thank you for this report. I have a few comments:

- In chapters 4-7 MassDOT 'Districts' are referred to as 'Divisions', please correct
- Section 6.7 Recommendations - Alternatives 1 \& 2 are recommended, my understanding is that Alt 1 is contained within Alt2, should this be Alternatives $1 \& 3$ ?

Thanks,
Geri

Geraldine Vatan | District 6 Project Development Engineer
185 Kneeland Street Boston, MA 02111 | Office (857) 368-6115 | Cell (508) 330-1078
MassDOT Highway Division geraldine.vatan@dot.state.ma.us

From: Seth Asante [mailto:sasante@ctps.orq]
Sent: Monday, November 20, 2017 3:20 PM
To: Boudreau, Neil (DOT); Danila, James (DOT); Raphael, Connie (DOT); Gregg, John (DOT); Timoner, Sara (DOT);
Vatan, Geraldine (DOT); Kulen, Raj (DOT); Lipton, Amitai (DOT); Patel, Hasmukh (DOT); Clark, Michael (DOT); Pounds, Bryan (DOT); Gascon, Cassandra (DOT); Paul, Andrew (DOT)
Cc: Mark Abbott
Subject: Low-Cost Improvements to Express-Highway Bottleneck Locations Study

Good afternoon,
The attached report—Low-Cost Improvements to Express-Highway Bottleneck Locations is available for review.

MPO staff analyzed four bottleneck locations in the study:

- Location 1: Interstate-95 northbound between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) in Lexington
- Location 2: Interstate-93 southbound between Exit 37C (Commerce Way) and Exit 37B (I-95) in Woburn and Reading
- Location 3: Route 24 northbound between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton
- Location 4: Route 24 southbound between Exit 21 (I-93) and Exit 20 (Route 139) in Randolph, Canton, and Stoughton

The study results for Locations 1 and 2, which are in MassDOT Highway District 4, are presented in Chapters 4 and 5 of the report. The study results for Locations 3 and 4, which are in MassDOT Highway District 6, are presented in Chapters 6 and 7 of the report.

Please review the attached report and provide me with comments by December 7, 2017.

| From: | Vatan, Geraldine (DOT) |
| :--- | :--- |
| Sent: | Thursday, December 7, 2017 8:19 AM |
| To: | Seth Asante |
| Cc: | Mark Abbott; Boudreau, Neil (DOT); Danila, James (DOT); Raphael, Connie (DOT); |
|  | Gregg, John (DOT); Timoner, Sara (DOT); Kulen, Raj (DOT); Lipton, Amitai (DOT); Patel, |
|  | Hasmukh (DOT); Clark, Michael (DOT); Pounds, Bryan (DOT); Gascon, Cassandra (DOT); |
|  | Paul, Andrew (DOT) |
| Subject: | RE: Low-Cost Improvements to Express-Highway Bottleneck Locations Study |

Hello Seth,
Thank you for this report. I have a few comments:

- In chapters 4-7 MassDOT 'Districts' are referred to as 'Divisions', please correct
- Section 6.7 Recommendations - Alternatives $1 \& 2$ are recommended, my understanding is that Alt 1 is contained within Alt2, should this be Alternatives $1 \& 3$ ?

Thanks,
Geri

Geraldine Vatan | District 6 Project Development Engineer
185 Kneeland Street Boston, MA 02111 | Office (857) 368-6115 | Cell (508) 330-1078
MassDOT Highway Division geraldine.vatan@dot.state.ma.us

From: Seth Asante [mailto:sasante@ctps.org]
Sent: Monday, November 20, 2017 3:20 PM
To: Boudreau, Neil (DOT); Danila, James (DOT); Raphael, Connie (DOT); Gregg, John (DOT); Timoner, Sara (DOT); Vatan, Geraldine (DOT); Kulen, Raj (DOT); Lipton, Amitai (DOT); Patel, Hasmukh (DOT); Clark, Michael (DOT); Pounds, Bryan (DOT); Gascon, Cassandra (DOT); Paul, Andrew (DOT)
Cc: Mark Abbott
Subject: Low-Cost Improvements to Express-Highway Bottleneck Locations Study

Good afternoon,
The attached report—Low-Cost Improvements to Express-Highway Bottleneck Locations is available for review.

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- Location 3: Route 24 northbound between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton

$$
A-6
$$

- Location 4: Route 24 southbound between Exit 21 (I-93) and Exit 20 (Route 139) in Randolph, Canton, and Stoughton

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Please review the attached report and provide me with comments by December 7, 2017.
Thank you,
Seth

## Seth Asante

From:
Gascon, Cassandra (DOT)
Sent:
Monday, December 4, 2017 12:59 PM
To:
Seth Asante
Subject:
RE: Low-Cost Improvements to Express-Highway Bottleneck Locations Study

Hi Seth,
Please see below OTP's comments on the Bottleneck Study:

- p. 12 - "would result in..." should be more along the lines of "expected to result in..."
- 1.2, Background, is written kind of sloppily on p. 12.
o So is 2.1, Screening Criteria, on p. 15—consider a bit of revision to both parts
- Consider taking the time to note what is included or not included in the projected costs. We are assuming they don't include ROW acquisition but this is not made clear. This would provide clarity for some of the cost estimates, particularly how Alt. 3 for Location 1 (signage improvements) is projected to cost more than the other two
- Alt. 3 for Location 2 - Even though the alternatives are measured against 2030 model conditions, to expect LOS on the I-93 SB to I-95 SB off-ramp to go from F to A as a result of adding a second lane is ignoring induced demand and seems very unrealistic. It should be acknowledged that induced demand may result in 2030 conditions not meeting the expectations set by the model, even if a more nuanced projection can't be made.
- p. 41 - the long-term improvement at the I-93/I-95 interchange seems like it could be important to this study but is only acknowledged as a footnote. This should be brought into the body of the report and discussed in context of the proposed alternatives

And a few typos we noticed:

- p. 4 last paragraph, third line, should read "location" not "locations"
- p. 16 - "the" PM peak period
- p. 19 - don't start sentence with an acronym
- Some labels from Figure 11 carry over to Figure 12
- p. $38-$ " $\mathrm{I}-93$ " is termed as " $1-93$ "
- p. 41 third to last line- should read "affect" not "affects"

Lastly, as CTPS moves forward with other studies, we have a suggestion for the formatting/organization of the report. It's really tricky to flip back and forth between the text and the graphics/figures at the end of the study. We recommend integrating most, if not all, of graphics and figures into the report text itself to make it simpler to read and understand.

We hope this is helpful to your editing efforts. If you have questions on these, give me or Michael Clark (he made most of these comments) a call.

Thanks,
Cassandra
Cassandra Gascon

From: Seth Asante [mailto:sasante@ctps.org]
Sent: Monday, November 20, 2017 3:20 PM
To: Boudreau, Neil (DOT); Danila, James (DOT); Raphael, Connie (DOT); Gregg, John (DOT); Timoner, Sara (DOT); Vatan, Geraldine (DOT); Kulen, Raj (DOT); Lipton, Amitai (DOT); Patel, Hasmukh (DOT); Clark, Michael (DOT); Pounds, Bryan (DOT); Gascon, Cassandra (DOT); Paul, Andrew (DOT)
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The study results for Locations 1 and 2, which are in MassDOT Highway District 4, are presented in Chapters 4 and 5 of the report. The study results for Locations 3 and 4, which are in MassDOT Highway District 6, are presented in Chapters 6 and 7 of the report.

Please review the attached report and provide me with comments by December 7, 2017.
Thank you,
Seth

## 2. Selection Process

# TECHNICAL MEMORANDUM 

DATE: March 30, 2017
TO: Boston Region Metropolitan Planning Organization (MPO)
FROM: Seth Asante, MPO Staff
RE: Low-Cost Improvements to Express-Highway Bottleneck Locations Selection of Study Locations

## 1 BACKGROUND

This memorandum presents the results of Task 2—screen bottleneck locations and select locations for analysis-of the work program for Low-Cost Improvements to Express-Highway Bottleneck Locations: federal fiscal year (FFY) 2017. ${ }^{1}$ In Task 2, MPO staff indicated that we will present the results to the MPO for discussion.

According to the Federal Highway Administration (FHWA), "Much of recurring congestion is due to physical bottlenecks-potentially correctible points on the highway system where traffic flow is restricted. While many of the nation's bottlenecks can only be addressed through costly major construction projects, there is a significant opportunity for the application of operational and low-cost infrastructure solutions to bring about relief at these chokepoints." ${ }^{2}$

In the past, MPO staff analyzed several express-highway bottleneck locations in three studies, which were very well received by the Massachusetts Department of Transportation (MassDOT) and FHWA. ${ }^{3,4,5}$ Previous study locations included

[^23]sections of I-95 in Burlington, Lexington, and Weston; sections of I-93 in Woburn; and sections of Route 3 in Braintree. Some of the recommendations from those studies have been executed, such as the I-95 northbound and southbound subtract-a-lane at Interchange 24 in Weston; I-95/Route 3/Middlesex Turnpike Interchange in Lexington and Burlington; and FHWA has interviewed MPO staff about these successful implementations.

The cause and duration of highway bottlenecks vary. In general, recurring bottlenecks, the subject of this work program, are influenced by the design or operation present at the point where the bottleneck begins, for example: merges, diverges, lane drops, traffic weaving, abrupt changes in highway alignment, lowclearance structures, lane narrowing, intended disruption of traffic for management purposes, and less-than-optimal express-highway design.

This memorandum presents the process used to select the bottleneck study locations. MPO staff will submit this proposal to the MPO for discussion and approval.

## 2 SELECTION OF STUDY LOCATIONS

Selection of study locations was a two-stage process that comprised inventorying and screening candidate locations.

### 2.1 Inventorying Candidate Locations

MPO staff developed an initial list of candidate locations in the MPO region based on the following parameters:

- Consultations with MassDOT Highway Division
- Staff knowledge of bottleneck locations in the Boston MPO region
- Review of congestion management process (CMP) monitoring data, and recent MPO and other planning studies
The inventory process yielded 14 bottleneck locations for screening, which are presented in the following table. Nine of the locations are in the Boston Region MPO area and five are located in the Merrimack Valley Planning Commission (MVPC).

Inventory of Express-Highway Bottleneck Locations for Screening

| Location Number | City / Town | MPO Region | MassDOT District | Express-Highway Section | Problem |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Lexington* | Boston | 4 | I-95 northbound between Exit 29 (Rte 2) | Merge/ diverge |
|  |  | Region |  | and Exit 30 (Rte 2A/ Service Plaza) |  |
|  | Woburn/ Reading* | Boston |  | $\mathrm{I}-93$ southbound between Commerce |  |
| 2 |  | Region | 4 | Way and I-95 | Merge/ diverge |
| 3 | Randolph/ Canton | Boston | 6 | Rte 24 northbound between Exit 20 (Rte |  |
|  |  | Region |  | 139) and Exit 21 (I-93) | Merge/ diverge |
| 4 | Randolph/ Canton* | Boston Region | 6 | Rte 24 southbound between Exit 20 (Rte 139) and Exit 21 (I-93) | Merge/ diverge |
| 5 | Medford | Boston | 4 | I-93 southbound between Rte 16 on- | Weave |
|  |  | Region |  | ramp and Exit 31 (Rte 16 off-ramp) |  |
|  |  | Boston |  | I-93 northbound between Exit 40 (Rte |  |
| 6 | Wilmington | Region | 4 | 62) and Exit 41 (Rte 125) | Merge/ diverge Merge/ diverge/ |
|  |  | Boston |  | I-93 northbound between Exit 1 (I-95) |  |
| 7 | Canton / Randolph | Region | 6 | and Exit 4 (Rte 24) | Merge/ diverge/ weave |
|  |  | Boston |  | I-93 southbound between Exit 1 (I-95) and Exit 4 (Rte 24) <br> I-95 northbound between Exit 37 (I-93) |  |
| 8 | Canton / Randolph | Region | 6 |  |  |
|  |  | Boston |  |  |  |
| 9 | Reading | Region | 4 | and Exit 38 (Rte 28) | Weave |
|  |  |  |  | I-495 northbound between Exit 41 (Rte |  |
| 10 | Andover/ Lawrence | MVPC | 4 | 28) and Exit 42 (Route 114) | Merge/ diverge |
|  |  |  |  | I-495 northbound between Exit 42 (Rte 114) and Exit 43 (Massachusetts |  |
| 11 | North Andover/ Lawrence | MVPC | 4 | Avenue) | Merge/ diverge |
|  |  |  |  | I-495 southbound between Exit 42 (Rte |  |
| 12 | North Andover/ Lawrence | MVPC | 4 | $114)$ and Exit 43 (Massachusetts Ave) | Merge/ diverge Acceleration/ deceleration lane lengths Acceleration/ deceleration lane lengths |
|  |  |  |  |  |  |
| 13 | Methuen | MVPC | 4 | I-495 northbound Exit 47 (Rte 213) |  |
|  |  |  |  |  |  |
| 14 | Methuen | MVPC | 4 | I-495 southbound Exit 47 (Rte 213) |  |

Source: Central Transportation Planning Staff.
MVPC = Merrimack Valley Planning Commission
Note: Asterisks and bolding denote locations selected for analysis.

### 2.2 Screening Candidate Locations

MPO staff selected four bottleneck locations for analysis in FFY 2017 (the first four locations cited in the table above). After consulting with the MassDOT Highway Division, staff determined that these four locations likely could be corrected with low-cost mitigation strategies. The other bottlenecks in the Boston Region MPO area also could be corrected in a low-cost manner, but were not selected because of funding resources-these locations would be considered in future bottleneck studies. However, location 9 in the table above likely could not be correctible in a low-cost manner.

MPO staff used the following criteria to screen the bottleneck locations:

- Does the location qualify as a bottleneck? A long traffic queue upstream trailing free-flowing traffic downstream usually characterizes the location as a bottleneck. In addition, the upstream congestion must be recurringin other words, the location experiences routine and predictable congestion because traffic volume exceeds the available capacity at that location.
- Is a physical design constraint or operational conflict that is inherent in the location the cause of the bottleneck? Examples of these are:
o Lane drop-one or more travel lanes are lost, requiring traffic to merge
o Weaving area-drivers must merge across one or more lanes in order to access an entry or exit ramp
o Merge area-on-ramp traffic merges with mainline traffic in order to enter the freeway
o Major interchanges-high-volume traffic is directed from one freeway to another
o Horizontal curves-abrupt changes in highway alignment force drivers to slow down because of safety concerns
- Can the bottleneck be fixed with low-cost operational and geometric improvements? These would exclude costly long-term solutions such as expansion and major transit investments that alter drivers' mode choice. Examples of low-cost operational and geometric improvements are:
o Using a short section of shoulder as an additional travel lane, an auxiliary lane, or for lengthening an acceleration or deceleration lane
o Restriping merge and diverge areas to better serve traffic demand
o Providing better traveler information to allow drivers to respond to temporary changes in lane assignment, such as using a shoulder as an additional travel lane during peak periods
o Providing all-purpose reversible lanes
o Changing or adding signs and striping

Based on the screening criteria and consultations with MassDOT Highway Division officials, MPO staff selected locations 1, 2, 3 and 4 for study. Below is staff's rationale for not selecting locations 9 through 14:

## Location 9: I-95 Northbound between Exit 37 (I-93) and Exit 38 (Route 28) in Reading

This section of highway frequently is congested because of a lane drop, intensive weaving, and merging and diverging activities, especially during the PM peak period, which slows down mainline traffic. During that time, The I-95 northbound
mainline carries about 6,000 vehicles per hour, the Exit 37 off-ramps carry about 3,000 vehicles per hour, and the Exit 37 on-ramps carry about 2,600 vehicles per hour. Adding an auxiliary lane northbound on I-95 would provide more room for the merging and diverging activities and reduce disturbance to mainline traffic. Staff did not select this location because the weave problem at Exit 37 could not be corrected in low-cost manner and an auxiliary lane would need to be extended for a long distance (about three-to-four interchanges downstream) to reduce congestion and queue, which could be expensive.

## Locations 10, 11, 12, 13, and 14

These bottleneck locations are in the MVPC area; they were not screened or considered in the selection process because they are not in the Boston Region MPO area.

## 3 SELECTED BOTTLENECK LOCATIONS FOR STUDY

Location 1: I-95 Northbound between Exit 29 (Route 2) and Exit 30 (Route 2A/Service Plaza) in Lexington
This section of highway, about 0.75 miles long, frequently is congested because of merging and diverging activities, especially during the PM peak period. The northbound on- and off-ramps connect to and from Route 2 (Concord Turnpike), Route 2A (Merrett Road), and the service plaza. During peak periods, I-95 northbound carries about 6,100 vehicles per hour; the on-ramp from Route 2 westbound carries about 1,000 vehicles per hour; and about 600 vehicles per hour exit to Route 2A at Exit 30 and the service plaza. The merging and diverging activities of these vehicles slow down I-95 northbound mainline traffic upstream of the Route 2A interchange, which makes it difficult to enter l-95 northbound for the Route 2 traffic.

## Location 2: I-93 Southbound between Commerce Way and I-95 in Woburn and Reading

This bottleneck is located on I-93 southbound in the section where traffic diverges onto I-95 southbound. During the AM peak period, traffic going to I-95 southbound backs up that ramp onto l-93 mainline traffic, thus impacting flow on the rightmost low-speed southbound lane. As a result, motorists attempt to get into the breakdown lane as soon as possible to stay clear of the low-speed lane, but usually vehicles are still queuing on the low-speed lane. The other three southbound lanes are almost in free flow conditions (that is, uncongested conditions with drivers traveling at posted speeds) during this period. In the segment, the four I-93 southbound lanes carry between 6,500 and 7,000 vehicles per hour of which about 2,000 vehicles exit to l-95 southbound.

## Location 3: Route 24 Northbound between Exit 20 (Route 139) and Exit 21 (I-93) in Randolph, Canton, and Stoughton

This bottleneck is located on Route 24 northbound at the point where traffic diverges onto l-93 northbound and southbound during AM peak periods. The impact of the bottleneck extends from l-93 in Randolph to Route 139 in Stoughton, about two miles long. During this period, Route 24 northbound carries about 6,000 vehicles per hour, of which 2,500 vehicles exit to I-93 southbound and 3,500 to I-93 northbound. The merging activity of these vehicles on I-93 slows down traffic on the Route 24 connector ramps and backs up traffic on Route 24.

## Location 4: Route 24 Southbound between Exit 20 (Route 139) and Exit 21 (l-93) in Randolph, Canton, and Stoughton

This bottleneck is located on Route 24 southbound at the point where traffic from the I-93 connector ramps merge onto Route 24 southbound during PM peak periods. The merging activity of these vehicles creates a bottleneck that causes a traffic queue to extend from the Canton Street Bridge under Route 24 onto the I93 northbound and southbound lanes, creating a bottleneck about a mile long. During this period, Route 24 southbound carries about 6,000 vehicles per hour of which about 3,000 vehicles enter from I-93 southbound and another 3,000 from I93 northbound.

## 4 SUMMARY

By identifying and evaluating a comprehensive list of potential improvements at the four locations, MPO staff will rely on their technical expertise and judgment regarding the nature of bottlenecks. MPO staff will seek input from MassDOT Highway Division staff that are familiar with the region's express-highway system operations.

This study addresses the MPO's goal of reducing congestion and increasing safety on the region's express-highway system. MPO staff will submit this proposal to the MPO for discussion and approval. If the MPO approves these locations for study, staff will meet with officials from MassDOT to discuss specifics, conduct field visits, collect data, and perform various analyses.

## APPENDIX B

1. ATR data
2. Classification data



Appendix B



| TIME | $\begin{array}{r} \text { MON } \\ 12 \end{array}$ | $\begin{array}{r} \text { TUE } \\ 13 \end{array}$ | $\begin{array}{r} \text { WED } \\ 14 \end{array}$ | $\begin{array}{r} \text { THU } \\ 15 \end{array}$ | $\begin{array}{r} \text { FRI } \\ 16 \end{array}$ | WKDAY <br> AVG | SAT | SUN | WEEK <br> AVG | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01:00 |  | 125 | 136 | 110 | 114 | 121 |  |  | 121 | 485 |
| 02:00 |  | 46 | 54 | 57 | 47 | 51 |  |  | 51 | 204 |
| 03:00 |  | 20 | 36 | 23 | 47 | - 31 |  |  | 31 | 126 |
| 04:00 |  | 14 | 20 | 24 | 21 | 19 |  |  | 19 | 79 |
| 05:00 |  | 31 | 44 | 41 | 42 | 39 |  |  | 39 | 158 |
| 06:00 |  | 197 | 202 | 190 | 178 | 191 |  |  | 191 | 767 |
| 07:00 |  | 605 | 609 | 597 | 526 | 584 |  |  | 584 | 2337 |
| 08:00 |  | 1511 | 1464 | 1471 | 1399 | 1461 |  |  | 1461 | 5845 |
| 09:00 |  | 1547 | 1521 | 1507 | 1537 | 1528 |  |  | 1528 | 6112 |
| 10:00 |  | 1160 | 1189 | 1229 | 1054 | 1158 |  |  | 1158 | 4632 |
| 11:00 |  | 874 | 838 | 864 | 88 B | 866 |  |  | 866 | 3464 |
| 12:00 |  | 788 | 766 | 810 |  | 788 |  |  | 788 | 2364 |
| 13:00 | 803 | 866 | 834 | 966 |  | 867 |  |  | B67 | 3469 |
| 14:00 | 797 | 829 | 925 | 982 |  | 883 |  |  | 883 | 3533 |
| 15:00 | 957 | 1065 | 1059 | 866 |  | 986 |  |  | 986 | 3947 |
| 16:00 | 891 | 877 | 950 | 976 |  | 923 |  |  | 923 | 3694 |
| 17:00 | 793 | 836 | 925 | 875 |  | 857 |  |  | 857 | 3429 |
| 18:00 | 816 | 1071 | 979 | 974 |  | 960 |  |  | 960 | 3840 |
| 19:00 | 1123 | 1082 | 1088 | 1154 |  | 1111 |  |  | 1111 | 4447 |
| 20:00 | 714 | 877 | 921 | 911 |  | 855 |  |  | 855 | 3423 |
| 21:00 | 468 | 522 | 547 | 545 |  | 520 |  |  | 520 | 2082 |
| 22:00 | 392 | 414 | 521 | 448 |  | 443 |  |  | 443 | 1775 |
| 23:00 | 302 | 378 | 360 | 359 |  | 349 |  |  | 349 | 1399 |
| 24:00 | 197 | 266 | 237 | 232 |  | 233 |  |  | 233 | 932 |
| TOTALS | 8253 | 16001 | 16225 | 16211 | 5853 | 15824 | 0 | 0 | 15824 | 62543 |
| \% AVG WKDY | 52.1 | 101.1 | 102.5 | 102.4 | 36.9 |  |  |  |  |  |
| \% AVG WEEK | 52.1 | 101. 1 | 102.5 | 102.4 | 36.9 |  |  |  |  |  |
| AM Times |  | 09:00 | 09:00 | 09:00 | 09:00 | 09:00 |  |  | 09:00 |  |
| AM Peaks |  | 1547 | 1521 | 1507 | 1537 | 1528 |  |  | 1528 |  |
| PM Times | 19:00 | 19:00 | 19:00 | 19:00 |  | 19:00 |  |  | 19:00 |  |
| PM Peaks | 1123 | 1082 | 1088 | 1154 |  | 1111 |  |  | 1111 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 14 | 10 | 9 | 9 | 26 |  |  |  |  |  |

Appendix B



| TOTALS | 5905 | 9406 | 9654 | 9413 | 3087 | 9488 | 0 | 0 | 9488 | 37465 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% AVG WKDY | 62.2 | 99.1 | 101.7 | 99.2 | 32.5 |  |  |  |  |  |
| \% AVG WEEK | 62.2 | 99.1 | 101.7 | 99.2 | 32.5 |  |  |  |  |  |
| AM Times |  | 09:00 | 10:00 | 11:00 | 11:00 | 11:00 |  |  | 11:00 |  |
| AM Peaks |  | 525 | 552 | 532 | 674 | 558 |  |  | 558 |  |
| PM Times | 15:00 | 15:00 | 15:00 | 15:00 |  | 15:00 |  |  | 15:00 |  |
| PM Peaks | 723 | 781 | 688 | 671 |  | 715 |  |  | 715 |  |
| D8 | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 12 | 8 | 7 | 7 | 22 |  |  |  |  |  |

Appendix B


Appendix B


Appendix B

Traffic Count Data B-8

MassDOT Highway Division WEEKLY SUMMARY FOR LANE

Page: 1
Starting: 6/12/2017

| Site Refere <br> Site ID: 000 <br> Location: <br> Direction: |  | $\begin{aligned} & 0000671 \\ & \text { N-RAMP } \end{aligned}$ | I-95N $\operatorname{STA,7}$ |  |  |  | ```File: R12640.prn City: LEXINGTON County: VOLUME-RAMP``` |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIME | $\begin{array}{r} \text { MON } \\ 12 \end{array}$ | $\begin{array}{r} T U E \\ 13 \end{array}$ | $\begin{array}{r} \text { WED } \\ 14 \end{array}$ | $\begin{array}{r} \text { THU } \\ 15 \end{array}$ | $\begin{array}{r} \text { FRI } \\ 16 \end{array}$ | WKDAY <br> AVG | SAT | SUN | $\begin{array}{r} \text { WEEK } \\ \text { AVG } \end{array}$ | TOTAL |
| 01:00 |  | 17 | 17 | 14 | 9 | 14 |  |  | 14 | 57 |
| 02:00 |  | 3 | 8 | 10 | 10 | 7 |  |  | 7 | 31 |
| 03:00 |  | 2 | 2 | 3 | 5 | 3 |  |  | 3 | 12 |
| 04:00 |  | 4 | 4 | 3 | 3 | 3 |  |  | 3 | 14 |
| 05:00 |  | 8 | 10 | 12 | 13 | 10 |  |  | 10 | 43 |
| 06:00 |  | 48 | 47 | 45 | 41 | 45 |  |  | 45 | 181 |
| 07:00 |  | 190 | 179 | 199 | 171 | 184 |  |  | 184 | 739 |
| 08:00 |  | 339 | 326 | 357 | 265 | 321 |  |  | 321 | 1287 |
| 09:00 |  | 334 | 380 | 344 | 245 | 325 |  |  | 325 | 1303 |
| 10:00 |  | 311 | 265 | 307 | 215 | 274 |  |  | 274 | 1098 |
| 11:00 |  | 213 | 205 | 184 | 178 | 195 |  |  | 195 | 780 |
| 12:00 |  | 186 | 172 | 181 |  | 179 |  |  | 179 | 539 |
| 13:00 | 163 | 186 | 179 | 195 |  | 180 |  |  | 180 | 723 |
| 14:00 | 184 | 201 | 230 | 177 |  | 198 |  |  | 198 | 792 |
| 15:00 | 203 | 190 | 213 | 132 |  | 184 |  |  | 184 | 738 |
| 16:00 | 177 | 185 | 206 | 176 |  | 186 |  |  | 186 | 744 |
| 17:00 | 124 | 119 | 134 | 112 |  | 122 |  |  | 122 | 489 |
| 18:00 | 147 | 162 | 141 | 93 |  | 135 |  |  | 135 | 543 |
| 19:00 | 101 | 140 | 146 | 152 |  | 134 |  |  | 134 | 539 |
| 20:00 | 89 | 110 | 113 | 129 |  | 110 |  |  | 110 | 441 |
| 21:00 | 78 | 76 | 141 | 72 |  | 91 |  |  | 91 | 367 |
| 22:00 | 37 | 53 | 62 | 64 |  | 54 |  |  | 54 | 216 |
| 23:00 | 37 | 38 | 50 | 36 |  | 40 |  |  | 40 | 161 |
| 24:00 | 36 | 28 | 35 | 45 |  | 36 |  |  | 36 | 144 |
| TOTALS | 1376 | 3143 | 3265 | 3042 | 1155 | 3030 | 0 | 0 | 3030 | 11981 |
| \% AVG WKDY | 45.4 | 103.7 | 107.7 | 100.3 | 38.1 |  |  |  |  |  |
| 告 AVG WEEK | 45.4 | 103.7 | 107.7 | 100.3 | 38.1 |  |  |  |  |  |
| AM Times |  | 08:00 | 09:00 | 08:00 | 08:00 | 09:00 |  |  | 09:00 |  |
| AM Peaks |  | 339 | 380 | 357 | 265 | 325 |  |  | 325 |  |
| PM Times | 15:00 | 14:00 | 14:00 | 13:00 |  | 14:00 |  |  | 14:00 |  |
| PM Peaks | 203 | 201 | 230 | 195 |  | 198 |  |  | 198 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K8 | 15 | 11 | 12 | 12 | 23 |  |  |  |  |  |

Appendix B

|  | MassDOT Highway Division WEEKLY SUMMARY EOR LANE Starting: 6/12/2017 | Page: |
| :---: | :---: | :---: |
|  | $57 A \cdot 8$ |  |
| Site Reference: 170170000717 |  | File: R12642.prn |
| Site ID: 000000012642 |  | City: LEXINGTON |
| Location: RTE.2A WB ON-RAMP TO I-95N Direction: ROAD TOTAL |  | County: VOLUME-RAMP |


| TIME | MON <br> 12 | $\begin{array}{r} \text { TUE } \\ 13 \end{array}$ | WED $14$ | $\begin{array}{r} \text { THU } \\ 15 \end{array}$ | $\begin{array}{r} \text { FRI } \\ 16 \end{array}$ | WKDAY <br> AVG | SAT | SUN | WEEK <br> AVG | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01:00 |  | 6 | 0 | 日 | 4 | 4 |  |  | 4 | 18 |
| 02:00 |  | 1 | 2 | 3 | 3 | 2 |  |  | 2 | 9 |
| 03:00 |  | 5 | 4 | 2 | 2 | 3 |  |  | 3 | 13 |
| 04:00 |  | 1 | 2 | 1 | 1 | 1 |  |  | 1 | 5 |
| 05:00 |  | 8 | 2 | 5 | 4 | 4 |  |  | 4 | 19 |
| 06:00 |  | 22 | 22 | 12 | 18 | 18 |  |  | 18 | 74 |
| 07:00 |  | 49 | 61 | 52 | 46 | 52 |  |  | 52 | 208 |
| 08:00 |  | 114 | 132 | 122 | 105 | 118 |  |  | 118 | 473 |
| 09:00 |  | 201 | 185 | 187 | 172 | 186 |  |  | 186 | 745 |
| 10:00 |  | 117 | 118 | 114 | 126 | 118 |  |  | 118 | 475 |
| 11:00 |  | 94 | 78 | 81 | 92 | 86 |  |  | B6 | 345 |
| 12:00 |  | 101 | 88 | 89 |  | 92 |  |  | 92 | 278 |
| 13:00 | 110 | 102 | 98 | 104 |  | 103 |  |  | 103 | 414 |
| 14:00 | 81 | 99 | 92 | 87 |  | 89 |  |  | 89 | 359 |
| 15:00 | 80 | 80 | 120 | 140 |  | 105 |  |  | 105 | 420 |
| 16:00 | 124 | 115 | 242 | 193 |  | 168 |  |  | 168 | 674 |
| 17:00 | 95 | B4 | 101 | 84 |  | 91 |  |  | 91 | 364 |
| 18:00 | 64 | 110 | 64 | 83 |  | 80 |  |  | 80 | 321 |
| 19:00 | 83 | 75 | 80 | 69 |  | 76 |  |  | 76 | 307 |
| 20:00 | 53 | 62 | 81 | 75 |  | 67 |  |  | 67 | 271 |
| 21:00 | 47 | 58 | 81 | 88 |  | 68 |  |  | 68 | 274 |
| 22:00 | 33 | 31 | 27 | 35 |  | 31 |  |  | 31 | 126 |
| 23:00 | 13 | 14 | 21 | 14 |  | 15 |  |  | 15 | 62 |
| 24:00 | 3 | 8 | 10 | 7 |  | 7 |  |  | 7 | 28 |
| TOTALS | 786 | 1557 | 1711 | 1655 | 573 | 1584 | 0 | 0 | 1584 | 6282 |
| \% AVG WKDY | 49.6 | 98.2 | 108 | 104.4 | 36.1 |  |  |  |  |  |
| \% AVG WEEK | 49.6 | 98.2 | 108 | 104.4 | 36.1 |  |  |  |  |  |
| AM Times |  | 09:00 | 09:00 | 09:00 | 09:00 | 09:00 |  |  | 09:00 |  |
| AM Peaks |  | 201 | 185 | 187 | 172 | 186 |  |  | 186 |  |
| PM Times | 16:00 | 16:00 | 16:00 | 16:00 |  | 16:00 |  |  | 16:00 | . |
| PM Peaks | 124 | 115 | 242 | 193 |  | 168 |  |  | 168 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 16 | 13 | 14 | 12 | 30 |  |  |  |  |  |

Appendix B


Appendix B

MassDOT Highway Division WEEKLY SUMMARY EOR LANE

Page: 1
Starting: 6/12/2017

$$
\text { STA. } 10
$$

Site Reference: 170170000611 Site ID: 000000012252

File: R12252.prn
Location: 193 SB EXIT 37C COMMERCE WAY/ATLANTIC AV
City: WOBURN
County: VOLUME-RAMP

| TIME | $\begin{array}{r} \text { MON } \\ 12 \end{array}$ | $\begin{array}{r} \text { TUE } \\ 13 \end{array}$ | $\begin{array}{r} \text { WED } \\ 14 \end{array}$ | $\begin{array}{r} \text { THU } \\ 15 \end{array}$ | $\begin{array}{r} \text { FRI } \\ 16 \end{array}$ | WKDAY AVG | SAT | SUN | WEEK AVG | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01:00 |  | 6 | 10 | 8 | 10 | 8 |  |  | 8 | 34 |
| 02:00 |  | 13 | 15 | 12 | 15 | 13 |  |  | 13 | 55 |
| 03:00 |  | 45 | 38 | 49 | 42 | 43 |  |  | 43 | 174 |
| 04:00 |  | 74 | 86 | 105 | 73 | 84 |  |  | 84 | 338 |
| 05:00 |  | 152 | 142 | 144 | 142 | 145 |  |  | 145 | 580 |
| 06:00 |  | 477 | 509 | 529 | 493 | 502 |  |  | 502 | 2008 |
| 07:00 |  | 924 | 922 | 886 | 801 | 883 |  |  | 883 | 3533 |
| 08:00 |  | 1297 | 1365 | 1437 | 1223 | 1330 |  |  | 1330 | 5322 |
| 09:00 |  | 1285 | 1286 | 1479 | 970 | 1255 |  |  | 1255 | 5020 |
| 10:00 |  | 645 | 657 | 772 | 539 | 653 |  |  | 653 | 2613 |
| 11:00 |  | 288 | 357 | 367 | 373 | 346 |  |  | 346 | 1385 |
| 12:00 |  | 282 | 306 | 336 |  | 308 |  |  | 308 | 924 |
| 13:00 | 218 | 273 | 285 | 631 |  | 351 |  |  | 351 | 1407 |
| 14:00 | 237 | 246 | 291 | 343 |  | 279 |  |  | 279 | 1117 |
| 15:00 | 274 | 330 | 352 | 447 |  | 350 |  |  | 350 | 1403 |
| 16:00 | 212 | 244 | 281 | 267 |  | 251 |  |  | 251 | 1004 |
| 17:00 | 202 | 226 | 265 | 276 |  | 242 |  |  | 242 | 969 |
| 18:00 | 337 | 261 | 334 | 277 |  | 302 |  |  | 302 | 1209 |
| 19:00 | 213 | 206 | 269 | 236 |  | 231 |  |  | 231 | 924 |
| 20:00 | 135 | 140 | 181 | 169 |  | 156 |  |  | 156 | 625 |
| 21:00 | 116 | 121 | 139 | 117 |  | 123 |  |  | 123 | 493 |
| 22:00 | 74 | 80 | 100 | 99 |  | 88 |  |  | 88 | 353 |
| 23:00 | 46 | 42 | 49 | 50 |  | 46 |  |  | 46 | 187 |
| 24:00 | 43 | 51 | 59 | 49 |  | 50 |  |  | 50 | 202 |
| TOTALS | 2107 | 7708 | 8298 | 9085 | 4681 | 8039 | 0 | 0 | 8039 | 31879 |
| \% AVG WKDY | 26.2 | 95.8 | 103.2 | 113 | 58.2 |  |  |  |  |  |
| \% AVG WEEK | 26.2 | 95.8 | 103.2 | 113 | 58.2 |  |  |  |  |  |
| AM Times |  | 08:00 | 08:00 | 09:00 | 08:00 | 08:00 |  |  | 08:00 |  |
| AM Peaks |  | 1297 | 1365 | 1479 | 1223 | 1330 |  | . | 1330 |  |
| PM Times | 18:00 | 15:00 | 15:00 | 13:00 |  | 13:00 |  |  | 13:00 |  |
| PM Peaks | 337 | 330 | 352 | 631 |  | 351 |  |  | 351 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 16 | 17 | 16 | 16 | 26 |  |  |  |  |  |

Appendix B

|  | STA.11 |  |
| :--- | :--- | :--- |
| Site Reference: 170170000747 |  | File: R12253.prn |
| Site ID: 000000012253 | City: WOBURN |  |
| Location: COMMERCE WAY ON RAMP TO I93 SB |  | County: VOLUME-RAMP |
| Direction: ROAD TOTAL |  |  |


| TIME | $\begin{array}{r} M O N \\ 12 \end{array}$ | $\begin{array}{r} \text { TUE } \\ 13 \end{array}$ | $\begin{array}{r} \text { WED } \\ 14 \end{array}$ | $\begin{array}{r} \text { THU } \\ 15 \end{array}$ | $\begin{array}{r} \text { FRI } \\ 16 \end{array}$ | WKDAY AVG | SAT | SUN | $\begin{aligned} & \text { WEEK } \\ & \text { AVG } \end{aligned}$ | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01:00 |  | 33 | 29 | 39 | 31 | 33 |  |  | 33 | 132 |
| 02:00 |  | 28 | 24 | 26 | 27 | 26 |  |  | 26 | 105 |
| 03:00 |  | 20 | 23 | 21 | 16 | 20 |  |  | 20 | 80 |
| 04:00 |  | 34 | 37 | 46 | 58 | 43 |  |  | 43 | 175 |
| 05:00 |  | 54 | 36 | 47 | 44 | 45 |  |  | 45 | 181 |
| 06:00 |  | 107 | 117 | 111 | 135 | 117 |  |  | 117 | 470 |
| 07:00 |  | 176 | 201 | 182 | 194 | 188 |  |  | 188 | 753 |
| 08:00 |  | 183 | 173 | 151 | 171 | 169 |  |  | 169 | 678 |
| 09:00 |  | 160 | 175 | 143 | 175 | 163 |  |  | 163 | 653 |
| 10:00 |  | 264 | 206 | 226 | 264 | 240 |  | , | 240 | 960 |
| 11:00 |  | 316 | 383 | 298 | 311 | 327 |  |  | 327 | 1308 |
| 12:00 |  | 434 | 401 | 457 |  | 430 |  |  | 430 | 1292 |
| 13:00 | 470 | 461 | 476 | 557 |  | 491 |  |  | 491 | 1964 |
| 14:00 | 443 | 427 | 432 | 497 |  | 449 |  |  | 449 | 1799 |
| 15:00 | 487 | 489 | 559 | 542 |  | 519 |  |  | 519 | 2077 |
| 16:00 | 515 | 519 | 490 | 487 |  | 502 |  |  | 502 | 2011 |
| 17:00 | 730 | 773 | 744 | 756 |  | 750 |  |  | 750 | 3003 |
| 18:00 | 948 | 974 | 964 | 990 |  | 969 |  |  | 969 | 3876 |
| 19:00 | 527 | 609 | 584 | 575 |  | 573 |  |  | 573 | 2295 |
| 20:00 | 363 | 375 | 337 | 342 |  | 354 |  |  | 354 | 1417 |
| 21:00 | 272 | 265 | 256 | 259 |  | 263 |  |  | 263 | 1052 |
| 22:00 | 150 | 179 | 230 | 169 |  | 182 |  |  | 182 | 728 |
| 23:00 | 102 | 103 | 110 | 137 |  | 113 |  |  | 113 | 452 |
| 24:00 | 105 | 118 | 96 | 106 |  | 106 |  |  | 106 | 425 |
| totals | 5112 | 7101 | 7083 | 7164 | 1426 | 7072 | 0 | 0 | 7072 | 27886 |
| \% AVG WKDY | 72.2 | 100.4 | 100.1 | 101.3 | 20.1 |  |  |  |  |  |
| \% AVG WEEK | 72.2 | 100.4 | 100.1 | 101.3 | 20.1 |  |  |  |  |  |
| AM Times |  | 12:00 | 12:00 | 12:00 | 11:00 | 12:00 |  |  | 12:00 |  |
| AM Peaks |  | 434 | 401 | 457 | 311 | 430 |  |  | 430 |  |
| PM Times | 18:00 | 18:00 | 18:00 | 18:00 |  | 18:00 |  |  | 18:00 |  |
| PM Peaks | 948 | 974 | 964 | 990 |  | 969 |  |  | 969 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 19 | 14 | 14 | 14 | 22 |  |  |  |  |  |

Appendix B

| MassDOT Highway Division WEEKLY SUMMARY FOR LANE Starting: 6/12/2017 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STA. 12 |  |  |  |  |  |  |  |  |  |  |
| Site Reference: 170170000672 <br> Site ID: 000000012175 |  |  |  |  |  |  | $\begin{aligned} & \text { File: R12175.prn } \\ & \text { City: WOBURN } \end{aligned}$ |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| Location: I93 SB EX 37B TO I-95 S. WALTHAM County: VOLUME-RAMP <br> Direction: ROAD TOTAL |  |  |  |  |  |  | County: VOLUME-RAMP |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| TIME | MON | TUE | WED | THU | FRI | WKDAY | SAT | SUN | WEEK | TOTAL |
|  | 12 | 13 | 14 | 15 | 16 | AVG |  |  | AVG |  |
| 01:00 |  | 85 | 83 | 90 | 85 | 85 |  |  | 85 | 343 |
| 02:00 |  | 56 | 72 | 85 | 77 | 72 |  |  | 72 | 290 |
| 03:00 |  | 67 | 72 | 72 | 77 | 72 |  |  | 72 | 288 |
| 04:00 |  | 111 | 128 | 124 | 119 | 120 |  |  | 120 | - 482 |
| 05:00 |  | 256 | 251 | 278 | 283 | 267 |  |  | 267 | 1068 |
| 06:00 |  | 815 | 851 | 859 | 794 | 829 |  |  | 829 | 3319 |
| 07:00 |  | 1151 | 1136 | 1186 | 1459 | 1233 |  |  | 1233 | 4932 |
| 08:00 |  | 1798 | 1913 | 1801 | 1906 | 1854 |  |  | 1854 | 7418 |
| 09:00 |  | 1865 | 1884 | 1932 | 2015 | 1924 |  |  | 1924 | 7696 |
| 10:00 |  | 1894 | 1903 | 1792 | 1688 | 1819 |  |  | 1819 | 7277 |
| 11:00 |  | 1401 | 1525 | 1483 | 1266 | 1418 |  |  | 1418 | 5675 |
| 12:00 |  | 1256 | 1343 | 1512 |  | 1370 |  |  | 1370 | 4111 |
| 13:00 975 |  | 1259 | 1328 | 1454 |  | 1254 |  |  | 1254 | 5016 |
| 14:00 | 1066 | 1165 | 1138 | 1520 |  | 1222 |  |  | 1222 | 4889 |
| 15:00 | 1193 | 1115 | 1237 | 1471 |  | 1254 |  |  | 1254 | 5016 |
| 16:00 | 945 | 958 | 1071 | 1192 |  | 1041 |  |  | 1041 | 4166 |
| 17:00 | 1230 | 1207 | 1330 | 1421 |  | 1297 |  |  | 1297 | 5188 |
| 18:00 | 1377 | 1262 | 1442 | 1425 |  | 1376 |  |  | 1376 | 5506 |
| 19:00 | 1064 | 1081 | 1297 | 1173 |  | 1153 |  |  | 1153 | 4615 |
| 20:00 | 628 | 572 | 779 | 770 |  | 687 |  |  | 687 | 2749 |
| $21: 00$ | 478 | 458 | 531 | 513 |  | 495 |  |  | 495 | 1980 |
| 22:00 | 309 | 363 | 439 | 372 |  | 370 |  |  | 370 | 1483 |
| 23:00 | 270 | 280 | 298 | 329 |  | 294 |  |  | 294 | 1177 |
| 24:00 | 164 | 162 | 180 | 189 |  | 173 |  |  | 173 | 695 |
| TOTALS | 9699 | 20637 | 22231 | 23043 | 9769 | 21679 | 0 | 0 | 21679 | 85379 |
| \% AVG WKDY | 44.7 | 95.1 | 102.5 | 106.2 | 45 |  |  |  |  |  |
| \% AVG WEEK | 44.7 | 95.1 | 102.5 | 106.2 | 45 |  |  |  |  |  |
| AM Times |  | 10:00 | 08:00 | 09:00 | 09:00 | 09:00 |  |  | 09:00 |  |
| AM Peaks |  | 1894 | 1913 | 1932 | 2015 | 1924 |  |  | 1924 |  |
| PM Times PM Peaks | 18:00 | 18:00 | 18:00 | 14:00 |  | 18:00 |  |  | 18:00 |  |
|  | 1377 | 1262 | 1442 | 1520 |  | 1376 |  |  | 1376 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 14 | 9 | 9 | 8 | 21 |  |  |  |  |  |

Appendix B


Appendix B


Appendix B

| MassDOT Highway Division WEEKLY SUMMARY EOR LANE Starting: 6/12/2017 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $5 T A \cdot 15$ |  |  |  |  |  |  |  |  |  |  |
| Site Reference: 170170000692 <br> Site ID: 000000022550 |  |  |  |  |  |  | File: R22550.prn <br> City: RANDOLPH |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| Location: RTE. 24 NB EXIT2IA TO 93 N BOSTON |  |  |  |  |  |  | County: VOLUME-RAMP |  |  |  |
| Direction: ROAD TOTAL |  |  |  |  |  |  |  |  |  |  |
| TIME | MON | TUE | WED | THU | FRI | WKDAY | SAT | SUN | WEEK | TOTAL |
|  | 12 | 13 | 14 | 15 | 16 | AVG |  |  | AVG |  |
| 01:00 |  | 343 | 283 | 361 | 307 | 323 |  |  | 323 | 1294 |
| 02:00 |  | 245 | 231 | 241 | 255 | 243 |  |  | 243 | 972 |
| 03:00 |  | 234 | 251 | 249 | 303 | 259 |  |  | 259 | 1037 |
| 04:00 |  | 410 | 413 | 463 | 421 | 426 |  |  | 426 | 1707 |
| 05:00 |  | 1326 | 1247 | 1275 | 1166 | 1253 |  |  | 1253 | 5014 |
| 06:00 |  | 3062 | 3049 | 3042 | 3029 | 3045 |  |  | 3045 | 12182 |
| 07:00 |  | 2071 | 2256 | 2196 | 2278 | 2200 |  |  | 2200 | 8801 |
| 08:00 |  | 2189 | 2168 | 2303 | 2493 | 2288 |  |  | 2288 | 9153 |
| 09:00 |  | 2228 | 2223 | 2228 | 1246 | 1981 |  |  | 1981 | 7925 |
| 10:00 |  | 2365 | 2472 | 2603 | 2623 | 2515 |  |  | 2515 | 10063 |
| 11:00 |  | 2327 | 2454 | 2457 |  | 2412 |  |  | 2412 | 7238 |
| 12:00 | 2472 | 2357 | 2356 | 2479 |  | 2416 |  |  | 2416 | 9664 |
| 13:00 | 2527 | 2461 | 2479 | 2314 |  | 2445 |  |  | 2445 | 9781 |
| 14:00 | 2291 | 2375 | 2439 | 2346 |  | 2362 |  |  | 2362 | 9451 |
| 15:00 | 2168 | 2198 | 2248 | 2222 |  | 2209 |  |  | 2209 | 8836 |
| 16:00 | 2150 | 2083 | 2150 | 2060 |  | 2110 |  |  | 2110 | 8443 |
| 17:00 | 2076 | 2053 | 2034 | 2083 |  | 2061 |  |  | 2061 | 8246 |
| 18:00 | - 1962 | 2090 | 1963 | 2060 |  | 2018 |  |  | 2018 | 8075 |
| 19:00 | 1690 | 1776 | 1675 | 1813 |  | 1738 |  |  | 1738 | 6954 |
| 20:00 | 1525 | 1487 | 1471 | 1512 |  | 1498 |  |  | 1498 | 5995 |
| 21:00 | 1436 | 1351 | 1401 | 1485 |  | 1418 |  |  | 1418 | 5673 |
| 22:00 | 1211 | 1147 | 1288 | 1424 |  | 1267 |  |  | 1267 | 5070 |
| 23:00 | 931 | 918 | 1035 | 1045 |  | 982 |  |  | 982 | 3929 |
| 24:00 | 505 | 518 | 543 | 601 |  | 541 |  |  | 541 | 2167 |
| TOTALS | 22944 | 39614 | 40129 | 40862 | 14121 | 40010 | 0 | 0 | 40010 | 157670 |
| \% AVG WKDY | 57.3 | 99 | 100.2 | 102.1 | 35.2 |  |  |  |  |  |
| \% AVG WEEK | 57.3 | 99 | 100.2 | 102.1 | 35.2 |  |  |  |  |  |
| AM Times | 12:00 | 06:00 | 06:00 | 06:00 | 06:00 | 06:00 |  |  | 06:00 |  |
| AM Peaks | 2472 | 3062 | 3049 | 3042 | 3029 | 3045 |  |  | 3045 |  |
| PM Times | 13:00 | 13:00 | 13:00 | 14:00 |  | 13:00 |  |  | 13:00 |  |
| PM Peaks | 2527 | 2461 | 2479 | 2346 |  | 2445 |  |  | 2445 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 11 | 8 | 8 | 7 | 21 |  |  |  |  |  |

Appendix B

| MassDOT Highway Division <br> WEEKLY SUMMARY FOR LANE <br> Starting: 6/12/2017 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ```Site Reference: 170170000573 Site ID: 000000022549 Location: RTE.24 NB EXIT21B TO 93 S Direction: ROAD TOTAL``` |  |  |  | $5 T A \cdot 16 \quad \begin{aligned} & \text { File: R22549.prn } \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \end{aligned}$ |  |  |  |  |  |  |
| TIME | MON 12 | $\begin{array}{r} \text { TUE } \\ 13 \end{array}$ | WED 14 | $\begin{array}{r} \text { THU } \\ 15 \end{array}$ | $\begin{array}{r} \text { FRI } \\ 16 \end{array}$ | $\begin{gathered} \text { WKDAY } \\ \text { AVG } \end{gathered}$ | SAT | SUN | WEEK <br> AVG | TOTAL |
| 01:00 188 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{lllllll}03: 00 & 131 & 127 & 106 & 143 & 126 & 126\end{array}$ |  |  |  |  |  |  |  |  |  |  |
| 04:00 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| 06:00 2388 2341 240023568 |  |  |  |  |  |  |  |  |  |  |
| $07: 002238$ 2474 2488 2487 2421 2421 |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| $11: 001901819315$ |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{llllll}12: 00 & 1656 & 1585 & 1736 & 1743 & 1680\end{array}$ |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{lllllll}13: 00 & 1566 & 1626 & 1668 & 1736 & 1649 & 1649\end{array}$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{llllll}15: 00 & 1927 & 1932 & 1956 & 1969 & 1946\end{array}$ |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{llllll}16: 00 & 1813 & 1896 & 1846 & 1792 & 1836\end{array}$ |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{lllllll}17.00 & 1774 & 1847 & 1895 & 1779 & 1823 & 1823\end{array}$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| $19: 00$ 1332 1322 1367 1428 1362  <br> 136492       |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{llllll}20: 00 & 1011 & 942 & 985 & 1108 & 1011\end{array}$ |  |  |  |  |  |  |  |  |  |  |
| $\begin{array}{llllll}21: 00 & 814 & 758 & 754 & 798 & 781\end{array}$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| 24:00 | 313 | 292 | 294 | 341 |  | 310 |  |  | 310 | 1240 |
|  |  |  |  |  |  |  |  |  |  |  |
| TOTALS | 16984 | 31458 | 31932 | 32462 | 11905 | 31657 | 0 | 0 | 31657 | 124741 |
| \% AVG WKDY | 53.6 | 99.3 | 100.8 | 102.5 | 37.6 |  |  |  |  |  |
| \% AVG WEEK | 53.6 | 99.3 | 100.8 | 102.5 | 37.6 |  |  |  |  |  |
| AM Times | 12:00 | 06:00 | 07:00 | 07:00 | 07:00 | 07:00 |  |  | 07:00 |  |
| AM Peaks | 1656 | 2388 | 2474 | 2488 | 2487 | 2421 |  |  | 2421 |  |
| PM Times | 15:00 | 15:00 | 15:00 | 15:00 |  | 15:00 |  |  | 15:00 |  |
|  | 1927 | 1932 | 1956 | 1969 |  | 1946 |  |  | 1946 |  |
| $\begin{aligned} & \mathrm{D} \% \\ & \mathrm{~K} \% \end{aligned}$ | 100 | 100 8 | 100 8 | 100 8 | 100 21 |  |  |  |  |  |

Appendix B

| MassDOT Highway Division WEEKLY SUMMARY FOR LANE Starting: 6/12/2017 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $5 T A, 17$ |  |  |  |  |  |  |  |  |  |  |
| Site Reference: 170170000430Site ID: 00000012024Location: I93 SB EXIT 4 TO RTE. 24 S . FALL RIVE |  |  |  |  |  |  | $\begin{aligned} & \text { File: R12024.prn } \\ & \text { City: RANDOLPH } \end{aligned}$ |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | Direction: ROAD TOTAL |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TIME | MON | TUE | WED | THU | FRI | WKDAY | SAT | SUN | WEEK | TOTAL |
|  | 12 | 13 | 14 | 15 | 16 | AVG |  |  | AVG |  |
| 01:00 |  | 813 | 740 | 652 | 747 | 738 |  |  | 738 | 2952 |
| 02:00 |  | 423 | 369 | 409 | 477 | 419 |  |  | 419 | 1678 |
| 03:00 |  | 239 | 321 | 323 | 406 | 322 |  |  | 322 | 1289 |
| 04:00 |  | 244 | 259 | 264 | 280 | 261 |  |  | 261 | 1047 |
| 05:00 |  | 398 | 413 | 393 | 413 | 404 |  |  | 404 | 1617 |
| 06:00 |  | 896 | 891 | 907 | 891 | 896 |  |  | 896 | 3585 |
| $07: 00$ |  | 1420 | 1472 | 1475 | 1436 | 1450 |  |  | 1450 | 5803 |
| 08:00 |  | 1816 | 1882 | 1953 | 1907 | 1889 |  |  | 1889 | 7558 |
| 09:00 |  | 1828 | 1808 | 1857 | 1759 | 1813 |  |  | 1813 | 7252 |
| 10:00 |  | 1593 | 1767 | 1795 | 1834 | 1747 |  |  | 1747 | 6989 |
| 11:00 |  | 1899 | 1828 | 1647 |  | 1791 |  |  | 1791 | 5374 |
| 12:00 2288 |  | 2228 | 2187 | 2410 |  | 2278 |  |  | 2278 | 9113 |
| 13:00 | 2376 | 2311 | 2451 | 2450 |  | 2397 |  |  | 2397 | 9588 |
| 14:00 | 2419 | 2613 | 2496 | 2599 |  | 2531 |  |  | 2531 | 10127 |
| 15:00 | 2892 | 1835 | 2458 | 2772 |  | 2489 |  |  | 2489 | 9957 |
| 16:00 | 2734 | 2504 | 2637 | 2576 |  | 2612 |  |  | 2612 | 10451 |
| 17:00 | 2558 | 2479 | 2518 | 2488 |  | 2510 |  |  | 2510 | 10043 |
| 18:00 | 2542 | 2319 | 2229 | 2536 |  | 2406 |  |  | 2406 | 9626 |
| 19:00 | 2539 | 2539 | 2531 | 2523 |  | 2533 |  |  | 2533 | 10132 |
| 20:00 | 2513 | 2536 | 2557 | 2575 |  | 2545 |  |  | 2545 | 10181 |
| 21:00 | 2158 | 1915 | 2135 | 2139 |  | 2086 |  |  | 2086 | 8347 |
| 22:00 | 1874 | 1657 | 1747 | 1987 |  | 1816 |  |  | 1816 | 7265 |
| 23:00 | 1446 | 1367 | 1476 | 1442 |  | 1432 |  |  | 1432 | 5731 |
| 24:00 | 1057 | 1227 | 1212 | 1188 |  | 1171 |  |  | 1171 | 4684 |
| TOTALS | 29396 | 39099 | 40384 | 41360 | 10150 | 40536 | 0 | 0 | 40536 | 160389 |
| \% AVG WKDY | 72.5 | 96.4 | 99.6 | 102 | 25 |  |  |  |  |  |
| A AVG WEEK | 72.5 | 96.4 | 99.6 | 102 | 25 |  |  |  |  |  |
| AM Times | 12:00 | 12:00 | 12:00 | 12:00 | 08:00 | 12:00 |  |  | 12:00 |  |
| AM Peaks | 2288 | 2228 | 2187 | 2410 | 1907 | 2278 |  |  | 2278 |  |
| PM Times | 15:00 | 14:00 | 16:00 | 15:00 |  | 16:00 |  |  | 16:00 |  |
| PM Peaks | 2892 | 2613 | 2637 | 2772 |  | 2612 |  |  | 2612 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 10 | 7 | 7 | 7 | 19 |  |  |  |  |  |

Appendix B

```
MassDOT Highway Division
WEEKLY SUMMARY FOR LANE Page: 1
    Starting: 6/12/2017
STA. 18
File: R12007.prn
City: RANDOLPH
```

Site Reference: 170070000494
Site ID: 000000012007
Location: I93 NB EXIT 4 TO RTE. 24 S. FALL RIVE
Direction: ROAD TOTAL

| TIME | $\begin{array}{r} \text { MON } \\ 12 \end{array}$ | $\begin{array}{r} \text { TUE } \\ 13 \end{array}$ | $\begin{array}{r} \text { WED } \\ 14 \end{array}$ | $\begin{array}{r} \text { THU } \\ 15 \end{array}$ | $\begin{array}{r} \text { FRI } \\ 16 \end{array}$ | WKDAY AVG | SAT | SUN | $\begin{gathered} \text { WEEK } \\ \text { AVG } \end{gathered}$ | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $01: 00$ |  | 362 | 328 | 332 | 334 | 339 |  |  | 339 | 1356 |
| 02:00 |  | 214 | 202 | 204 | 243 | 215 |  |  | 215 | 863 |
| 03:00 |  | 140 | 149 | 145 | 149 | 145 |  |  | 145 | 583 |
| 04:00 |  | 128 | 115 | 136 | 118 | 124 |  |  | 124 | 497 |
| 05:00 |  | 180 | 191 | 203 | 224 | 199 |  |  | 199 | 798 |
| 06:00 |  | 558 | 542 | 542 | 490 | 533 |  |  | 533 | 2132 |
| 07:00 |  | 1026 | 1028 | 1121 | 1037 | 1053 |  |  | 1053 | 4212 |
| 08:00 |  | 1457 | 1465 | 1470 | 1494 | 1471 |  |  | 1471 | 5896 |
| 09:00 |  | 1526 | 1596 | 1536 | 1554 | 1553 |  |  | 1553 | 6212 |
| 10:00 |  | 1393 | 1446 | 1373 | 1461 | 1418 |  |  | 1418 | 5673 |
| 11:00 |  | 1565 | 1495 | 1428 |  | 1496 |  |  | 1496 | 4488 |
| 12:00 | 1596 | 1578 | 1612 | 1511 |  | 1574 |  |  | 1574 | 6297 |
| 13:00 | 1694 | 1723 | 1630 | 1773 |  | 1705 |  |  | 1705 | 6820 |
| 14:00 | 1843 | 1909 | 1879 | 2000 |  | 1907 |  |  | 1907 | 7631 |
| 15:00 | 2389 | 2500 | 2406 | 2534 |  | 2457 |  |  | 2457 | 9829 |
| 16:00 | 2701 | 2832 | 2642 | 2765 |  | 2735 |  |  | 2735 | 10940 |
| 17:00 | 2632 | 2664 | 2708 | 2724 |  | 2682 |  |  | 2682 | 10728 |
| 18:00 | 2654 | 2575 | 2493 | 2726 |  | 2612 |  |  | 2612 | 10448 |
| 19:00 | 2465 | 2607 | 2610 | 2628 |  | 2577 |  |  | 2577 | 10310 |
| 20:00 | 1620 | 1728 | 2058 | 2210 |  | 1904 |  |  | 1904 | 7616 |
| 21:00 | 1192 | 1203 | 1429 | 1383 |  | 1301 |  |  | 1301 | 5207 |
| 22:00 | 889 | 1271 | 1110 | 1039 |  | 1077 |  |  | 1077 | 4309 |
| 23:00 | 616 | 733 | 712 | 755 |  | 704 |  |  | 704 | 2816 |
| 24:00 | 546 | 631 | 616 | 629 |  | 605 |  |  | 605 | 2422 |
| TOTALS | 22837 | 32503 | 32462 | 33167 | 7104 | 32386 | 0 | 0 | 32386 | 128073 |
| \% AVG WKDY | 70.5 | 100.3 | 100.2 | 102.4 | 21.9 |  |  |  |  |  |
| \% AVG WEEK | 70.5 | 100.3 | 100.2 | 102.4 | 21.9 |  |  |  |  |  |
| AM Times | 12:00 | 12:00 | 12:00 | 09:00 | 09:00 | 12:00 |  |  | 12:00 |  |
| AM Peaks | 1596 | 1578 | 1612 | 1536 | 1554 | 1574 |  |  | 1574 |  |
| PM Times | 16:00 | 16:00 | 17:00 | 16:00 |  | 16:00 |  |  | 16:00 |  |
| PM Peaks | 2701 | 2832 | 2708 | 2765 |  | 2735 |  |  | 2735 |  |
| D\% | 100 | 100 | 100 | 100 | 100 |  |  |  |  |  |
| K\% | 12 | 9 | 8 | 8 |  |  |  |  |  |  |

Appendix B

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 6227 _NB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | YANKEE DIVISION HIGHWAY |
| Loc On Alias |  |
| Direction | NB |
| County | NORFOLK |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID | 189014800900 |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Mon 11/9/2015 |
| End Date | Tue 11/10/2015 |
| Start Time | $12: 00: 00$ AM |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Station | 100000000475 |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| INTERVAL:60-MIIN |  |
| :---: | :---: |
| Time | Hourly Count |
| (1) 0:00-1:00 | 540 |
| 1:00-2:00 | 367 |
| 2:00-3:00 | 357 |
| 3:00-4:00 | 427 |
| 4:00-5:00 | 1,094 |
| 5:00-6:00 | 4,202 |
| 6:00-7:00 | 7,314 |
| 7:00-8:00 | 7,559 |
| 8:00-9:00 | 7,292 |
| 9:00-10:00 | 6,194 |
| 10:00-11:00 | 4,983 |
| 11:00-12:00 | 4,900 |
| 12:00-13:00 | 5,081 |
| 13:00-14:00 | 5,212 |
| 14:00-15:00 | 5,847 |
| 15:00-16:00 | 5,741 |
| 16:00-17:00 | 5,133 |
| 17:00-18:00 | 5,315 |
| 18:00-19:00 | 4,653 |
| 19:00-20:00 | 3,225 |
| 20:00-21:00 | 2,582 |
| 21:00-22:00 | 2,094 |
| 22:00-23:00 | 1,565 |
| 23:00-24:00 (i) | 1,008 |
| Total | 92,685 |
| AADT | 84,494 |
| AM Peak | $\begin{array}{r} \hline 07: 00-08: 00 \\ 7,559 \end{array}$ |
| PM Peak | $\begin{array}{r} 14: 00-15: 00 \\ 5,847 \\ \hline \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 6227 _SB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | YANKEE DIVISION HIGHWAY |
| Loc On Alias |  |
| Direction | SB |
| County | NORFOLK |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID | 189014800900 |
| Agency | MHD |


| INTERVAL:60-MIN |  |
| :---: | :---: |
| Time | Hourly Count |
| (1) 0:00-1:00 | 679 |
| 1:00-2:00 | 487 |
| 2:00-3:00 | 386 |
| 3:00-4:00 | 485 |
| 4:00-5:00 | 1,197 |
| 5:00-6:00 | 2,823 |
| 6:00-7:00 | 3,918 |
| 7:00-8:00 | 4,868 |
| 8:00-9:00 | 4,969 |
| 9:00-10:00 | 4,517 |
| 10:00-11:00 | 4,335 |
| 11:00-12:00 | 4,233 |
| 12:00-13:00 | 4,588 |
| 13:00-14:00 | 4,787 |
| 14:00-15:00 | 5,669 |
| 15:00-16:00 | 6,869 |
| 16:00-17:00 | 6,770 |
| 17:00-18:00 | 7,036 |
| 18:00-19:00 | 6,085 |
| 19:00-20:00 | 3,547 |
| 20:00-21:00 | 2,795 |
| 21:00-22:00 | 2,250 |
| 22:00-23:00 | 1,588 |
| 23:00-24:00 © | 1,214 |
| Total | 86,095 |
| AADT | 78,486 |
| AM Peak | $\begin{array}{r} \hline 08: 00-09: 00 \\ 4,969 \\ \hline \end{array}$ |
| PM Peak | $\begin{array}{r} 17: 00-18: 00 \\ 7,036 \\ \hline \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 4065 _NB |
| Type | SPOT |
| Fnct'l Class | 1 |
| Located On | YANKEE DIVISION HIGHWAY |
| SOUTH OF | RAMP-RT 2 EB TO RT 95 SB |
| Direction | NB |
| County | MIDDLESEX |
| Community | LEXINGTON |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| INTERVAL:60-MIN |  |
| :---: | :---: |
| Time | Hourly Count |
| (1) 0:00-1:00 | 473 |
| 1:00-2:00 | 287 |
| 2:00-3:00 | 191 |
| 3:00-4:00 | 236 |
| 4:00-5:00 | 599 |
| 5:00-6:00 | 2,498 |
| 6:00-7:00 | 5,407 |
| 7:00-8:00 | 6,650 |
| 8:00-9:00 | 6,405 |
| 9:00-10:00 | 5,812 |
| 10:00-11:00 | 5,011 |
| 11:00-12:00 | 4,999 |
| 12:00-13:00 | 5,211 |
| 13:00-14:00 | 5,630 |
| 14:00-15:00 | 6,891 |
| 15:00-16:00 | 7,210 |
| 16:00-17:00 | 7,320 |
| 17:00-18:00 | 7,291 |
| 18:00-19:00 | 6,405 |
| 19:00-20:00 | 4,756 |
| 20:00-21:00 | 3,267 |
| 21:00-22:00 | 2,468 |
| 22:00-23:00 | 1,634 |
| 23:00-24:00 (-) | 968 |
| Total | 97,619 |
| AM Peak | $\begin{array}{r} \hline 07: 00-08: 00 \\ 6,650 \end{array}$ |
| PM Peak | $\begin{array}{r} \hline 16: 00-17: 00 \\ 7,320 \\ \hline \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | H8456_SB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | I-93 |
| Loc On Alias | I-93, 0.3 mile N. of West St |
| Direction | SB |
| County | MIDDLESEX |
| Community |  |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| INTERVAL:15-MIN |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Time | 15-min Interval |  |  |  | Hourly Count |
|  | 1st | 2nd | 3rd | 4th |  |
| (1) 0:00-1:00 | 144 | 125 | 129 | 92 | 490 |
| 1:00-2:00 | 89 | 110 | 112 | 112 | 423 |
| 2:00-3:00 | 112 | 118 | 104 | 135 | 469 |
| 3:00-4:00 | 128 | 170 | 225 | 232 | 755 |
| 4:00-5:00 | 278 | 392 | 537 | 679 | 1,886 |
| 5:00-6:00 | 1,095 | 1,624 | 1,692 | 1,771 | 6,182 |
| 6:00-7:00 | 1,750 | 1,746 | 1,758 | 1,750 | 7,004 |
| 7:00-8:00 | 1,785 | 1,837 | 1,791 | 1,727 | 7,140 |
| 8:00-9:00 | 1,727 | 1,675 | 1,725 | 1,757 | 6,884 |
| 9:00-10:00 | 1,780 | 1,532 | 1,608 | 1,503 | 6,423 |
| 10:00-11:00 | 1,421 | 1,407 | 1,408 | 1,312 | 5,548 |
| 11:00-12:00 | 1,270 | 1,244 | 1,291 | 1,042 | 4,847 |
| 12:00-13:00 | 1,155 | 1,363 | 1,278 | 1,198 | 4,994 |
| 13:00-14:00 | 1,106 | 1,176 | 1,240 | 1,251 | 4,773 |
| 14:00-15:00 | 1,357 | 1,328 | 1,370 | 1,369 | 5,424 |
| 15:00-16:00 | 1,299 | 1,304 | 1,345 | 1,407 | 5,355 |
| 16:00-17:00 | 1,301 | 1,470 | 1,575 | 1,598 | 5,944 |
| 17:00-18:00 | 1,783 | 1,800 | 1,753 | 1,698 | 7,034 |
| 18:00-19:00 | 1,526 | 1,398 | 1,347 | 1,276 | 5,547 |
| 19:00-20:00 | 1,087 | 884 | 844 | 808 | 3,623 |
| 20:00-21:00 | 803 | 723 | 699 | 634 | 2,859 |
| 21:00-22:00 | 584 | 595 | 481 | 458 | 2,118 |
| 22:00-23:00 | 451 | 371 | 381 | 354 | 1,557 |
| 23:00-24:00 © | 304 | 254 | 251 | 207 | 1,016 |
| Total |  |  |  |  | 98,295 |
| AM Peak |  |  |  |  | $\begin{array}{r} 45-07: 45 \\ 7,163 \end{array}$ |
| PM Peak |  |  |  |  | $\begin{array}{r} \hline 00-18: 00 \\ 7,034 \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | H8516_SB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | I-95 |
| Loc On Alias | I-95, 280 feet N. of Washington St |
| Direction | SB |
| County | MIDDLESEX |
| Community |  |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| INTERVAL:15-MIN |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Time | 15-min Interval |  |  |  | Hourly Count |
|  | 1st | 2nd | 3rd | 4th |  |
| (1) 0:00-1:00 | 241 | 210 | 218 | 213 | 882 |
| 1:00-2:00 | 120 | 157 | 152 | 168 | 597 |
| 2:00-3:00 | 164 | 157 | 166 | 154 | 641 |
| 3:00-4:00 | 247 | 165 | 163 | 241 | 816 |
| 4:00-5:00 | 235 | 329 | 367 | 470 | 1,401 |
| 5:00-6:00 | 629 | 940 | 1,395 | 1,629 | 4,593 |
| 6:00-7:00 | 1,855 | 2,077 | 2,180 | 2,090 | 8,202 |
| 7:00-8:00 | 2,000 | 2,017 | 1,912 | 1,979 | 7,908 |
| 8:00-9:00 | 1,972 | 1,947 | 1,995 | 2,117 | 8,031 |
| 9:00-10:00 | 2,033 | 1,996 | 2,039 | 2,010 | 8,078 |
| 10:00-11:00 | 1,856 | 1,809 | 1,745 | 1,732 | 7,142 |
| 11:00-12:00 | 1,742 | 1,691 | 1,699 | 1,747 | 6,879 |
| 12:00-13:00 | 1,733 | 1,794 | 1,813 | 1,702 | 7,042 |
| 13:00-14:00 | 1,684 | 1,719 | 1,685 | 1,668 | 6,756 |
| 14:00-15:00 | 1,790 | 1,895 | 1,840 | 1,841 | 7,366 |
| 15:00-16:00 | 1,794 | 1,701 | 1,688 | 1,683 | 6,866 |
| 16:00-17:00 | 1,572 | 1,612 | 1,654 | 1,628 | 6,466 |
| 17:00-18:00 | 1,612 | 1,566 | 1,561 | 1,524 | 6,263 |
| 18:00-19:00 | 1,379 | 1,543 | 1,480 | 1,317 | 5,719 |
| 19:00-20:00 | 1,239 | 1,177 | 1,168 | 1,003 | 4,587 |
| 20:00-21:00 | 841 | 885 | 804 | 794 | 3,324 |
| 21:00-22:00 | 764 | 695 | 606 | 589 | 2,654 |
| 22:00-23:00 | 522 | 518 | 466 | 461 | 1,967 |
| 23:00-24:00 © | 380 | 457 | 372 | 263 | 1,472 |
| Total |  |  |  |  | 115,652 |
| AM Peak |  |  |  |  | $\begin{array}{r} 15-07: 15 \\ 8,347 \end{array}$ |
| PM Peak |  |  |  |  | $\begin{array}{r} 15-15: 15 \\ 7,370 \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22546 |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | 24 |
|  | Route 139 EB On-Ramp |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000000057 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| (1) 0:00-1:00 | 5 | 3 | 11 | 6 | 25 |
| 1:00-2:00 | 1 | 5 | 4 | 3 | 13 |
| 2:00-3:00 | 5 | 1 | 10 | 3 | 19 |
| 3:00-4:00 | 7 | 5 | 4 | 7 | 23 |
| 4:00-5:00 | 7 | 10 | 9 | 17 | 43 |
| 5:00-6:00 | 24 | 45 | 50 | 66 | 185 |
| 6:00-7:00 | 101 | 93 | 97 | 109 | 400 |
| 7:00-8:00 | 111 | 100 | 108 | 68 | 387 |
| 8:00-9:00 | 90 | 88 | 112 | 95 | 385 |
| 9:00-10:00 | 106 | 98 | 75 | 114 | 393 |
| 10:00-11:00 | 79 | 100 | 96 | 102 | 377 |
| 11:00-12:00 | 103 | 91 | 106 | 118 | 418 |
| 12:00-13:00 | 105 | 122 | 105 | 114 | 446 |
| 13:00-14:00 | 115 | 125 | 107 | 96 | 443 |
| 14:00-15:00 | 100 | 117 | 114 | 76 | 407 |
| 15:00-16:00 | 92 | 88 | 108 | 94 | 382 |
| 16:00-17:00 | 116 | 73 | 114 | 96 | 399 |
| 17:00-18:00 | 141 | 103 | 81 | 73 | 398 |
| 18:00-19:00 | 89 | 73 | 74 | 84 | 320 |
| 19:00-20:00 | 72 | 63 | 63 | 46 | 244 |
| 20:00-21:00 | 56 | 62 | 58 | 52 | 228 |
| 21:00-22:00 | 40 | 47 | 41 | 39 | 167 |
| 22:00-23:00 | 48 | 37 | 25 | 33 | 143 |
| 23:00-24:00 (i) | 19 | 20 | 17 | 24 | 80 |
| Total |  |  |  |  | 6,325 |
| AADT |  |  |  |  | 5,766 |
| AM Peak | 11:30-12:30 |  |  |  |  |
| PM Peak |  |  |  |  | $\begin{array}{r} 45-13: 45 \\ 461 \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22548 |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | 24 |
|  | Route 139 WB On-Ramp |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000000766 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| (3) 0:00-1:00 | 4 | 11 | 21 | 6 | 42 |
| 1:00-2:00 | 7 | 10 | 9 | 4 | 30 |
| 2:00-3:00 | 10 | 17 | 17 | 12 | 56 |
| 3:00-4:00 | 14 | 8 | 12 | 19 | 53 |
| 4:00-5:00 | 9 | 11 | 25 | 32 | 77 |
| 5:00-6:00 | 39 | 73 | 74 | 95 | 281 |
| 6:00-7:00 | 89 | 109 | 96 | 119 | 413 |
| 7:00-8:00 | 114 | 107 | 91 | 76 | 388 |
| 8:00-9:00 | 88 | 66 | 81 | 75 | 310 |
| 9:00-10:00 | 100 | 85 | 75 | 75 | 335 |
| 10:00-11:00 | 73 | 74 | 78 | 47 | 272 |
| 11:00-12:00 | 71 | 66 | 61 | 61 | 259 |
| 12:00-13:00 | 69 | 72 | 71 | 65 | 277 |
| 13:00-14:00 | 82 | 90 | 91 | 84 | 347 |
| 14:00-15:00 | 83 | 82 | 76 | 91 | 332 |
| 15:00-16:00 | 88 | 73 | 117 | 59 | 337 |
| 16:00-17:00 | 75 | 83 | 100 | 88 | 346 |
| 17:00-18:00 | 96 | 87 | 75 | 60 | 318 |
| 18:00-19:00 | 91 | 68 | 61 | 44 | 264 |
| 19:00-20:00 | 51 | 58 | 58 | 37 | 204 |
| 20:00-21:00 | 43 | 40 | 52 | 28 | 163 |
| 21:00-22:00 | 59 | 34 | 57 | 53 | 203 |
| 22:00-23:00 | 30 | 32 | 36 | 19 | 117 |
| 23:00-24:00 (i) | 30 | 17 | 11 | 11 | 69 |
| Total |  |  |  |  | 5,493 |
| AADT |  |  |  |  | 5,008 |
| AM Peak | $\begin{array}{r} 06: 15-07: 15 \\ 438 \end{array}$ |  |  |  |  |
| PM Peak | $\begin{array}{r} \hline 16: 30-17: 30 \\ 371 \end{array}$ |  |  |  |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | H8462_NB |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | SR-24 |
| Loc On Alias | SR-24, 1.0 mile N. of Lindelof Ave <br> (Rt. 139) |
| Direction | NB |
| Community |  |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Wed 3/29/2017 |
| End Date | Thu 3/30/2017 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | H8462 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type |  |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| (B) 0:00-1:00 | 120 | 96 | 97 | 68 | 381 |
| 1:00-2:00 | 64 | 100 | 90 | 85 | 339 |
| 2:00-3:00 | 69 | 77 | 76 | 69 | 291 |
| 3:00-4:00 | 81 | 120 | 132 | 137 | 470 |
| 4:00-5:00 | 220 | 323 | 425 | 652 | 1,620 |
| 5:00-6:00 | 995 | 1,196 | 1,290 | 1,205 | 4,686 |
| 6:00-7:00 | 1,168 | 1,201 | 1,182 | 1,115 | 4,666 |
| 7:00-8:00 | 1,192 | 1,087 | 1,140 | 1,110 | 4,529 |
| 8:00-9:00 | 1,076 | 1,162 | 1,137 | 1,167 | 4,542 |
| 9:00-10:00 | 1,124 | 1,042 | 1,031 | 962 | 4,159 |
| 10:00-11:00 | 888 | 886 | 829 | 842 | 3,445 |
| 11:00-12:00 | 801 | 855 | 931 | 872 | 3,459 |
| 12:00-13:00 | 868 | 874 | 875 | 860 | 3,477 |
| 13:00-14:00 | 770 | 904 | 860 | 807 | 3,341 |
| 14:00-15:00 | 901 | 911 | 904 | 830 | 3,546 |
| 15:00-16:00 | 790 | 847 | 926 | 801 | 3,364 |
| 16:00-17:00 | 800 | 799 | 837 | 842 | 3,278 |
| 17:00-18:00 | 848 | 880 | 825 | 819 | 3,372 |
| 18:00-19:00 | 774 | 661 | 603 | 542 | 2,580 |
| 19:00-20:00 | 579 | 520 | 550 | 448 | 2,097 |
| 20:00-21:00 | 475 | 459 | 451 | 396 | 1,781 |
| 21:00-22:00 | 379 | 411 | 348 | 260 | 1,398 |
| 22:00-23:00 | 274 | 372 | 314 | 239 | 1,199 |
| 23:00-24:00 ( | 232 | 181 | 164 | 144 | 721 |
| Total |  |  |  |  | 62,741 |
| AM Peak |  |  |  | 05:30 | $\begin{array}{r} 30-06: 30 \\ 4,864 \\ \hline \end{array}$ |
| PM Peak |  |  |  | 14:0 | $\begin{array}{r} \hline 0-15: 00 \\ 3,546 \\ \hline \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22545 |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | 24 |
|  | Exit 20A Route 139 East Randolph |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000000402 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| ( ${ }^{\text {( }}$ :000-1:00 | 18 | 7 | 11 | 6 | 42 |
| 1:00-2:00 | 8 | 5 | 10 | 8 | 31 |
| 2:00-3:00 | 4 | 4 | 6 | 11 | 25 |
| 3:00-4:00 | 7 | 5 | 6 | 6 | 24 |
| 4:00-5:00 | 7 | 14 | 18 | 24 | 63 |
| 5:00-6:00 | 40 | 57 | 66 | 59 | 222 |
| 6:00-7:00 | 59 | 58 | 92 | 85 | 294 |
| 7:00-8:00 | 86 | 104 | 142 | 181 | 513 |
| 8:00-9:00 | 199 | 177 | 152 | 124 | 652 |
| 9:00-10:00 | 81 | 64 | 70 | 67 | 282 |
| 10:00-11:00 | 64 | 72 | 76 | 79 | 291 |
| 11:00-12:00 | 82 | 91 | 65 | 86 | 324 |
| 12:00-13:00 | 80 | 64 | 88 | 79 | 311 |
| 13:00-14:00 | 71 | 92 | 74 | 94 | 331 |
| 14:00-15:00 | 68 | 86 | 104 | 95 | 353 |
| 15:00-16:00 | 78 | 88 | 99 | 120 | 385 |
| 16:00-17:00 | 103 | 103 | 90 | 79 | 375 |
| 17:00-18:00 | 87 | 109 | 106 | 98 | 400 |
| 18:00-19:00 | 90 | 78 | 80 | 65 | 313 |
| 19:00-20:00 | 67 | 69 | 63 | 72 | 271 |
| 20:00-21:00 | 70 | 55 | 70 | 43 | 238 |
| 21:00-22:00 | 47 | 38 | 46 | 25 | 156 |
| 22:00-23:00 | 37 | 19 | 18 | 27 | 101 |
| 23:00-24:00 (i) | 12 | 17 | 18 | 16 | 63 |
| Total |  |  |  |  | 6,060 |
| AADT |  |  |  |  | 5,524 |
| AM Peak | $\begin{array}{r} \hline 07: 45-08: 45 \\ 709 \end{array}$ |  |  |  |  |
| PM Peak | $\begin{array}{r} 15: 30-16: 30 \\ 425 \end{array}$ |  |  |  |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22547 |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | 24 |
|  | Exit 20B Route 139 West Stoughton |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| INTERVAL:15-MIN |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Time | 15-min Interval |  |  |  | Hourly Count |
|  | 1st | 2nd | 3rd | 4th |  |
| (1) 0:00-1:00 | 2 | 2 | 0 | 1 | 5 |
| 1:00-2:00 | 2 | 1 | 1 | 0 | 4 |
| 2:00-3:00 | 0 | 0 | 2 | 1 | 3 |
| 3:00-4:00 | 2 | 4 | 1 | 0 | 7 |
| 4:00-5:00 | 1 | 4 | 3 | 8 | 16 |
| 5:00-6:00 | 22 | 15 | 14 | 9 | 60 |
| 6:00-7:00 | 5 | 8 | 20 | 13 | 46 |
| 7:00-8:00 | 23 | 24 | 35 | 49 | 131 |
| 8:00-9:00 | 60 | 50 | 34 | 35 | 179 |
| 9:00-10:00 | 29 | 31 | 32 | 22 | 114 |
| 10:00-11:00 | 27 | 21 | 22 | 34 | 104 |
| 11:00-12:00 | 26 | 21 | 24 | 25 | 96 |
| 12:00-13:00 | 35 | 26 | 23 | 28 | 112 |
| 13:00-14:00 | 31 | 20 | 21 | 21 | 93 |
| 14:00-15:00 | 22 | 19 | 16 | 24 | 81 |
| 15:00-16:00 | 25 | 20 | 16 | 31 | 92 |
| 16:00-17:00 | 33 | 31 | 24 | 27 | 115 |
| 17:00-18:00 | 31 | 25 | 40 | 24 | 120 |
| 18:00-19:00 | 27 | 22 | 23 | 29 | 101 |
| 19:00-20:00 | 22 | 14 | 29 | 16 | 81 |
| 20:00-21:00 | 6 | 11 | 14 | 18 | 49 |
| 21:00-22:00 | 5 | 5 | 5 | 4 | 19 |
| 22:00-23:00 | 5 | 3 | 3 | 5 | 16 |
| 23:00-24:00 (1) | 1 | 3 | 1 | 4 | 9 |
| Total |  |  |  |  | 1,653 |
| AADT |  |  |  |  | 1,507 |
| AM Peak |  |  |  |  | $\begin{array}{r} 30-08: 30 \\ 194 \end{array}$ |
| PM Peak |  |  |  |  | $\begin{array}{r} 45-17: 45 \\ 123 \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | $6278 \_$NB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | INTERSTATE 93 |
| Loc On Alias |  |
|  | BTWN. RTES.24 \& 28 |
| Direction | NB |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID | 244021801220 |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 11/10/2015 |
| End Date | Wed 11/11/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 100000000624 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| TNTERVAL:60-MIN |  |
| :---: | ---: |
| Time | Hourly <br> Count |
| $\mathbf{0 : 0 0 - 1 : 0 0}$ | 1,053 |
| $\mathbf{1 : 0 0 - 2 : 0 0}$ | 532 |
| $\mathbf{2 : 0 0 - 3 : 0 0}$ | 434 |
| $\mathbf{3 : 0 0 - 4 : 0 0}$ | 417 |
| $\mathbf{4 : 0 0 - 5 : 0 0}$ | 1,027 |
| $\mathbf{5 : 0 0 - 6 : 0 0}$ | 3,348 |
| $\mathbf{6 : 0 0 - 7 : 0 0}$ | 6,648 |
| $\mathbf{7 : 0 0 - 8 : 0 0}$ | 7,256 |
| $\mathbf{8 : 0 0 - 9 : 0 0}$ | 6,780 |
| $\mathbf{9 : 0 0 - 1 0 : 0 0}$ | 5,852 |
| $\mathbf{1 0 : 0 0 - 1 1 : 0 0}$ | 5,438 |
| $\mathbf{1 1 : 0 0 - 1 2 : 0 0}$ | 5,345 |
| $\mathbf{1 2 : 0 0 - 1 3 : 0 0}$ | 5,885 |
| $\mathbf{1 3 : 0 0 - 1 4 : 0 0}$ | 6,618 |
| $\mathbf{1 4 : 0 0 - 1 5 : 0 0}$ | 7,192 |
| $\mathbf{1 5 : 0 0 - 1 6 : 0 0}$ | 6,063 |
| $\mathbf{1 6 : 0 0 - 1 7 : 0 0}$ | 6,227 |
| $\mathbf{1 7 : 0 0 - 1 8 : 0 0}$ | 6,532 |
| $\mathbf{1 8 : 0 0 - 1 9 : 0 0}$ | 5,999 |
| $\mathbf{1 9 : 0 0 - 2 0 : 0 0}$ | 4,987 |
| $\mathbf{2 0 : 0 0 - 2 1 : 0 0}$ | 3,911 |
| $\mathbf{2 1 : 0 0 - 2 2 : 0 0}$ | 3,176 |
| $\mathbf{2 2 : 0 0 - 2 3 : 0 0}$ | 2,508 |
| $\mathbf{2 3 : 0 0 - 2 4 : 0 0}$ | 1,796 |
| Total | 105,024 |
| AADT | 92,306 |
|  | 7,256 |
|  | 792 |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 252107_SB |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | RAMP-RT 93 NB TO RT 24 SB |
|  | INTERSTATE 93 |
| Direction | SB |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 9/20/2005 |
| End Date | Wed 9/21/2005 |
| Start Time | $5: 15: 00 \mathrm{AM}$ |
| End Time | $5: 15: 00 \mathrm{AM}$ |
| Direction | 2 |
| Notes |  |
| Count Source |  |
| Weather |  |
| Study | MassHighway Special Counts |
| Speed Limit |  |
| Description |  |
| Sensor Type |  |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| 0:00-1:00 | 91 | 92 | 62 | 58 | 303 |
| 1:00-2:00 | 36 | 44 | 25 | 30 | 135 |
| 2:00-3:00 | 34 | 36 | 37 | 27 | 134 |
| 3:00-4:00 | 31 | 21 | 30 | 33 | 115 |
| 4:00-5:00 | 30 | 51 | 40 | 48 | 169 |
| (1) 5:00-6:00 | 68 | 97 | 138 | 155 | 458 |
| 6:00-7:00 | 169 | 221 | 297 | 359 | 1,046 |
| 7:00-8:00 | 349 | 392 | 440 | 399 | 1,580 |
| 8:00-9:00 | 362 | 392 | 341 | 378 | 1,473 |
| 9:00-10:00 | 317 | 342 | 333 | 342 | 1,334 |
| 10:00-11:00 | 358 | 372 | 318 | 371 | 1,419 |
| 11:00-12:00 | 334 | 315 | 354 | 343 | 1,346 |
| 12:00-13:00 | 330 | 309 | 369 | 348 | 1,356 |
| 13:00-14:00 | 378 | 404 | 399 | 356 | 1,537 |
| 14:00-15:00 | 392 | 454 | 472 | 513 | 1,831 |
| 15:00-16:00 | 639 | 683 | 727 | 713 | 2,762 |
| 16:00-17:00 | 745 | 748 | 774 | 730 | 2,997 |
| 17:00-18:00 | 692 | 771 | 723 | 694 | 2,880 |
| 18:00-19:00 | 591 | 551 | 512 | 479 | 2,133 |
| 19:00-20:00 | 387 | 371 | 333 | 289 | 1,380 |
| 20:00-21:00 | 238 | 224 | 256 | 223 | 941 |
| 21:00-22:00 | 220 | 194 | 197 | 162 | 773 |
| 22:00-23:00 | 155 | 134 | 125 | 115 | 529 |
| 23:00-24:00 | 115 | 134 | 132 | 93 | 474 |
| Total |  |  |  |  | 29,105 |
| AM Peak | $\begin{array}{r} \hline 07: 15-08: 15 \\ 1,593 \end{array}$ |  |  |  |  |
| PM Peak | $\begin{array}{r} 16: 00-17: 00 \\ 2,997 \end{array}$ |  |  |  |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 6227 _NB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | YANKEE DIVISION HIGHWAY |
| Loc On Alias |  |
|  | BETWEEN RTE.24 AND <br> PONKAPOAG RD. |
| Direction | NB |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID | 189014800900 |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 11/10/2015 |
| End Date | Wed 11/11/2015 |
| Start Time | $12: 00: 00$ AM |
| End Time | $12: 00: 00$ AM |
| Direction |  |
| Notes |  |
| Count Source | 100000000475 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| INTERVAL:60-MIN |  |
| :---: | :---: |
| Time | Hourly Count |
| (1) 0:00-1:00 | 687 |
| 1:00-2:00 | 329 |
| 2:00-3:00 | 351 |
| 3:00-4:00 | 438 |
| 4:00-5:00 | 1,135 |
| 5:00-6:00 | 4,609 |
| 6:00-7:00 | 7,608 |
| 7:00-8:00 | 7,802 |
| 8:00-9:00 | 7,551 |
| 9:00-10:00 | 6,250 |
| 10:00-11:00 | 5,213 |
| 11:00-12:00 | 5,012 |
| 12:00-13:00 | 5,076 |
| 13:00-14:00 | 5,501 |
| 14:00-15:00 | 6,031 |
| 15:00-16:00 | 5,166 |
| 16:00-17:00 | 5,238 |
| 17:00-18:00 | 5,525 |
| 18:00-19:00 | 4,604 |
| 19:00-20:00 | 3,619 |
| 20:00-21:00 | 2,835 |
| 21:00-22:00 | 2,300 |
| 22:00-23:00 | 1,890 |
| 23:00-24:00 (i) | 1,174 |
| Total | 95,944 |
| AADT | 84,325 |
| AM Peak | $\begin{array}{r} \hline 07: 00-08: 00 \\ 7,802 \\ \hline \end{array}$ |
| PM Peak | $\begin{array}{r} 14: 00-15: 00 \\ 6,031 \\ \hline \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 691 _SB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | YANKEE DIVISION HIGHWAY |
| NORTH OF | RTE.28 |
| Direction | SB |
| Community | QUINCY |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 3/7/2017 |
| End Date | Wed 3/8/2017 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000069102 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type |  |


| INTERVAL:60-MIN |  |
| :---: | ---: |
| Time | Hourly <br> Count |
| $\mathbf{0 : 0 0 - 1 : 0 0}$ | 1,028 |
| $\mathbf{1 : 0 0 - 2 : 0 0}$ | 535 |
| $\mathbf{2 : 0 0 - 3 : 0 0}$ | 408 |
| $\mathbf{3 : 0 0 - 4 : 0 0}$ | 413 |
| $\mathbf{4 : 0 0 - 5 : 0 0}$ | 872 |
| $\mathbf{5 : 0 0 - 6 : 0 0}$ | 2,849 |
| $\mathbf{6 : 0 0 - 7 : 0 0}$ | 5,916 |
| $\mathbf{7 : 0 0 - 8 : 0 0}$ | 6,583 |
| $\mathbf{8 : 0 0 - 9 : 0 0}$ | 6,513 |
| $\mathbf{9 : 0 0 - 1 0 : 0 0}$ | 5,579 |
| $\mathbf{1 0 : 0 0 - 1 1 : 0 0}$ | 5,019 |
| $\mathbf{1 1 : 0 0 - 1 2 : 0 0}$ | 5,483 |
| $\mathbf{1 2 : 0 0 - 1 3 : 0 0}$ | 5,864 |
| $\mathbf{1 3 : 0 0 - 1 4 : 0 0}$ | 6,085 |
| $\mathbf{1 4 : 0 0 - 1 5 : 0 0}$ | 6,872 |
| $\mathbf{1 5 : 0 0 - 1 6 : 0 0}$ | 6,720 |
| $\mathbf{1 6 : 0 0 - 1 7 : 0 0}$ | 5,795 |
| $\mathbf{1 7 : 0 0 - 1 8 : 0 0}$ | 5,950 |
| $\mathbf{1 8 : 0 0 - 1 9 : 0 0}$ | 5,871 |
| $\mathbf{1 9 : 0 0 - 2 0 : 0 0}$ | 5,170 |
| $\mathbf{2 0 : 0 0 - 2 1 : 0 0}$ | 4,056 |
| $\mathbf{2 1 : 0 0 - 2 2 : 0 0}$ | 3,301 |
| $\mathbf{2 2 : 0 0 - 2 3 : 0 0}$ | 2,380 |
| $\mathbf{2 3 : 0 0 - 2 4 : 0 0}$ | 1,856 |
| Total | 101,118 |
| AM Peak | $07: 00-08: 00$ |
| 6,583 |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 6227 _SB |
| Type | SPOT |
| Fnct'I Class | 1 |
| Located On | YANKEE DIVISION HIGHWAY |
| Loc On Alias |  |
|  | BETWEEN RTE.24 AND <br> PONKAPOAG RD. |
| Direction | SB |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID | 189014800900 |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 11/10/2015 |
| End Date | Wed 11/11/2015 |
| Start Time | $12: 00: 00$ AM |
| End Time | $12: 00: 00$ AM |
| Direction |  |
| Notes |  |
| Count Source | 000000000988 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| TNTERVAL:60-MIN |  |
| :---: | ---: |
| Time | Hourly <br> Count |
| $\mathbf{0 : 0 0 - 1 : 0 0}$ | 688 |
| $\mathbf{1 : 0 0 - 2 : 0 0}$ | 437 |
| $\mathbf{2 : 0 0 - 3 : 0 0}$ | 373 |
| $\mathbf{3 : 0 0 - 4 : 0 0}$ | 516 |
| $\mathbf{4 : 0 0 - 5 : 0 0}$ | 1,246 |
| $\mathbf{5 : 0 0 - 6 : 0 0}$ | 2,788 |
| $\mathbf{6 : 0 0 - 7 : 0 0}$ | 3,834 |
| $\mathbf{7 : 0 0 - 8 : 0 0}$ | 5,000 |
| $\mathbf{8 : 0 0 - 9 : 0 0}$ | 4,913 |
| $\mathbf{9 : 0 0 - 1 0 : 0 0}$ | 4,530 |
| $\mathbf{1 0 : 0 0 - 1 1 : 0 0}$ | 4,358 |
| $\mathbf{1 1 : 0 0 - 1 2 : 0 0}$ | 4,390 |
| $\mathbf{1 2 : 0 0 - 1 3 : 0 0}$ | 5,005 |
| $\mathbf{1 3 : 0 0 - 1 4 : 0 0}$ | 5,149 |
| $\mathbf{1 4 : 0 0 - 1 5 : 0 0}$ | 5,954 |
| $\mathbf{1 5 : 0 0 - 1 6 : 0 0}$ | 6,507 |
| $\mathbf{1 6 : 0 0 - 1 7 : 0 0}$ | 6,937 |
| $\mathbf{1 7 : 0 0 - 1 8 : 0 0}$ | 6,770 |
| $\mathbf{1 8 : 0 0 - 1 9 : 0 0}$ | 6,388 |
| $\mathbf{1 9 : 0 0 - 2 0 : 0 0}$ | 4,294 |
| $\mathbf{2 0 : 0 0 - 2 1 : 0 0}$ | 3,029 |
| $\mathbf{2 1 : 0 0 - 2 2 : 0 0}$ | 2,546 |
| $\mathbf{2 2 : 0 0 - 2 3 : 0 0}$ | 1,846 |
| $\mathbf{2 3 : 0 0 - 2 4 : 0 0}$ | 1,311 |
| Total | 88,809 |
| AADT | 78,054 |
| Peak | $16: 00-17: 00$ |
| 6,937 |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22554 |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | 24 |
|  | Route 139 EB On-Ramp |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000000595 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| (1) 0:00-1:00 | 4 | 0 | 1 | 3 | 8 |
| 1:00-2:00 | 2 | 0 | 2 | 1 | 5 |
| 2:00-3:00 | 0 | 0 | 1 | 1 | 2 |
| 3:00-4:00 | 3 | 1 | 4 | 0 | 8 |
| 4:00-5:00 | 1 | 1 | 1 | 3 | 6 |
| 5:00-6:00 | 4 | 1 | 13 | 7 | 25 |
| 6:00-7:00 | 9 | 8 | 20 | 21 | 58 |
| 7:00-8:00 | 19 | 28 | 27 | 26 | 100 |
| 8:00-9:00 | 27 | 24 | 30 | 22 | 103 |
| 9:00-10:00 | 13 | 28 | 25 | 24 | 90 |
| 10:00-11:00 | 28 | 32 | 30 | 28 | 118 |
| 11:00-12:00 | 24 | 29 | 33 | 23 | 109 |
| 12:00-13:00 | 39 | 33 | 33 | 39 | 144 |
| 13:00-14:00 | 38 | 41 | 33 | 39 | 151 |
| 14:00-15:00 | 31 | 29 | 31 | 36 | 127 |
| 15:00-16:00 | 51 | 45 | 48 | 44 | 188 |
| 16:00-17:00 | 38 | 42 | 62 | 55 | 197 |
| 17:00-18:00 | 66 | 68 | 49 | 42 | 225 |
| 18:00-19:00 | 53 | 26 | 29 | 30 | 138 |
| 19:00-20:00 | 37 | 21 | 20 | 18 | 96 |
| 20:00-21:00 | 36 | 28 | 27 | 10 | 101 |
| 21:00-22:00 | 19 | 15 | 11 | 16 | 61 |
| 22:00-23:00 | 14 | 13 | 12 | 8 | 47 |
| 23:00-24:00 (i) | 15 | 8 | 3 | 2 | 28 |
| Total |  |  |  |  | 2,135 |
| AADT |  |  |  |  | 1,946 |
| AM Peak | $\begin{array}{r} 11: 30-12: 30 \\ 128 \\ \hline \end{array}$ |  |  |  |  |
| PM Peak | $\begin{array}{r} 16: 30-17: 30 \\ 251 \\ \hline \end{array}$ |  |  |  |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22552 |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | 24 |
|  | Route 139 WB On-Ramp |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000000616 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| (1) 0:00-1:00 | 9 | 19 | 16 | 9 | 53 |
| 1:00-2:00 | 10 | 4 | 5 | 4 | 23 |
| 2:00-3:00 | 5 | 5 | 11 | 5 | 26 |
| 3:00-4:00 | 8 | 6 | 8 | 12 | 34 |
| 4:00-5:00 | 7 | 3 | 4 | 14 | 28 |
| 5:00-6:00 | 17 | 16 | 23 | 22 | 78 |
| 6:00-7:00 | 40 | 62 | 61 | 86 | 249 |
| 7:00-8:00 | 78 | 63 | 81 | 88 | 310 |
| 8:00-9:00 | 65 | 69 | 83 | 71 | 288 |
| 9:00-10:00 | 68 | 78 | 68 | 59 | 273 |
| 10:00-11:00 | 63 | 51 | 66 | 65 | 245 |
| 11:00-12:00 | 59 | 57 | 67 | 69 | 252 |
| 12:00-13:00 | 64 | 79 | 84 | 74 | 301 |
| 13:00-14:00 | 69 | 83 | 83 | 96 | 331 |
| 14:00-15:00 | 108 | 106 | 118 | 117 | 449 |
| 15:00-16:00 | 112 | 118 | 137 | 128 | 495 |
| 16:00-17:00 | 181 | 157 | 169 | 170 | 677 |
| 17:00-18:00 | 162 | 153 | 146 | 99 | 560 |
| 18:00-19:00 | 142 | 115 | 66 | 82 | 405 |
| 19:00-20:00 | 96 | 61 | 65 | 51 | 273 |
| 20:00-21:00 | 66 | 62 | 68 | 71 | 267 |
| 21:00-22:00 | 49 | 40 | 40 | 34 | 163 |
| 22:00-23:00 | 47 | 30 | 39 | 29 | 145 |
| 23:00-24:00 (i) | 41 | 22 | 18 | 14 | 95 |
| Total |  |  |  |  | 6,020 |
| AADT |  |  |  |  | 5,488 |
| AM Peak |  |  |  |  | $\begin{array}{r} 00-08: 00 \\ 310 \\ \hline \end{array}$ |
| PM Peak |  |  |  |  | $\begin{array}{r} \hline 00-17: 00 \\ 677 \\ \hline \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22553 |
| Type | SPOT |
| Fnct'I Class | 3 |
| Located On | 24 |
|  | Exit 20A Route 139 East Randolph |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000000493 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| (1) 0:00-1:00 | 30 | 38 | 32 | 32 | 132 |
| 1:00-2:00 | 29 | 38 | 26 | 32 | 125 |
| 2:00-3:00 | 20 | 17 | 16 | 20 | 73 |
| 3:00-4:00 | 15 | 12 | 12 | 12 | 51 |
| 4:00-5:00 | 12 | 16 | 8 | 33 | 69 |
| 5:00-6:00 | 17 | 31 | 41 | 40 | 129 |
| 6:00-7:00 | 52 | 63 | 88 | 98 | 301 |
| 7:00-8:00 | 90 | 127 | 145 | 131 | 493 |
| 8:00-9:00 | 149 | 157 | 127 | 130 | 563 |
| 9:00-10:00 | 117 | 108 | 99 | 116 | 440 |
| 10:00-11:00 | 94 | 117 | 110 | 128 | 449 |
| 11:00-12:00 | 114 | 164 | 150 | 157 | 585 |
| 12:00-13:00 | 162 | 152 | 145 | 147 | 606 |
| 13:00-14:00 | 172 | 123 | 128 | 185 | 608 |
| 14:00-15:00 | 145 | 175 | 180 | 196 | 696 |
| 15:00-16:00 | 204 | 195 | 194 | 183 | 776 |
| 16:00-17:00 | 210 | 170 | 157 | 148 | 685 |
| 17:00-18:00 | 187 | 196 | 194 | 223 | 800 |
| 18:00-19:00 | 188 | 178 | 214 | 214 | 794 |
| 19:00-20:00 | 174 | 160 | 181 | 160 | 675 |
| 20:00-21:00 | 109 | 143 | 114 | 160 | 526 |
| 21:00-22:00 | 111 | 133 | 174 | 167 | 585 |
| 22:00-23:00 | 151 | 136 | 72 | 70 | 429 |
| 23:00-24:00 ( | 62 | 71 | 71 | 73 | 277 |
| Total |  |  |  |  | 10,867 |
| AADT |  |  |  |  | 9,489 |
| AM Peak | $\begin{array}{r} 11: 15-12: 15 \\ 633 \\ \hline \end{array}$ |  |  |  |  |
| PM Peak | $\begin{array}{r} \hline 17: 45-18: 45 \\ 803 \\ \hline \end{array}$ |  |  |  |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | R22551 |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | 24 |
|  | Exit 20B Route 139 West Stoughton |
| Direction | RAMP |
| Community | - |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000000429 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Axle/Tube |


| Time | 15-min Interval |  |  |  | Hourly Count |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1st | 2nd | 3rd | 4th |  |
| (3) 0:00-1:00 | 18 | 11 | 21 | 18 | 68 |
| 1:00-2:00 | 14 | 9 | 8 | 6 | 37 |
| 2:00-3:00 | 12 | 11 | 11 | 8 | 42 |
| 3:00-4:00 | 6 | 11 | 10 | 5 | 32 |
| 4:00-5:00 | 4 | 4 | 16 | 24 | 48 |
| 5:00-6:00 | 26 | 45 | 78 | 73 | 222 |
| 6:00-7:00 | 71 | 73 | 98 | 106 | 348 |
| 7:00-8:00 | 91 | 97 | 107 | 86 | 381 |
| 8:00-9:00 | 110 | 105 | 78 | 98 | 391 |
| 9:00-10:00 | 94 | 85 | 101 | 99 | 379 |
| 10:00-11:00 | 111 | 118 | 115 | 119 | 463 |
| 11:00-12:00 | 90 | 125 | 118 | 114 | 447 |
| 12:00-13:00 | 112 | 109 | 104 | 96 | 421 |
| 13:00-14:00 | 109 | 98 | 85 | 114 | 406 |
| 14:00-15:00 | 112 | 137 | 124 | 169 | 542 |
| 15:00-16:00 | 133 | 144 | 139 | 100 | 516 |
| 16:00-17:00 | 123 | 131 | 131 | 89 | 474 |
| 17:00-18:00 | 145 | 114 | 129 | 104 | 492 |
| 18:00-19:00 | 145 | 132 | 125 | 103 | 505 |
| 19:00-20:00 | 90 | 101 | 77 | 75 | 343 |
| 20:00-21:00 | 99 | 74 | 76 | 74 | 323 |
| 21:00-22:00 | 52 | 54 | 54 | 59 | 219 |
| 22:00-23:00 | 47 | 40 | 46 | 35 | 168 |
| 23:00-24:00 (i) | 42 | 42 | 33 | 23 | 140 |
| Total |  |  |  |  | 7,407 |
| AADT |  |  |  |  | 6,752 |
| AM Peak | $11: 15-12: 15$ |  |  |  |  |
| PM Peak | $14: 45-15: 45$ |  |  |  |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | H8462_SB |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | SR-24 |
| Loc On Alias | SR-24, 1.0 mile N. of Lindelof Ave <br> (Rt. 139) |
| Direction | SB |
| Community |  |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |

## INTERVAL: 15-MIN

| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Wed 3/29/2017 |
| End Date | Thu 3/30/2017 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | H8462 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type |  |


| Time | 15-min Interval |  |  | Hourly |  |
| :---: | ---: | ---: | ---: | ---: | ---: |
|  | Count |  |  |  |  |
| $\mathbf{1 s t}$ | 2nd | 3rd | 4th |  |  |
| $\mathbf{0 : 0 0 - 1 : 0 0}$ | 309 | 278 | 242 | 227 | 1,056 |
| $\mathbf{1 : 0 0 - 2 : 0 0}$ | 186 | 157 | 136 | 120 | 599 |
| $\mathbf{2 : 0 0 - 3 : 0 0}$ | 118 | 100 | 98 | 64 | 380 |
| $\mathbf{3 : 0 0 - 4 : 0 0}$ | 79 | 87 | 83 | 81 | 330 |
| $\mathbf{4 : 0 0 - 5 : 0 0}$ | 91 | 123 | 137 | 173 | 524 |
| $\mathbf{5 : 0 0 - 6 : 0 0}$ | 237 | 315 | 367 | 481 | 1,400 |
| $\mathbf{6 : 0 0 - 7 : 0 0}$ | 454 | 499 | 629 | 791 | 2,373 |
| $\mathbf{7 : 0 0 - 8 : 0 0}$ | 725 | 864 | 904 | 977 | 3,470 |
| $\mathbf{8 : 0 0 - 9 : 0 0}$ | 884 | 885 | 915 | 809 | 3,493 |
| $\mathbf{9 : 0 0 - 1 0 : 0 0}$ | 759 | 746 | 774 | 845 | 3,124 |
| $\mathbf{1 0 : 0 0 - 1 1 : 0 0}$ | 798 | 808 | 863 | 878 | 3,347 |
| $\mathbf{1 1 : 0 0 - 1 2 : 0 0}$ | 866 | 875 | 939 | 874 | 3,554 |
| $\mathbf{1 2 : 0 0 - 1 3 : 0 0}$ | 991 | 991 | 955 | 965 | 3,902 |
| $\mathbf{1 3 : 0 0 - 1 4 : 0 0}$ | 1,022 | 1,056 | 1,149 | 1,239 | 4,466 |
| $\mathbf{1 4 : 0 0 - 1 5 : 0 0}$ | 1,230 | 1,288 | 1,440 | 1,411 | 5,369 |
| $\mathbf{1 5 : 0 0 - 1 6 : 0 0}$ | 1,472 | 1,482 | 1,319 | 1,094 | 5,367 |
| $\mathbf{1 6 : 0 0 - 1 7 : 0 0}$ | 1,333 | 1,485 | 1,403 | 1,453 | 5,674 |
| $\mathbf{1 7 : 0 0 - 1 8 : 0 0}$ | 1,355 | 1,378 | 1,409 | 1,455 | 5,597 |
| $\mathbf{1 8 : 0 0 - 1 9 : 0 0}$ | 1,322 | 1,224 | 1,244 | 1,259 | 5,049 |
| $\mathbf{1 9 : 0 0 - 2 0 : 0 0}$ | 958 | 1,058 | 878 | 851 | 3,745 |
| $\mathbf{2 0 : 0 0 - 2 1 : 0 0}$ | 883 | 766 | 778 | 744 | 3,171 |
| $\mathbf{2 1 : 0 0 - 2 2 : 0 0}$ | 720 | 665 | 634 | 564 | 2,583 |
| $\mathbf{2 2 : 0 0 - 2 3 : 0 0}$ | 461 | 538 | 513 | 519 | 2,031 |
| $\mathbf{2 3 : 0 0 - 2 4 : 0 0}$ | 458 | 455 | 352 | 302 | 1,567 |
| PM Peak |  |  |  | $14: 30-15: 30$ |  |
| Total |  |  |  |  | 72,171 |
| AM Peak |  |  |  | $11: 45-12: 45$ |  |
|  |  |  |  |  | 5,805 |
|  |  |  |  |  |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | $614 \_$SB |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | AMVETS MEMORIAL HIGHWAY |
|  | ON SO. \& NO. RAMPS OF <br> RTE.I-93 |
| Direction | SB |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Wed 2/15/2017 |
| End Date | Thu 2/16/2017 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000061402 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type |  |


| INTERVAL:60-MIN |  |
| :---: | :---: |
| Time | Hourly Count |
| (1) 0:00-1:00 | 1,014 |
| 1:00-2:00 | 530 |
| 2:00-3:00 | 319 |
| 3:00-4:00 | 276 |
| 4:00-5:00 | 459 |
| 5:00-6:00 | 1,175 |
| 6:00-7:00 | 2,262 |
| 7:00-8:00 | 3,117 |
| 8:00-9:00 | 3,453 |
| 9:00-10:00 | 3,009 |
| 10:00-11:00 | 2,912 |
| 11:00-12:00 | 3,354 |
| 12:00-13:00 | 3,618 |
| 13:00-14:00 | 3,954 |
| 14:00-15:00 | 5,009 |
| 15:00-16:00 | 5,138 |
| 16:00-17:00 | 4,559 |
| 17:00-18:00 | 4,363 |
| 18:00-19:00 | 4,524 |
| 19:00-20:00 | 4,306 |
| 20:00-21:00 | 3,051 |
| 21:00-22:00 | 2,470 |
| 22:00-23:00 | 1,882 |
| 23:00-24:00 (i) | 1,441 |
| Total | 66,195 |
| AM Peak | $\begin{array}{r} 08: 00-09: 00 \\ 3,453 \\ \hline \end{array}$ |
| PM Peak | $\begin{array}{r} 15: 00-16: 00 \\ 5,138 \end{array}$ |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 614 _SB |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | AMVETS MEMORIAL HIGHWAY |
|  | ON SO. \& NO. RAMPS OF <br> RTE.I-93 |
| Direction | SB |
| Community | RANDOLPH |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | $12: 00: 00 \mathrm{AM}$ |
| End Time | $12: 00: 00 \mathrm{AM}$ |
| Direction |  |
| Notes |  |
| Count Source | 000000061402 |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type |  |


| TNTERVAL:60-MIN |  |
| :---: | ---: |
| Time | Hourly <br> Count |
| $\mathbf{0 : 0 0 - 1 : 0 0}$ | 810 |
| $\mathbf{1 : 0 0 - 2 : 0 0}$ | 430 |
| $\mathbf{2 : 0 0 - 3 : 0 0}$ | 276 |
| $\mathbf{3 : 0 0 - 4 : 0 0}$ | 257 |
| $\mathbf{4 : 0 0 - 5 : 0 0}$ | 429 |
| $\mathbf{5 : 0 0 - 6 : 0 0}$ | 1,115 |
| $\mathbf{6 : 0 0 - 7 : 0 0}$ | 2,364 |
| $\mathbf{7 : 0 0 - 8 : 0 0}$ | 3,275 |
| $\mathbf{8 : 0 0 - 9 : 0 0}$ | 3,134 |
| $\mathbf{9 : 0 0 - 1 0 : 0 0}$ | 2,760 |
| $\mathbf{1 0 : 0 0 - 1 1 : 0 0}$ | 3,009 |
| $\mathbf{1 1 : 0 0 - 1 2 : 0 0}$ | 3,216 |
| $\mathbf{1 2 : 0 0 - 1 3 : 0 0}$ | 3,409 |
| $\mathbf{1 3 : 0 0 - 1 4 : 0 0}$ | 3,632 |
| $\mathbf{1 4 : 0 0 - 1 5 : 0 0}$ | 5,127 |
| $\mathbf{1 5 : 0 0 - 1 6 : 0 0}$ | 5,737 |
| $\mathbf{1 6 : 0 0 - 1 7 : 0 0}$ | 5,639 |
| $\mathbf{1 7 : 0 0 - 1 8 : 0 0}$ | 5,595 |
| $\mathbf{1 8 : 0 0 - 1 9 : 0 0}$ | 5,217 |
| $\mathbf{1 9 : 0 0 - 2 0 : 0 0}$ | 3,915 |
| $\mathbf{2 0 : 0 0 - 2 1 : 0 0}$ | 3,050 |
| $\mathbf{2 1 : 0 0 - 2 2 : 0 0}$ | 2,513 |
| $\mathbf{2 2 : 0 0 - 2 3 : 0 0}$ | 2,087 |
| $\mathbf{2 3 : 0 0 - 2 4 : 0 0}$ | 1,525 |
| Total | 68,521 |
| AADT | 64,067 |
| AM Peak | $07: 00-08: 00$ |
| 3,275 |  |
| $15: 00-16: 00$ |  |
| 5,737 |  |

## Volume Count Report

| LOCATION INFO |  |
| ---: | :--- |
| Location ID | 6237 _SB |
| Type | SPOT |
| Fnct'I Class | 2 |
| Located On | AMVETS MEMORIAL HIGHWAY |
| SOUTH OF | RTE.139 |
| Direction | SB |
| Community | STOUGHTON |
| MPO ID |  |
| HPMS ID |  |
| Agency | MHD |


| COUNT DATA INFO |  |
| ---: | :--- |
| Count Status | Accepted |
| Start Date | Tue 5/5/2015 |
| End Date | Wed 5/6/2015 |
| Start Time | 12:00:00 AM |
| End Time | $12: 00: 00$ AM |
| Direction | SB |
| Notes |  |
| Count Source |  |
| Weather |  |
| Study |  |
| Speed Limit |  |
| Description |  |
| Sensor Type | Loop |


| INTERVAL:60-MIN |  |
| :---: | :---: |
| Time | Hourly Count |
| (1) 0:00-1:00 | 776 |
| 1:00-2:00 | 354 |
| 2:00-3:00 | 252 |
| 3:00-4:00 | 249 |
| 4:00-5:00 | 368 |
| 5:00-6:00 | 860 |
| 6:00-7:00 | 2,127 |
| 7:00-8:00 | 2,947 |
| 8:00-9:00 | 2,854 |
| 9:00-10:00 | 2,568 |
| 10:00-11:00 | 2,658 |
| 11:00-12:00 | 2,780 |
| 12:00-13:00 | 3,096 |
| 13:00-14:00 | 3,341 |
| 14:00-15:00 | 4,728 |
| 15:00-16:00 | 5,348 |
| 16:00-17:00 | 5,590 |
| 17:00-18:00 | 5,421 |
| 18:00-19:00 | 4,940 |
| 19:00-20:00 | 3,619 |
| 20:00-21:00 | 2,858 |
| 21:00-22:00 | 2,273 |
| 22:00-23:00 | 1,878 |
| 23:00-24:00 (i) | 1,418 |
| Total | 63,303 |
| AADT | 59,188 |
| AM Peak | $\begin{array}{r} \hline 07: 00-08: 00 \\ 2,947 \\ \hline \end{array}$ |
| PM Peak | $\begin{array}{r} 16: 00-17: 00 \\ 5,590 \\ \hline \end{array}$ |

## APPENDIX C

1. Crash Tables

| Study Location | Area of Crash | Count | Crash Number | Crash Year | Crash Time | Crash Date | Crash Severity | Number of Vehicles | Nonfatal Injuries | Fatal Injuries | Manner of Collision | Vehicle Travelled Direction | Road Surface Condition | Ambient Light Condition | Weather Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Exit 29 (from Route 2) | 1 | 2553682 | 2010 | 6:20 PM | 1/9/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Dark - roadway not lighted | Cloudy |
|  | Exit 29 (from Route 2) | 2 | 2657960 | 2010 | 7:56 AM | 11/5/2010 | Non-fatal injury | 4 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Daylight | Rain |
|  | Exit 29 (from Route 2) | 3 | 2701711 | 2011 | 12:27 PM | 2/24/2011 | Non-fatal injury | 2 | 3 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 29 (from Route 2) | 4 | 3175559 | 2012 | 6:10 PM | 2/22/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 29 (from Route 2) | 5 | 3246604 | 2012 | 3:18 PM | 8/15/2012 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
|  | Exit 29 (from Route 2) | 6 | 3257816 | 2012 | 10:54 PM | 8/31/2012 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Clear |
|  | Exit 29 (from Route 2) | 7 | 3655172 | 2013 | 6:56 PM | 10/25/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI D | Dry | Dark - roadway not lighted | Clear |
|  | Exit 29 (from Route 2) | 8 | 3655176 | 2013 | 12:00 AM | 11/1/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound / V3:Northbound | Wet | Dark - unknown roadway lig |  |
|  | Exit 29 (from Route 2) | 9 | 3752728 | 2014 | 11:20 AM | 2/27/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
|  | Exit 29 (from Route 2) | 10 | 3950070 | 2014 | 9:00 AM | 9/10/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 1 | 2566650 | 2010 | 4:10 PM | 2/11/2010 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 2 | 2575282 | 2010 | 6:35 AM | 3/1/2010 | Non-fatal injury | 3 | 1 | 0 | Sideswipe, same direction | V1:Northbound | Wet | Daylight | Rain |
|  | Exit 30 (Route 2A/Service Plaza) | 3 | 2576747 | 2010 | 12:50 PM | 3/12/2010 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | clear |
|  | Exit 30 (Route 2A/Service Plaza) | 4 | 2590398 | 2010 | 6:10 AM | 4/5/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound / V3:Northbound / V4:N |  | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 5 | 2590444 | 2010 | 3:50 PM | 4/14/2010 | Property damage only | 5 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 6 | 2592555 | 2010 | 3:44 PM | 4/21/2010 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route $2 \mathrm{~A} /$ Service Plaza) | 7 | 2600091 | 2010 | 4:11 AM | 5/3/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 8 | 2600978 | 2010 | 4:11 AM | 5/3/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 9 | 2608067 | 2010 | 8:55 PM | 6/3/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Dark - roadway not lighted | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 10 | 2622743 | 2010 | 9:05 AM | 7/7/2010 | Property damage only | 3 | 0 | 0 | Angle | V1:Northbound / V2:Northbound | Dry | Daylight | Not Reported |
|  | Exit 30 (Route 2A/Service Plaza) | 11 | 2645138 | 2010 | 3:53 PM | 9/22/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route $2 \mathrm{~A} /$ Service Plaza) | 12 | 2643855 | 2010 | 12:00 AM | 9/26/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Westbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 13 | 2652741 | 2010 | 1:35 PM | 10/6/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Wet | Daylight | Cloudy/Rain |
|  | Exit 30 (Route 2A/Service Plaza) | 14 | 2657956 | 2010 | 3:43 PM | 11/2/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 15 | 2659107 | 2010 | 6:40 PM | 11/4/2010 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:N |  | Dark - roadway not lighted | Cloudy |
|  | Exit 30 (Route $2 \mathrm{~A} /$ Service Plaza) | 16 | 2668189 | 2010 | 1:30 PM | 11/24/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 17 | 2667890 | 2010 | 5:55 PM | 11/30/2010 | Property damage only |  | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI D |  | Dark - lighted roadway | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 18 | 2667894 | 2010 | 6:30 PM | 12/1/2010 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Dark - lighted roadway | Rain |
|  | Exit 30 (Route $2 \mathrm{~A} /$ Service Plaza) | 19 | 2673802 | 2010 | 6:15 AM | 12/10/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 20 | 2671292 | 2010 | 10:07 AM | 12/13/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Wet | Daylight | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 21 | 2690290 | 2011 | 6:40 PM | 1/6/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 22 | 2682396 | 2011 | 11:18 AM | 1/10/2011 | Non-fatal injury | 2 | 1 | 0 | Angle | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) |  | 2689420 | 2011 | 5:02 PM | 1/11/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dusk | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 24 | 2690294 | 2011 | 8:00 AM | 1/12/2011 | Property damage only | 2 | 0 | 0 | Angle | V1:Northbound / V2:Northbound / V3:Northbound | Snow | Daylight | Not Reported |
|  | Exit 30 (Route 2A/Service Plaza) | 25 | 2689422 | 2011 | 3:10 PM | 1/14/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 26 | 2689426 | 2011 | 6:25 AM | 1/20/2011 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound / V3:Northbound | Wet | Dawn | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 27 | 2690308 | 2011 | 7:24 PM | 1/20/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound | Wet | Dark - lighted roadway | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 28 | 2701695 | 2011 | 2:36 AM | 1/27/2011 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Snow | Dark - roadway not lighted | Snow |
|  | Exit 30 (Route 2A/Service Plaza) | 29 | 2701701 | 2011 | 5:57 AM | 2/3/2011 | Property damage only |  | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Dawn | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 30 | 2703451 | 2011 | 4:35 PM | 3/4/2011 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 31 | 2702745 | 2011 | 3:54 PM | 3/8/2011 | Non-fatal injury | 2 | 2 | 0 | Angle | V1:Northbound / V2:Northbound / V3:Not reported | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 32 | 2703453 | 2011 | 5:50 PM | 3/10/2011 | Non-fatal injury | 3 | 1 | 0 | Rear-end | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 33 | 2703543 | 2011 | 9:05 PM | 3/11/2011 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Wet | Dark - lighted roadway | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 34 | 2727549 | 2011 | 4:30 PM | 4/15/2011 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 35 | 2727551 | 2011 | 3:20 PM | 4/28/2011 | Non-fatal injury | 2 | 1 | 0 | Angle | V1:Northbound / V2:Northbound | Dry | Daylight | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 36 | 2754001 | 2011 | 10:29 PM | 7/29/2011 | Non-fatal injury | 2 | 1 | 0 | Not reported | V1:Northbound / V2:Northbound | Wet | Dark - roadway not lighted | Cloudy/Rain |
|  | Exit 30 (Route 2A/Service Plaza) | 37 | 2754543 | 2011 | 5:08 PM | 8/12/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 38 | 2752978 | 2011 | 4:20 AM | 8/13/2011 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 39 | 2756716 | 2011 | 6:26 AM | 8/28/2011 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Wet | Daylight | Cloudy/Rain |
|  | Exit 30 (Route $2 \mathrm{~A} /$ Service Plaza) | 40 | 2841957 | 2011 | 8:17 AM | 9/4/2011 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 41 | 2782933 | 2011 | 4:50 PM | 9/23/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 42 | 3371935 | 2011 | 4:56 AM | 11/5/2011 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 43 | 2832813 | 2011 | 8:39 AM | 12/2/2011 | Property damage only |  | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 44 | 2891186 | 2012 | 4:55 PM | 1/6/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound | Dry | Dark - lighted roadway | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 45 | 2882437 | 2012 | 11:51 AM | 1/17/2012 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Not reported | Wet | Daylight | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 46 | 2932754 | 2012 | 4:13 PM | 2/8/2012 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 47 | 2949190 | 2012 | 9:07 AM | 2/13/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 48 | 2932756 | 2012 | 8:16 PM | 2/13/2012 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 49 | 2949192 | 2012 | 6:17 PM | 2/17/2012 | Property damage only |  | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Cloudy |
|  | Exit 30 (Route $2 \mathrm{~A} /$ Service Plaza) | 50 | 2966301 | 2012 | 6:55 PM | 3/16/2012 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Wet | Dusk | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) | 51 | 3079862 | 2012 | 8:13 PM | 4/15/2012 | Not Reported | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Not Reported |
|  | Exit 30 (Route 2A/Service Plaza) | 52 | 3097939 | 2012 | 4:40 PM | 5/3/2012 | Not Reported | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Cloudy |
|  | Exit 30 (Route 2A/Service Plaza) Exit 30 (Route $2 \mathrm{~A} /$ Service Plaza) | 53 54 | 3125766 | 2012 | 4:42 PM 5:10 PM | 6/8/2012 | Not Reported | 2 | 0 | 0 | Rear-end Rear-end | V1:Northbound / V2:Northbound V1:Northbound | Dry | Daylight | Clear Clear |


| Study <br> Location | Area of Crash | Count | Crash Number | $\begin{aligned} & \text { Crash } \\ & \text { Year } \end{aligned}$ | Crash Time | Crash Date | Crash Severity | Number of Vehicles | Nonfatal Injuries | Fatal Injuries | Manner of Collision | Vehicle Travelled Direction | Road Surface Condition | Ambient Light Condition | Weather Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Exit 30 (Route 2A/Service Plaza) | 55 | 3240531 | 2012 | 3:06 PM | 7/24/2012 | Property damage only | 1 | , | , | Single vehicle crash | V1:Northbound / V2:Northbound | Wet | Daylight | Rain |
|  | Exit 30 (Route 2A/Service Plaza) | 56 | 3288538 | 2012 | 10:23 AM | 10/30/2012 | Non-fatal injury | 2 | 1 | 0 | Angle | V1:Northbound / V2:Northbound / V3:Northbound / V4:Noi W |  | Daylight | Cloudy |
| 1 | Exit 30 (Route 2A/Service Plaza) | 57 | 3293150 | 2012 | 4:54 PM | 11/16/2012 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 58 | 3305576 | 2012 | 1:51 PM | 12/1/2012 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound / V3:Northbound / V4:Noi W | Wet | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 59 | 3364515 | 2013 | 9:06 AM | 2/6/2013 | Non-fatal injury | 4 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Daylight | Cloudy |
| 1 | Exit 30 (Route 2A/Service Plaza) | 60 | 3362354 | 2013 | 3:15 PM | 2/15/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 61 | 3364187 | 2013 | 4:11 PM | 2/26/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 62 | 3369059 | 2013 | 4:00 PM | 3/3/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Daylight | Cloudy |
| 1 | Exit 30 (Route 2A/Service Plaza) | 63 | 3391524 | 2013 | 4:55 PM | 4/1/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:Noi D |  | Daylight | Not Reported |
| 1 | Exit 30 (Route 2A/Service Plaza) | 64 | 3394432 | 2013 | 5:40 PM | 4/23/2013 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Daylight | Rain |
| 1 | Exit 30 (Route 2A/Service Plaza) | 65 | 3548335 | 2013 | 3:35 PM | 7/23/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:Noi W | Wet | Daylight | Rain |
| 1 | Exit 30 (Route 2A/Service Plaza) | 66 | 3561252 | 2013 | 12:50 PM | 8/10/2013 | Property damage only | 4 | 0 | 0 | Rear-to-rear | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 67 | 3598958 | 2013 | 3:55 PM | 9/10/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 68 | 3616729 | 2013 | 3:42 PM | 10/7/2013 | Property damage only | 2 | 0 | 0 | Rear-end | v1:Westbound/v2:Westbound | Dry | Daylight | Cloudy |
| 1 | Exit 30 (Route 2A/Service Plaza) | 69 | 3655174 | 2013 | 8:06 PM | 10/29/2013 | Property damage only | 5 | 0 | 0 | Rear-end | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 70 | 3664844 | 2013 | 3:24 PM | 11/19/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 71 | 3709210 | 2013 | 4:49 PM | 11/22/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:No1 D |  | Dusk | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 72 | 3674682 | 2013 | 4:45 PM | 12/3/2013 | Non-fatal injury | 5 | 1 | 0 | Rear-end | V1:Northbound | Dry | Dark - lighted roadway | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 73 | 3712094 | 2013 | 3:10 AM | 12/15/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Snow | Dark - roadway not lighted | Snow/Other |
| 1 | Exit 30 (Route 2A/Service Plaza) | 74 | 3724021 | 2014 | 10:13 PM | 1/21/2014 | Property damage only | 2 | 0 | 0 | Angle | V1:Northbound | Snow | Dark - roadway not lighted | Snow |
| 1 | Exit 30 (Route 2A/Service Plaza) | 75 | 3772221 | 2014 | 2:55 PM | 3/7/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 76 | 3789242 | 2014 | 3:20 PM | 4/2/2014 | Non-fatal injury | 3 | 1 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 77 | 3800820 | 2014 | 5:00 PM | 5/5/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 78 | 3850237 | 2014 | 12:00 AM | 6/17/2014 | Non-fatal injury | 3 | 2 | 0 | Not reported | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 79 | 3883585 | 2014 | 11:25 AM | 7/17/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 80 | 3887788 | 2014 | 1:05 PM | 7/18/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 81 | 3896025 | 2014 | 10:40 PM | 7/25/2014 | Property damage only | 1 |  | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Cloudy |
| 1 | Exit 30 (Route 2A/Service Plaza) | 82 | 3890233 | 2014 | 1:27 AM | 7/28/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 83 | 3950337 | 2014 | 3:25 PM | 9/15/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
|  | Exit 30 (Route 2A/Service Plaza) | 84 | 3950077 | 2014 | 8:31 AM | 9/17/2014 | Property damage only | 2 |  | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 85 | 3962187 | 2014 | 11:32 PM | 10/4/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound / V3:Northbound | Wet | Dark - lighted roadway | Not Reported |
| 1 | Exit 30 (Route 2A/Service Plaza) | 86 | 3970274 | 2014 | 4:36 PM | 10/7/2014 | Non-fatal injury | 3 | 1 | 0 | Angle | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 87 | 3970827 | 2014 | 2:45 PM | 10/10/2014 | Property damage only | 3 | 0 | 0 | Rear-to-rear | V1:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 88 | 3971201 | 2014 | 8:32 PM | 10/22/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Wet | Dark - roadway not lighted | Rain |
| 1 | Exit 30 (Route 2A/Service Plaza) | 89 | 3971219 | 2014 | 9:00 AM | 10/28/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 90 | 3975859 | 2014 | 4:50 PM | 10/31/2014 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 91 | 3975862 | 2014 | 3:11 PM | 11/5/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound | Dry | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 92 | 3984686 | 2014 | 7:36 AM | 11/24/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Wet | Daylight | Cloudy/Rain |
| 1 | Exit 30 (Route 2A/Service Plaza) | 93 | 3979910 | 2014 | 6:10 AM | 11/28/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound ${ }^{\text {S }}$ | Snow | Dawn | Snow |
| 1 | Exit 30 (Route 2A/Service Plaza) | 94 | 3979912 | 2014 | 1:55 AM | 12/1/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI D |  | Dark - lighted roadway | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 95 | 3980692 | 2014 | 9:40 PM | 12/2/2014 | Property damage only | 4 | 0 | 0 | Not reported | V1:Northbound / V2:Northbound | Wet | Dark- lighted roadway | Snow |
| 1 | Exit 30 (Route 2A/Service Plaza) | 96 | 3984744 | 2014 | 9:41 PM | 12/2/2014 | Property damage only | 2 | 0 | 0 | Angle | V1:Northbound / V2:Northbound | Snow | Dark - roadway not lighted | Snow |
| 1 | Exit 30 (Route 2A/Service Plaza) | 97 | 3987639 | 2014 | 1:10 PM | 12/4/2014 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound / V3:Northbound W | Wet | Daylight | Clear |
| 1 | Exit 30 (Route 2A/Service Plaza) | 98 | 3988003 | 2014 | 4:30 PM | 12/23/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Dusk | Rain |
| 2 | Exit 378 (tol-95) | 1 | 2602779 | 2010 | 4:05 PM | 5/20/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (tol -95) | 2 | 2628477 | 2010 | 1:29 PM | 8/12/2010 | Property damage only | 3 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (to 1-95) | 3 | 2639290 | 2010 | 8:00 AM | 8/30/2010 | Property damage only |  | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Not Reported |
| 2 | Exit 378 (to -95) | 4 | 2662859 | 2010 | 9:00 AM | 11/13/2010 | Non-fatal injury | 2 | 1 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (tol -95) | 5 | 2673680 | 2010 | 7:50 AM | 12/14/2010 | Property damage only | 3 | 0 | 0 | Rear-end | $\mathrm{V} 1:$ Northbound | Dry | Daylight | clear |
| 2 | Exit 378 (to -95) | 6 | 2782601 | 2011 | 1:47 PM | 10/13/2011 | Property damage only | 2 | 0 | 0 | Angle | V1:Southbound / V2:Northbound | Wet | Daylight | Rain |
| 2 | Exit 378 (tol -95) | 7 | 3376968 | 2012 | 8:20 AM | 1/11/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (tol-95) | 8 | 3168167 | 2012 | 9:00 AM | 2/25/2012 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Not Reported |
| 2 | Exit 378 (to -95) | 9 | 3027277 | 2012 | 7:51 PM | 4/10/2012 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound | Dry | Dark - roadway not lighted | Clear |
| 2 | Exit 378 (tol-95) | 10 | 3175587 | 2012 | 10:11 AM | 4/15/2012 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (tol-95) | 11 | 3229544 | 2012 | 11:50 AM | 6/2/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Not Reported |
| 2 | Exit 378 (to -99) | 12 | 3150248 | 2012 | 5:39 PM | 6/16/2012 | Not Reported | 1 | 0 | 0 | Single vehicle crash | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (tol $1-95$ ) | 13 | 3245391 | 2012 | 8:15 AM | 8/8/2012 | Property damage only | 2 | 0 |  | Rear-end | V1:Southbound / V2:Southbound / v3:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (to -95) | 14 | 3248536 | 2012 | 6:50 AM | 8/27/2012 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (to -95) | 15 | 3299081 | 2012 | 7:33 AM | 11/19/2012 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Southbound / V2:Southbound / / 3:Southbound / V4:Sol D | Dry | Daylight | Not Reported |
|  | Exit 378 (to -95) | 16 | 3301795 | 2012 | 6:13 PM | 12/6/2012 | Property damage only | 5 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Dark - lighted roadway | Clear |
|  | Exit 378 (to 1-95) | 17 | 3328535 | 2013 | 8:45 AM | 1/7/2013 | Property damage only | 3 | 0 | 0 | Angle | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 2 | Exit 378 (to -95) | 18 | 3347125 | 2013 | 5:53 PM | 1/25/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Dark -lighted roadway | Clear |
|  | Exit 378 (to -95) | 19 | 3351197 | 2013 | 6:17 PM | 1/30/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Dark - roadway not lighted | Cloudy |
|  | Exit 378 |  | 3384399 |  | 8:55 AM | 2/6/2 | Proper |  |  |  | Rear-end | V1:Southbound |  | Daylight |  |



| Study Location | Area of Crash | Count | Crash Number | Crash Year | Crash Time | Crash Date | Crash Severity | Number of Vehicles | Nonfatal Injuries | Fatal Injuries | Manner of Collision | Vehicle Travelled Direction | Road Surface Condition | Ambient Light Condition | Weather Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Rt. 24 NB Exit 21 (at Diverge) | 38 | 3560865 | 2,013 | 8:40 AM | 7/31/2013 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 39 | 3561457 | 2,013 | 12:00 AM | 8/10/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - lighted roadway | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 40 | 3594178 | 2,013 | 8:35 AM | 9/17/2013 | Non-fatal injury | 3 | 2 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 41 | 3599018 | 2,013 | 8:50 AM | 9/23/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 42 | 3604044 | 2,013 | 5:59 AM | 9/27/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Cloudy |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 43 | 3604258 | 2,013 | 3:18 AM | 9/29/2013 | Property damage only | 2 | 0 | 0 | Single vehicle cr | V1:Northbound / V2:Not reported | Dry | Dark - roadway not lighted | Fog, smog, smok |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 44 | 3623333 | 2,013 | 1:32 PM | 10/19/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 45 | 3656640 | 2,013 | 6:45 PM | 11/7/2013 | Property damage only | 3 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound / V3:Northbound | Wet | Dark - roadway not lighted | Not Reported |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 46 | 3713444 | 2,013 | 5:30 AM | 12/19/2013 | Non-fatal injury | 2 | 1 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Wet | Dark - roadway not lighted | Cloudy |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 47 | 3715423 | 2,014 | 12:00 PM | 1/7/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 48 | 3782666 | 2,014 | 1:53 PM | 3/4/2014 | Non-fatal injury | 1 | 2 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 49 | 3804748 | 2,014 | 7:42 AM | 4/24/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 50 | 3826752 | 2,014 | 5:30 PM | 5/17/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 51 | 3899701 | 2,014 | 10:54 AM | 5/20/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 52 | 3896047 | 2,014 | 5:54 PM | 5/28/2014 | Fatal injury | 2 | 1 | 1 | Rear-end | V1:Northbound / V2:Northbound | Wet | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 53 | 3862692 | 2,014 | 12:00 AM | 6/8/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 54 | 3923779 | 2,014 | 4:55 PM | 8/23/2014 | Non-fatal injury | 3 | 3 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 55 | 393044 | 2,014 | 8:11 PM | 9/8/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 56 | 3963926 | 2,014 | 8:30 AM | 10/1/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Not reported | Wet | Daylight | Not Reported |
|  | Rt. 24 NB Exit 21 (at Diverge) | 57 | 3972157 | 2,014 | 5:35 AM | 10/10/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dawn | Cloudy |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 58 | 3972186 | 2,014 | 6:20 AM | 10/21/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Wet | Dawn | Cloudy |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 59 | 3973140 | 2,014 | 12:00 AM | 11/5/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - lighted roadway | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 60 | 3975942 | 2,014 | 6:55 AM | 11/18/2014 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 61 | 4028980 | 2,014 | 3:38 AM | 12/5/2014 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Cloudy |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 62 | 3987252 | 2,014 | 12:00 AM | 12/18/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
| 3 | Rt. 24 NB Exit 21 (at Diverge) | 63 | 3999146 | 2,014 | 5:25 AM | 12/21/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Snow | Dawn | Cloudy/Snow |
| 3 | Rt. 24 NB merge with 1-93 NB | 1 | 2563635 | 2,010 | 1:50 AM | 2/4/2010 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - lighted roadway | Clear |
| 3 | Rt. 24 NB merge with $1-93 \mathrm{NB}$ | 2 | 2734431 | 2,010 | 3:30 PM | 11/19/2010 | Non-fatal injury | 3 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ NB | 3 | 2736942 | 2,011 | 5:50 PM | 6/29/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with I-93 NB | 4 | 3013909 | 2,012 | 2:15 PM | 3/29/2012 | Non-fatal injury | 2 | 2 | 0 | Angle | V1:Not reported / V2:Not reported | Dry | Daylight | Not Reported |
| 3 | Rt. 24 NB merge with I-93 NB | 5 | 3291270 | 2,012 | 1:17 AM | 7/29/2012 | Property damage only | 7 |  | 0 | Single vehicle crash | V1:Not reported / V2:Northbound / V3:Northbound / V4:N |  | Dark - roadway not lighted | Rain |
| 3 | Rt. 24 NB merge with $1-93 \mathrm{NB}$ | 6 | 3249283 | 2,012 | 1:25 PM | 8/26/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Eastbound/ V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ NB | 7 | 3248919 | 2,012 | 5:33 AM | 9/4/2012 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Dawn | Rain |
| 3 | Rt. 24 NB merge with $1-93 \mathrm{NB}$ | 8 | 3349121 | 2,012 | 12:15 PM | 12/20/2012 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ NB | 9 | 3369758 | 2,013 | 2:13 PM | 2/10/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Wet | Daylight | Not Reported |
| 3 | Rt. 24 NB merge with $1-93$ NB | 10 | 3369915 | 2,013 | 1:59 PM | 2/12/2013 | Non-fatal injury | 2 | 2 | 0 | Angle | V1:Northbound / V2:Northbound | Wet | Daylight | Not Reported |
| 3 | Rt. 24 NB merge with $1-93$ NB | 11 | 3584155 | 2,013 | 6:00 PM | 3/12/2013 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Dusk | Rain |
| 3 | Rt. 24 NB merge with I-93 NB | 12 | 3578978 | 2,013 | 2:15 PM | 8/30/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ NB | 13 | 3708805 | 2,013 | 8:01 PM | 12/21/2013 | Not Reported | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
| 3 | Rt. 24 NB merge with $1-93 \mathrm{NB}$ | 14 | 3737864 | 2,014 | 6:01 PM | 2/14/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Clear |
| 3 | Rt. 24 NB merge with I-93 NB | 15 | 3743802 | 2,014 | 6:07 PM | 2/22/2014 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 3 | Rt. 24 NB merge with $1-93 \mathrm{NB}$ | 16 | 3791671 | 2,014 | 8:25 AM | 3/10/2014 | Property damage only | 2 | 0 | 0 | Angle | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ NB | 17 | 3923769 | 2,014 | 9:15 PM | 6/23/2014 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Not reported / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93 \mathrm{NB}$ | 18 | 3973499 | 2,014 | 7:40 AM | 9/18/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ SB | 1 | 2561294 | 2,010 | 5:13 PM | 1/30/2010 | Property damage only |  | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ SB | 2 | 2607085 | 2,010 | 12:30 PM | 5/20/2010 | Property damage only | 4 | 0 | 0 | Angle | V1:Southbound / V2:Southbound / V3:Southbound / V4:Sol Dr | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ SB | 3 | 2621262 | 2,010 | 11:50 AM | 6/26/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with I-93 SB | 4 | 2634871 | 2,010 | 7:56 AM | 7/29/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Daylight | Cloudy/Rain |
| 3 | Rt. 24 NB merge with $1-93$ SB | 5 | 264554 | 2,010 | 3:55 PM | 9/27/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Daylight | Cloudy |
| 3 | Rt. 24 NB merge with $1-93$ SB | 6 | 2653968 | 2,010 | 9:40 AM | 10/18/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ SB | 7 | 2718180 | 2,011 | 10:15 AM | 4/21/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ SB | \% | 3242552 | 2,012 | 5:11 PM | 8/1/2012 | Non-fatal injury | 1 | 3 | 0 | Single vehicle crash | V1:Southbound | Wet | Daylight | Cloudy |
| 3 | Rt. 24 NB merge with $1-93$ SB | 9 | 3369127 | 2,013 | 4:34 PM | 2/17/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Snow | Dusk | Snow |
| 3 | Rt. 24 NB merge with $1-93 \mathrm{SB}$ | 10 | 3560866 | 2,013 | 11:05 PM | 8/1/2013 | Property damage only | 1 | 0 |  | Single vehicle crash | V1:Southbound | Wet | Dark - lighted roadway | Not Reported |
| 3 | Rt. 24 NB merge with I-93 SB | 11 | 3718384 | 2,014 | 3:03 PM | 1/4/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Southbound | Dry | Daylight | Clear |
| 3 | Rt. 24 NB merge with $1-93$ SB | 12 | 3972165 | 2,014 | 9:48 AM | 10/13/2014 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Dry | Daylight | Not Reported |
| 3 | Rt. 24 NB merge with 1-93 SB | 13 | 3972185 | 2,014 | 1:40 AM | 10/21/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - roadway not lighted | Clear |
| 3 | Rt. 24 NB merge with $1-93$ SB | 14 | 3972191 | 2,014 | 2:30 PM | 10/23/2014 | Non-fatal injury | 2 | 2 |  | Head-on | V1:Southbound/ /2:Southbound | Wet | Daylight | Rain |
| 3 | Rt. 24 NB merge with $1-93$ SB | 15 | 3984907 | 2,014 | 1:11 PM | 11/25/2014 | Not Reported | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Not reported | Dry | Daylight | Cloudy |
| 4 | Rt. 24 SB at Merge | 1 | 2553183 | 2,010 | 5:45 AM | 1/5/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | Rt. 24 SB at Merge | 2 | 2560670 | 2,010 | 10:30 AM | 1/18/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Wet | Daylight | Cloudy/Sleet, hail ( |
|  | Rt. 24 SB at Merge | 3 | 2591138 | 2,010 | 11:24 PM | 3/25/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Dry | Dark - roadway not lighted | Clear |
|  | Rt. 24 SB at Merge <br> Rt. 24 SB at Merge | 4 | 2604889 | 2,010 2,010 | 4:20 PM 4:05 PM | 5/15/2010 5/24/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction Rear-end | V1:Not reported / V2:Not reported | Dry | Daylight Daylight | Clear Clear |



| Study Location | Area of Crash | Count | Crash Number | Crash Year | Crash Time | Crash Date | Crash Severity | Number of Vehicles | Nonfatal Injuries | Fatal Injuries | Manner of Collision | Vehicle Travelled Direction | Road Surface Condition | Ambient Light Condition | Weather Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 1 -93 NB Exit 4 to Rt. 24 | 12 | 2649795 | 2,010 | 3:28 PM | 9/22/2010 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Cloudy |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 13 | 2650231 | 2,010 | 11:13 PM | 9/25/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 14 | 2669023 | 2,010 | 5:31 PM | 11/15/2010 | Non-fatal injury | 4 | 2 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI Dr |  | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 15 | 2663264 | 2,010 | 5:15 PM | 11/18/2010 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 16 | 2664293 | 2,010 | 6:00 PM | 11/19/2010 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 17 | 2672098 | 2,010 | 5:10 PM | 12/16/2010 | Property damage only | 3 | 0 | 0 | Angle | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 18 | 2689763 | 2,011 | 8:00 AM | 1/10/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Cloudy |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 19 | 2689681 | 2,011 | 5:10 PM | 1/31/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 20 | 2713269 | 2,011 | 5:15 PM | 4/1/2011 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 21 | 2715350 | 2,011 | 3:05 PM | 4/14/2011 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 22 | 2715351 | 2,011 | 5:46 PM | 4/14/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 23 | 2727009 | 2,011 | 9:52 PM | 5/11/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Dark - roadway not lighted | Not Reported |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 24 | 2728166 | 2,011 | 5:12 PM | 5/12/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 25 | 2727013 | 2,011 | 11:38 PM | 5/14/2011 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 26 | 2757494 | 2,011 | 8:25 AM | 6/13/2011 | Non-fatal injury | 3 | 2 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 27 | 2733897 | 2,011 | 4:18 PM | 6/15/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 28 | 2751484 | 2,011 | 12:47 PM | 7/22/2011 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 29 | 2759779 | 2,011 | 4:50 PM | 8/29/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Not reported / V3:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 30 | 2782666 | 2,011 | 2:38 AM | 10/1/2011 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Wet | Dark - lighted roadway | Rain |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 31 | 2790953 | 2,011 | 5:05 PM | 10/24/2011 | Non-fatal injury | 4 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI Di |  | Daylight | Cloudy |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 32 | 2789046 | 2,011 | 6:22 PM | 10/25/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Dark - roadway not lighted | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 33 | 2788858 | 2,011 | 4:15 PM | 10/27/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Daylight | Rain |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 34 | 2834193 | 2,011 | 4:25 PM | 12/19/2011 | Non-fatal injury | 4 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI Did |  | Dark - lighted roadway | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 35 | 2861712 | 2,012 | 8:45 AM | 1/12/2012 | Property damage only | 2 | 0 | 0 | Angle | V1:Northbound / V2:Northbound | Wet | Daylight | Cloudy/Rain |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 36 | 2885389 | 2,012 | 11:27 PM | 1/19/2012 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Snow | Dark - lighted roadway | Snow |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 37 | 2891333 | 2,012 | 4:00 PM | 1/31/2012 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI D |  | Dusk | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 38 | 2903990 | 2,012 | 5:05 AM | 2/1/2012 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - lighted roadway | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 39 | 2942738 | 2,012 | 11:00 PM | 3/2/2012 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 40 | 2976126 | 2,012 | 3:40 PM | 3/6/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 41 | 2976231 | 2,012 | 3:47 PM | 3/19/2012 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 42 | 3013910 | 2,012 | 4:21 PM | 3/30/2012 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Cloudy |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 43 | 3027199 | 2,012 | 10:30 PM | 4/13/2012 | Property damage only | 2 | 0 | 0 | Single vehicle crash | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 44 | 3098027 | 2,012 | 3:35 AM | 5/13/2012 | Not Reported | 1 | 0 | 0 | Single vehicle crash | v1:Northbound | Dry | Dark- lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 45 | 3163132 | 2,012 | 3:56 PM | 6/14/2012 | Non-fatal injury | 4 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:N |  |  | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 46 | 3208045 | 2,012 | 4:20 PM | 6/18/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 47 | 3153181 | 2,012 | 5:46 PM | 6/21/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 48 | 3390290 | 2,012 | 1:00 PM | 7/17/2012 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry |  | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 49 | 3198592 | 2,012 | 7:55 AM | 7/18/2012 | Non-fatal injury | 3 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Eastbound | Dry | Daylight | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 50 | 3280766 | 2,012 | 4:46 PM | 10/4/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Daylight | Cloudy |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 51 | 3339369 | 2,012 | 5:55 AM | 11/4/2012 | Not Reported | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 52 | 3297460 | 2,012 | 5:26 PM | 11/5/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 53 | 3292062 | 2,012 | 10:21 PM | 11/9/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Not Reported |
| 4 | $1-93 \mathrm{NB}$ Exit 4 to Rt. 24 SB | 54 | 3321487 | 2,012 | 5:28 PM | 12/14/2012 | Property damage only | 2 | 0 | 0 | Angle | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 55 | 3337071 | 2,013 | 7:45 AM | 1/9/2013 | Property damage only | 1 | 0 | 0 | Head-on | V1:Northbound | Wet | Daylight | Clear/Cloudy |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 56 | 3340472 | 2,013 | 4:55 PM | 1/11/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Dark - roadway not lighted | Rain |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 57 | 3349170 | 2,013 | 6:06 PM | 2/1/2013 | Non-fatal injury | 2 | 2 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - roadway not lighted | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 58 | 3362677 | 2,013 | 8:38 PM | 2/23/2013 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Wet | Dark - lighted roadway | Cloudy/Rain |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 59 | 3369133 | 2,013 | 2:58 PM | 3/12/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet |  | Not Reported |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 60 | 3385798 | 2,013 | 3:25 PM | 4/4/2013 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 61 | 3393633 | 2,013 | 4:10 PM | 4/9/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 62 | 3414471 | 2,013 | 4:55 PM | 4/23/2013 | Property damage only |  | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 63 | 3430268 | 2,013 | 4:29 PM | 4/30/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 64 | 3430521 | 2,013 | 9:47 PM | 5/20/2013 | Non-fatal injury | 3 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Dark-lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 65 | 3453248 | 2,013 | 11:41 PM | 5/31/2013 | Property damage only | , | 0 | 0 | Rear-end | V1:Southbound/V2:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 66 | 3495738 | 2,013 | 5:05 PM | 6/19/2013 | Non-fatal injury | 4 | 2 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound / V4:NoI D | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 67 | 3548970 | 2,013 | 10:45 PM | 7/16/2013 | Property damage only | 3 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Southbound / V3:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 68 | 3548896 | 2,013 | 7:10 PM | 7/25/2013 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 69 | 3548975 | 2,013 | 5:33 PM | 8/2/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 70 | 3548899 | 2,013 | 9:40 PM | 8/3/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 71 | 3651275 | 2,013 | 2:18 PM | 8/30/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Not Reported |
| 4 | 1.93 NB Exit 4 to Rt. 24 SB | 72 | 3655449 | 2,013 | 2:20 PM | 10/26/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 73 | 3651464 | 2,013 | 4:08 PM | 11/1/2013 | Property damage only | 3 | 0 | 0 | Angle | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 74 | 3710734 | 2,013 | 10:17 AM | 11/18/2013 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound | Wet | Daylight | Clear |
|  | $1-93$ NB Exit 4 to R. 24 SB | 75 | 3665098 | 2,013 | 4:45 PM | 11/27/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Wet | Dark - roadway not lighted | Cloudy/Rain |


| Study Location | Area of Crash | Count | Crash Number | $\begin{array}{\|l\|} \hline \text { Crash } \\ \text { Year } \end{array}$ | Crash Time | Crash Date | Crash Severity | Number of Vehicles | Nonfatal Injuries | Fatal Injuries | Manner of Collision | Vehicle Travelled Direction | Road Surface Condition | Ambient Light Condition | Weather Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1-93$ NB Exit 4 to Rt. 24 SB | 76 | 3686343 | 2,013 | 5:20 PM | 12/12/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound | Dry | Daylight | Clear |
| 4 | $1-93 \mathrm{NB}$ Exit 4 to Rt. 24 SB | 77 | 3726716 | 2,014 | 5:20 PM | 1/24/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dark - lighted roadway | Clea |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 78 | 3785242 | 2,014 | 5:00 PM | 4/2/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound D | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 79 | 3785156 | 2,014 | 5:50 PM | 4/3/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 80 | 3823114 | 2,014 | 6:10 PM | 5/31/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 81 | 3896247 | 2,014 | 4:30 PM | 7/8/2014 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 82 | 3922725 | 2,014 | 9:00 PM | 8/22/2014 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Dark - lighted roadway | Clear |
| 4 | I-93 NB Exit 4 to Rt. 24 SB | 83 | 3972649 | 2,014 | 1:45 AM | 11/2/2014 | Non-fatal injury | 1 | 2 | 0 | Single vehicle crash | V1:Northbound | Wet | Dark - roadway not lighted | Rain |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 84 | 3972212 | 2,014 | 3:55 PM | 11/3/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Dusk | Clear |
| 4 | 1-93 NB Exit 4 to Rt. 24 SB | 85 | 3972213 | 2,014 | 6:14 PM | 11/4/2014 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound / V4:Sol D | Dry | Dark - roadway not lighted | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 86 | 3972218 | 2,014 | 5:25 PM | 11/12/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound D | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 87 | 3981774 | 2,014 | 6:43 PM | 12/2/2014 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Northbound / V2:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ NB Exit 4 to Rt. 24 SB | 88 | 3987249 | 2,014 | 4:50 PM | 12/16/2014 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound W | Wet | Dark - lighted roadway | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 1 | 2566582 | 2,010 | 8:25 AM | 2/7/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 2 | 257474 | 2,010 | 5:30 PM | 2/24/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound W | Wet | Dusk | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 3 | 2573848 | 2,010 | 5:15 PM | 3/5/2010 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Southbound | Dry | Dusk | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 4 | 2591271 | 2,010 | 7:20 AM | 4/15/2010 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Southbound D | Dry | Daylight | Clear |
| 4 | I-93 SB Exit 4 to Rt. 24 SB | 5 | 2608173 | 2,010 | 5:50 PM | 6/8/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound D | Dry | Daylight | Clear |
|  | $1-93$ SB Exit 4 to Rt. 24 SB |  | 2611367 | 2,010 | 7:00 PM | 6/9/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Daylight | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 7 | 2621055 | 2,010 | 8:30 AM | 6/30/2010 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound / V4:SoL D |  | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 8 | 2628437 | 2,010 | 1:00 PM | 7/29/2010 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Southbound ${ }^{\text {d }}$ | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to R. 24 SB |  | 2631011 | 2,010 | 8:20 AM | 8/3/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound D | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 10 | 2634383 | 2,010 | 11:00 AM | 8/12/2010 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 11 | 2638752 | 2,010 | 10:23 AM | 9/11/2010 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound D | Dry | Daylight | Cloudy |
|  | $1-93$ SB Exit 4 to Rt. 24 SB | 12 | 2649059 | 2,010 | 10:37 PM | 9/16/2010 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Southbound ${ }^{\text {a }}$ | Wet | Dark - lighted roadway | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 13 | 2647652 | 2,010 | 11:18 PM | 9/29/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Dry | Dark - lighted roadway | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 14 | 2648305 | 2,010 | 11:19 AM | 10/6/2010 | Property damage only | 1 | 0 |  | Single vehicle crash | V1:Southbound W | Wet | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 15 | 2660477 | 2,010 | 2:35 AM | 10/15/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Wet | Dark - roadway not lighted | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to R. 24 SB | 16 | 2657371 | 2,010 | 3:29 PM | 10/23/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 17 | 2657374 | 2,010 | 8:45 PM | 10/27/2010 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Dark - lighted roadway | Cloudy |
| 4 | 1 -93 SB Exit 4 to Rt. 24 SB | 18 | 2668836 | 2,010 | 11:30 PM | 11/2/2010 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound D | Dry | Dark - roadway not lighted | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 19 | 2664301 | 2,010 | 5:36 PM | 11/11/2010 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound / V4:Sol D |  | Dark - lighted roadway | Not Reported |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 20 | 2668804 | 2,010 | 1:24 AM | 11/19/2010 | Property damage only |  | 0 | 0 | Not reported | V1:Southbound / V2:Southbound | Not reported | Not reported | Not Reported |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 21 | 2664066 | 2,010 | 1:25 PM | 11/20/2010 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Southbound D | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 22 | 2665500 | 2,010 | 12:00 AM | 11/22/2010 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound D | Dry | Dark - roadway not lighted | Clear |
| 4 | $1-93$ SB Exit 4 to R. 24 SB | 23 | 2664403 | 2,010 | 1:10 AM | 11/22/2010 | Property damage only | 3 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound / V3:Southbound D | Dry | Dark - roadway not lighted | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 24 | 2670348 | 2,010 | 1:33 AM | 11/26/2010 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 25 | 2668689 | 2,010 | 7:10 PM | 12/1/2010 | Non-fatal injury | 1 | 1 |  | Single vehicle crash | V1:Southbound W | Wet | Dark - lighted roadway | Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 26 | 2673852 | 2,010 | 5:35 PM | 12/21/2010 | Property damage only | 4 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound / V4:Sol W |  | Dark - lighted roadway | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 27 | 2677332 | 2,010 | 7:25 AM | 12/29/2010 | Property damage only | 3 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound / V3:Southbound W | Wet | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 28 | 2678865 | 2,011 | 6:35 PM | 1/2/2011 | Non-fatal injury | 2 | 3 | 0 | Head-on | V1:Southbound / V2:Southbound | Wet | Dark - lighted roadway | Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 29 | 2701462 | 2,011 | 2:14 AM | 1/31/2011 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Dry | Dark-lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 30 | 2727758 | 2,011 | 1:49 AM | 4/17/2011 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound ${ }^{\text {W }}$ | Wet | Dark - lighted roadway | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 31 | 2728892 | 2,011 | 8:00 AM | 5/25/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Northbound / V3:Southbound D | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 32 | 2727016 | 2,011 | 7:50 AM | 5/26/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 33 | 2738115 | 2,011 | 9:16 PM | 6/30/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound D | Dry | Dark - roadway not lighted | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 34 | 3377504 | 2,011 | 10:30 AM | 8/7/2011 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound ${ }^{\text {d }}$ | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 35 | 2751501 | 2,011 | 3:23 PM | 8/7/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound We | Wet | Daylight | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 36 | 2756840 | 2,011 | 9:56 PM | 8/20/2011 | Non-fatal injury | 2 | 1 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound D | Dry | Dark-lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 37 | 2759862 | 2,011 | 9:34 PM | 9/4/2011 | Property damage only | 1 | 0 | 0 | Sideswipe, same direction | V1:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 38 | 3375409 | 2,011 | 6:56 AM | 9/8/2011 | Non-fatal injury | 1 | 1 | O | Single vehicle crash | V1:Southbound W | Wet | Daylight | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 39 | 2763615 | 2,011 | 5:00 PM | 9/18/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound D | Dry | Daylight | Not Reported |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 40 | 2767502 | 2,011 | 2:25 PM | 9/24/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound W | Wet | Daylight | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 41 | 2778897 | 2,011 | 3:55 PM | 10/7/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 42 | 2790275 | 2,011 | 4:35 PM | 10/22/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound D | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 43 | 2788859 | 2,011 | 3:10 PM | 10/29/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Daylight | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to R. 24 SB | 44 | 2817088 | 2,011 | 7:33 AM | 11/23/2011 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Daylight | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 45 | 2827626 | 2,011 | 6:25 PM | 12/7/2011 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Wet | Dark -lighted roadway | Rain |
|  | $1-93$ SB Exit 4 to Rt. 24 SB | 46 | 2839036 | 2,011 | 5:35 PM | 12/27/2011 | Non-fatal injury | 2 | 3 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to R. 24 SB | 47 | 2861709 | 2,012 | 3:28 PM | 1/12/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound W | Wet | Daylight | Not Reported |
|  | $1-93$ SB Exit 4 to Rt. 24 SB | 48 | 2926398 | 2,012 | 7:55 AM | 2/21/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
|  | $1-93$ SB Exit 4 to R. 24 SB | 49 | 2972766 | 2,012 | 4:10 PM | 3/15/2012 | Non-fatal injury | 2 | 2 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
|  | $1-93$ SB Exit 4 to Rt. 24 SB | 50 | 2995144 | 2,012 | 4:13 PM | 3/26/2012 | Non-fatal injury | 3 | 1 | 0 | Rear-end | V1:Northbound / V2:Northbound / V3:Northbound D | Dry | Daylight | Clear |
|  | $1-93$ SB Exit 4 to Rt. 24 SB | 51 | 3038691 | 2,012 | 12:00 AM | 4/6/2012 | Non-fatal injury |  | 1 | 0 | Sid | V1:Southbound / V2:Southbound | Dry | Dark - roa |  |


| Study Location | Area of Crash | Count | Crash Number | Crash Year | Crash Time | Crash Date | Crash Severity | Number of Vehicles | Nonfatal Injuries | Fatal Injuries | Manner of Collision | Vehicle Travelled Direction | Road Surface Condition | Ambient Light Condition | Weather Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | $1-93$ SB Exit 4 to R.t 24 SB | 52 | 3107264 | 2,012 | 2:15 AM | 4/23/2012 | Not Reported | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Wet | Dark - lighted roadway | Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 53 | 3121135 | 2,012 | 2:55 PM | 6/1/2012 | Not Reported | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southboun | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 54 | 3384369 | 2,012 | 2:31 AM | 7/15/2012 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 55 | 3219191 | 2,012 | 8:15 AM | 7/19/2012 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 56 | 3384442 | 2,012 | 8:21AM | 7/26/2012 | Property damage only | 3 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 57 | 3242555 | 2,012 | 5:49 PM | 8/9/2012 | Non-fatal injury | 3 | 2 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 58 | 3244510 | 2,012 | 1:00 PM | 8/18/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Daylight | Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 59 | 3248555 | 2,012 | 2:55 PM | 8/30/2012 | Property damage only | 2 | 0 | 0 | Angle | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 60 | 3299709 | 2,012 | 4:40 PM | 11/14/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 61 | 3341779 | 2,012 | 7:18 AM | 11/28/2012 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 62 | 3304280 | 2,012 | 7:46 AM | 12/2/2012 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Daylight | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 63 | 3298910 | 2,012 | 6:25 PM | 12/4/2012 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Dark - lighted roadway | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 64 | 3321625 | 2,012 | 3:05 PM | 12/9/2012 | Non-fatal injury | 2 | 1 | 0 | Angle | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 65 | 3312164 | 2,012 | 6:50 AM | 12/10/2012 | Property damage only | 3 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound / V3:Southbound | Wet | Dawn | Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 66 | 3359762 | 2,013 | 8:13 AM | 1/31/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Wet | Daylight | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 67 | 3384759 | 2,013 | 5:02 AM | 2/24/2013 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound | Wet | Dark - roadway not lighted | Rain/Fog, smog, s |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 68 | 3391683 | 2,013 | 9:05 AM | 4/8/2013 | Non-fatal injury | 2 | 1 | 0 | Sideswipe, same direction | V1:Southbound / V2:Not reported | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 69 | 3430383 | 2,013 | 10:20 AM | 5/27/2013 | Non-fatal injury | 3 | 1 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 70 | 3453208 | 2,013 | 5:13 AM | 6/4/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Dry | Dawn | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 71 | 3471478 | 2,013 | 7:10 PM | 6/8/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 72 | 3479533 | 2,013 | 7:40 AM | 6/19/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 73 | 3534501 | 2,013 | 7:30 AM | 7/15/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 74 | 3548897 | 2,013 | 4:35 PM | 7/31/2013 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 75 | 3560990 | 2,013 | 6:45 AM | 8/1/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 76 | 3560868 | 2,013 | 3:45 PM | 8/14/2013 | Non-fatal injury | 2 | 1 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 77 | 3584731 | 2,013 | 9:46 PM | 9/5/2013 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 78 | 3651613 | 2,013 | 9:00 AM | 9/16/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 79 | 3603414 | 2,013 | 3:10 PM | 9/20/2013 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 80 | 3594182 | 2,013 | 12:15 PM | 9/22/2013 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound/ /2:Southbound | Dry | Daylight | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 81 | 3599019 | 2,013 | 10:00 AM | 9/23/2013 | Non-fatal injury | 1 | 1 | 0 | Single vehicle crash | V1:Northbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 82 | 3607529 | 2,013 | 6:50 AM | 10/10/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Dawn | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 83 | 3626672 | 2,013 | 11:15 PM | 10/10/2013 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Dark - lighted roadway | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 84 | 3611128 | 2,013 | 5:30 PM | 10/12/2013 | Property damage only | 1 | 0 | 0 | Single vehicle crash | V1:Southbound | Wet | Daylight | Cloudy/Rain |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 85 | 3651465 | 2,013 | 12:00 PM | 11/2/2013 | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Northbound | Dry | Daylight | Not Reported |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 86 | 3655820 | 2,013 | 7:35 PM | 11/6/2013 | Property damage only | 2 | 0 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Dry | Dark - roadway not lighted | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 87 | 3667326 | 2,013 | 9:35 AM | 11/26/2013 | Property damage only | 2 | 0 |  | Angle | V1:Southbound / V2:Southbound | Dry | Daylight | Cloudy |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 88 | 3728536 | 2,014 | 10:20 AM | 1/23/2014 | Non-fatal injury | 2 | 1 | 0 | Sideswipe, same direction | V1:Southbound / V2:Southbound | Other | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 89 | 3862599 | 2,014 | 5:15 PM | 6/12/2014 | Property damage only | 3 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
| 4 | $1-93$ SB Exit 4 to Rt. 24 SB | 90 | 3880598 | 2,014 | 11:00 AM | 7/12/2014 | Property damage only | 3 | 0 | 0 | Angle | V1:Southbound / V2:Southbound / V3:Southbound | Dry | Daylight | Clear |
|  |  | 91 | 3922711 | 2,014 | 7.50 AM 8.50 PM | $7 / 22 / 2014$ $12 / 17 / 2014$ | Property damage only | 2 | 0 | 0 | Rear-end | V1:Southbound / V2:Southbound | Dry | Daylight |  |

## APPENDIX D

1. HCS Printouts

## Index

\left.| Page | Location | Roadway | Scenario | Analysis Type |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | I-95 NB | 2030 No-Build | Basic Freeway Segment |$\right]$ Peak

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - 2030 No-Build - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.2 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 7980 | Heavy Vehicle Adjustment Factor (fнv) | 0.976 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 2044 |
| Total Trucks, \% | 2.50 | Capacity (c), pc/h/ln | 2322 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2322 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.88 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 57.6 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 35.5 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | E |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.2 |  |  |

[^24]
## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - 2030 No-Build - Basic Freeway Segment - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.2 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 8800 | Heavy Vehicle Adjustment Factor (fuv) | 0.983 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 2238 |
| Total Trucks, \% | 1.70 | Capacity (c), pc/h/ln | 2322 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (cadj), pc/h/ln | 2322 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.96 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 53.7 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 41.7 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | E |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.2 |  |  |

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## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - 2030 No-Build - Diverge Analysis - AM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 65.0 | 1 |  |
| Free-Flow Speed (FFS), mi/h | 860 | 30.0 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | 600 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Right |  |
| Adjustment Factors |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7980 | 1155 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 2.50 | 1.70 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.976 | 0.983 |  |
| Flow Rate (vi), pc/h |  | 8176 | 1175 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.62 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R})}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 35.2 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ds) |  | 0.599 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1975 |
| Distance to Downstream Ramp (Loown), ft | - | Off-Ramp Influence Area Speed ( $\mathrm{S}_{\text {}}$, , mi/h |  | 51.2 |
| Prop. Freeway Vehicles in Lane 1 and 2 (PfD) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 67.5 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4227 | Ramp Junction Speed (S), mi/h |  | 58.0 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | - | Average Density (D), pc/mi/ln |  | 35.2 |
| Level of Service (LOS) | E |  |  |  |
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## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - 2030 No-Build - Diverge Analysis - PM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 65.0 | 1 |  |
| Free-Flow Speed (FFS), mi/h | 860 | 30.0 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | 600 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Right |  |
| Adjustmer\| |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 8800 | 1260 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.70 | 1.70 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.983 | 0.983 |  |
| Flow Rate (vi), pc/h |  | 8952 | 1282 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.95 | 0.67 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 38.6 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ds) |  | 0.608 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2163 |
| Distance to Downstream Ramp (Loww), ft | - | Off-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R})}$, mi/h |  | 51.0 |
| Prop. Freeway Vehicles in Lane 1 and 2 (PfD) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 66.8 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4626 | Ramp Junction Speed (S), mi/h |  | 57.6 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | - | Average Density (D), pc/mi/ln |  | 38.9 |
| Level of Service (LOS) | E |  |  |  |
| Location 1 - I-95 NB - 2030 No-Build - Diverge Analysis - PM.xuf Appendix D |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - 2030 No-Build - Merge Analysis - AM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 65.0 | 1 |  |
| Free-Flow Speed (FFS), mi/h | 860 | 25.0 |  |
| Segment Length (L) / Acceleration Length (LA), ft | Level | 620 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Right |  |
| Adjustment Factors |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 6405 | 1575 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 2.50 | 1.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.976 | 0.985 |  |
| Flow Rate (vi), pc/h |  | 6562 | 1599 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.84 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 33.9 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | 0.556 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1969 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\text {}}$, , mi/h |  | 52.2 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.018 | Outer Lanes Freeway Speed (So), mi/h |  | 59.7 |
| Flow in Lanes 1 and 2 (v12), pc/h | 2625 | Ramp Junction Speed (S), mi/h |  | 55.6 |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | 4224 | Average Density (D), pc/mi/ln |  | 36.7 |
| Level of Service (LOS) | D |  |  |  |
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## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1 - I-95 NB - 2030 No-Build - Merge Analysis - PM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 65.0 | 1 |  |
| Free-Flow Speed (FFS), mi/h | 860 | 25.0 |  |
| Segment Length (L) / Acceleration Length (LA), ft | Level | 620 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Right |  |
| Adjustmer\| |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 8800 | 945 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.70 | 2.00 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.983 | 0.980 |  |
| Flow Rate (vi), pc/h |  | 8952 | 964 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 1.05 | 0.51 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | - |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2686 |
| Distance to Downstream Ramp (Loown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{SR}_{\mathrm{R}}$, mi/h |  | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (PFM) | 0.097 | Outer Lanes Freeway Speed (So), mi/h |  | 56.2 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3581 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 4545 | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |
| Copyright © 2017 University of Florida. All Rights Reserved. <br> HCS7 ${ }^{\text {TM }}$ Freeways Version 7.3 <br> Generated: 10/2/20 <br> Location 1-I-95 NB - 2030 No-Build - Merge Analysis - PM.xuf |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - 2030 No-Build - Weaving Analysis - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1720 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), IC | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCRR), IC | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 0.83 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$, veh/h | 5250 | 1575 | 0 | 1155 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 2.50 | 1.50 | 0.00 | 1.70 |
| Heavy Vehicle Adjustment Factor (f fv ) | 0.976 | 0.985 | 1.000 | 0.983 |
| Flow Rate (vi), pc/h | 5379 | 1599 | 0 | 1175 |
| Weaving Flow Rate ( vw ), pc/h | 2774 | Freeway Max Capacity (CIFL), pc/h/ln |  | 2350 |
| Non-Weaving Flow Rate (vnw), pc/h | 5379 | Density-Based Capacity (ciwl), pc/h/ln |  | 2021 |
| Total Flow Rate (v), pc/h | 8153 | Demand Flow-Based Capacity (ciw), pc/h |  | 7059 |
| Volume Ratio (VR) | 0.340 | Weaving Segment Capacity (cw), veh/h |  | 6889 |
| Minimum Lane Change Rate (LCmin), Ic/h | 0 | Adjusted Weaving Area Capacity ( $\mathrm{Cwa}^{\text {a }}$, veh/h |  | 6889 |
| Maximum Weaving Length (Lmax), ft | 6017 | Volume-to-Capacity Ratio (v/c) |  | 1.16 |

## Speed and Density

| Non-Weaving Vehicle Index (Inw) | - | Average Weaving Speed (Sw), mi/h | - |
| :---: | :---: | :---: | :---: |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | - | Average Non-Weaving Speed (Snw), mi/h | - |
| Weaving Lane Change Rate (LCw), Ic/h | - | Average Speed (S), mi/h | - |
| Total Lane Change Rate (LCall), Ic/h | - | Density (D), pc/mi/ln | - |
| Weaving Intensity Factor (W) | - | Level of Service (LOS) | F |
| HCS7 ${ }^{\text {TM }}$ Freeways Version 7.3 Generated: 10/2/2017 9:12:26 PM <br> NB - 2030 No-Build - Weaving Analysis - AM.xuf  |  |  |  |

Appendix D

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - 2030 No-Build - Weaving Analysis - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1720 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), Ic | 0 |
| Interchange Density (ID), int/mi | 0.83 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume (Vi), veh/h | 6595 | 945 | 0 | 1260 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 1.70 | 2.00 | 0.00 | 1.70 |
| Heavy Vehicle Adjustment Factor (f fv ) | 0.983 | 0.980 | 1.000 | 0.983 |
| Flow Rate (vi), pc/h | 6709 | 964 | 0 | 1282 |
| Weaving Flow Rate (vw), pc/h | 2246 | Freeway Max Capacity (CIFL), pc/h/ln |  | 2350 |
| Non-Weaving Flow Rate (vnw), pc/h | 6709 | Density-Based Capacity (cıwl), pc/h/ln |  | 2094 |
| Total Flow Rate (v), pc/h | 8955 | Demand Flow-Based Capacity (cıw), pc/h |  | 9562 |
| Volume Ratio (VR) | 0.251 | Weaving Segment Capacity (cw), veh/h |  | 9399 |
| Minimum Lane Change Rate (LCmin), Ic/h | 2246 | Adjusted Weaving Area Capacity (cwa), veh/h |  | 9399 |
| Maximum Weaving Length (Lmax), ft | 5064 | Volume-to-Capacity Ratio (v/c) |  | 0.94 |

## Speed and Density

| Non-Weaving Vehicle Index (lnw) | 958 | Average Weaving Speed (Sw), mi/h | 49.3 |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | 1351 | Average Non-Weaving Speed (SNW), mi/h | 40.2 |
| Weaving Lane Change Rate (LCw), Ic/h | 2842 | Average Speed (S), mi/h | 42.2 |
| Total Lane Change Rate (LCAll), Ic/h | 4193 | Density (D), pc/mi/ln | 42.4 |
| Weaving Intensity Factor (W) | 0.457 | Level of Service (LOS) | E |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 1 - Merge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 25.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 950 | 890 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume (Vi), veh/h |  | 6405 | 1575 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 2.50 | 1.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f f v ) |  | 0.976 | 0.985 |  |
| Flow Rate (vi), pc/h |  | 6562 | 1599 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.84 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{DR}_{\mathrm{R}}$ ), pc/mi/ln |  | 32.2 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | 0.543 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1969 |
| Distance to Downstream Ramp (Loww), ft | - | On-Ramp Influence Area Speed (SR), mi/h |  | 52.5 |
| Prop. Freeway Vehicles in Lane 1 and 2 (PFm) | 0.018 | Outer Lanes Freeway Speed (So), mi/h |  | 59.7 |
| Flow in Lanes 1 and 2 (v12), pc/h | 2625 | Ramp Junction Speed (S), mi/h |  | 55.7 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 4224 | Average Density (D), pc/mi/ln |  | 36.6 |
| Level of Service (LOS) | D |  |  |  |
| Copyright © 2017 University of Florida. All Rights Reserv | cation 1 - | ys Version 7.3 <br> dix Derge Analysis - AM.xuf $^{\text {a }}$ | Gene | ted: 10/2/20 |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 1 - Merge Analysis - PM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 65.0 | 1 |  |
| Free-Flow Speed (FFS), mi/h | 950 | 25.0 |  |
| Segment Length (L) / Acceleration Length (LA), ft | Level | 890 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Right |  |
| Adjustmer\| |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 8800 | 945 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.70 | 2.00 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.983 | 0.980 |  |
| Flow Rate (vi), pc/h |  | 8952 | 964 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 1.05 | 0.51 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{DR}^{\text {) , }} \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | - |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2686 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R})}$, mi/h |  | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfm) | 0.097 | Outer Lanes Freeway Speed (So), mi/h |  | 56.2 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3581 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 4545 | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 61.6 |
| Right-Side Lateral Clearance, ft | 0 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 7980 | Heavy Vehicle Adjustment Factor (fнv) | 0.976 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1635 |
| Total Trucks, \% | 2.50 | Capacity (c), pc/h/ln | 2316 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2316 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.71 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 61.4 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.6 | Density (D), pc/mi/ln | 26.6 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 61.6 |  |  |

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## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Basic Freeway Segment - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 61.6 |
| Right-Side Lateral Clearance, ft | 0 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 8800 | Heavy Vehicle Adjustment Factor (frv) | 0.983 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1790 |
| Total Trucks, \% | 1.70 | Capacity (c), pc/h/ln | 2316 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2316 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.77 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 60.5 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.6 | Density (D), pc/mi/ln | 29.6 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 61.6 |  |  |

[^25]
## HCS7 Freeway Diverge Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Diverge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 30.0 |
| Segment Length (L) / Deceleration Length (LD), ft | 1500 | 1500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7980 | 1155 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 2.50 | 1.70 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.976 | 0.983 |  |
| Flow Rate (vi), pc/h |  | 8176 | 1175 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.62 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 27.1 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ds) |  | 0.599 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1975 |
| Distance to Downstream Ramp (Lown), ft | - | Off-Ramp Influence Area Speed (SR), mi/h |  | 51.2 |
| Prop. Freeway Vehicles in Lane 1 and 2 (PfD) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 67.5 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4227 | Ramp Junction Speed (S), mi/h |  | 58.0 |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | - | Average Density (D), pc/mi/ln |  | 35.2 |
| Level of Service (LOS) | C |  |  |  |
|  |  |  |  |  |

## HCS7 Freeway Diverge Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Diverge Analysis - PM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 30.0 |
| Segment Length (L) / Deceleration Length (LD), ft | 1500 | 1500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adju |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 8800 | 1260 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.70 | 1.70 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f f v ) |  | 0.983 | 0.983 |  |
| Flow Rate (vi), pc/h |  | 8952 | 1282 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.95 | 0.67 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), pc/mi/ln |  | 30.5 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ds) |  | 0.608 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2163 |
| Distance to Downstream Ramp (Loww), ft | - | Off-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R})}$, mi/h |  | 51.0 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 66.8 |
| Flow in Lanes 1 and 2 (V12), pc/h | 4626 | Ramp Junction Speed (S), mi/h |  | 57.6 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | - | Average Density (D), pc/mi/ln |  | 38.9 |
| Level of Service (LOS) | D |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Merge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 25.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 6405 | 1575 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 2.50 | 1.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.976 | 0.985 |  |
| Flow Rate (vi), pc/h |  | 6562 | 1599 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.84 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{R}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 28.4 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | 0.512 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1969 |
| Distance to Downstream Ramp (Loown), ft | - | On-Ramp Influence Area Speed (SR), mi/h |  | 53.2 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.018 | Outer Lanes Freeway Speed (So), mi/h |  | 59.7 |
| Flow in Lanes 1 and 2 (v12), pc/h | 2625 | Ramp Junction Speed (S), mi/h |  | 56.1 |
| Flow Entering Ramp-Infl. Area (vr12), pc/h | 4224 | Average Density (D), pc/mi/ln |  | 36.4 |
| Level of Service (LOS) | D |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Merge Analysis - PM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 25.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Sever | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 8800 | 945 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.70 | 2.00 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.983 | 0.980 |  |
| Flow Rate (vi), pc/h |  | 8952 | 964 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 1.05 | 0.51 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | - |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voA), pc/h/ln |  | 2686 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed | ), mi/h | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.097 | Outer Lanes Freeway Speed (So), |  | 56.2 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3581 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 4545 | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Weaving Analysis - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 6 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1720 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 0.83 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 5250 | 1575 | 0 | 1155 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 2.50 | 1.50 | 0.00 | 1.70 |
| Heavy Vehicle Adjustment Factor (f fv ) | 0.976 | 0.985 | 1.000 | 0.983 |
| Flow Rate ( $\mathrm{v}_{\mathrm{i}}$, $\mathrm{pc} / \mathrm{h}$ | 5379 | 1599 | 0 | 1175 |
| Weaving Flow Rate ( $\mathrm{v}_{\mathrm{w}}$ ), pc/h | 2774 | Freeway Max Capacity (cifl), pc/h/ln |  | 2350 |
| Non-Weaving Flow Rate (vnw), pc/h | 5379 | Density-Based Capacity (ciwl), pc/h/ln |  | 2021 |
| Total Flow Rate (v), pc/h | 8153 | Demand Flow-Based Capacity (cıw), pc/h |  | 7059 |
| Volume Ratio (VR) | 0.340 | Weaving Segment Capacity (cw), veh/h |  | 6889 |
| Minimum Lane Change Rate (LCmin), Ic/h | 0 | Adjusted Weaving Area Capacity ( cwa) , veh/h $^{\text {l }}$ |  | 6889 |
| Maximum Weaving Length (Lmax), ft | 6017 | Volume-to-Capacity Ratio (v/c) |  | 1.16 |

## Speed and Density

| Non-Weaving Vehicle Index (lnw) | - | Average Weaving Speed (Sw), mi/h | - |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | - | Average Non-Weaving Speed (Snw), mi/h | - |
| Weaving Lane Change Rate (LCw), Ic/h | - | Average Speed (S), mi/h | - |
| Total Lane Change Rate (LCAll), Ic/h | - | Density (D), pc/mi/ln | - |
| Weaving Intensity Factor (W) | - | Level of Service (LOS) | F |
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Location 1 - I-95 NB - Alternative 2 - Weaving Analysis - AM.xuf

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Alternative 2 - Weaving Analysis - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1720 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), Ic | 0 |
| Interchange Density (ID), int/mi | 0.83 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 6595 | 945 | 0 | 1260 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 1.70 | 2.00 | 0.00 | 1.70 |
| Heavy Vehicle Adjustment Factor (f fv ) | 0.983 | 0.980 | 1.000 | 0.983 |
| Flow Rate ( $\mathrm{v}_{\mathrm{i}}$, $\mathrm{pc} / \mathrm{h}$ | 6709 | 964 | 0 | 1282 |
| Weaving Flow Rate ( $\mathrm{v}_{\mathrm{w}}$ ), pc/h | 2246 | Freeway Max Capacity (ciFL), pc/h/ln |  | 2350 |
| Non-Weaving Flow Rate (vnw), pc/h | 6709 | Density-Based Capacity (ciwl), pc/h/ln |  | 2094 |
| Total Flow Rate (v), pc/h | 8955 | Demand Flow-Based Capacity (ciw), pc/h |  | 9562 |
| Volume Ratio (VR) | 0.251 | Weaving Segment Capacity (cw), veh/h |  | 9399 |
| Minimum Lane Change Rate (LCmin), Ic/h | 2246 | Adjusted Weaving Area Capacity (cwa), veh/h |  | 9399 |
| Maximum Weaving Length (Lmax), ft | 5064 | Volume-to-Capacity Ratio (v/c) |  | 0.94 |

## Speed and Density

| Non-Weaving Vehicle Index (InW) | 958 | Average Weaving Speed (Sw), mi/h | 49.3 |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | 1351 | Average Non-Weaving Speed (SNW), mi/h | 40.2 |
| Weaving Lane Change Rate (LCw), Ic/h | 2842 | Average Speed (S), mi/h | 42.2 |
| Total Lane Change Rate (LCAll), Ic/h | 4193 | Density (D), pc/mi/ln | 42.4 |
| Weaving Intensity Factor (W) | 0.457 | Level of Service (LOS) | E |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Existing Conditions - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.2 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 7600 | Heavy Vehicle Adjustment Factor (fнv) | 0.976 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1947 |
| Total Trucks, \% | 2.50 | Capacity (c), pc/h/ln | 2322 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (cadj), pc/h/ln | 2322 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.84 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 59.1 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 32.9 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.2 |  |  |

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## HCS7 Basic Freeway Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Existing Conditions - Basic Freeway Segment - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.2 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 8800 | Heavy Vehicle Adjustment Factor (fhv) | 0.983 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 2238 |
| Total Trucks, \% | 1.70 | Capacity (c), pc/h/ln | 2322 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2322 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.96 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 53.7 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 41.7 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | E |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.2 |  |  |

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HCS7 ${ }^{\text {TM }}$ Freeways Version 7.3

## HCS7 Freeway Diverge Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Existing Conditions - Diverge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 30.0 |
| Segment Length (L) / Deceleration Length (LD), ft | 860 | 600 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Sever | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7600 | 1100 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 2.50 | 1.70 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.976 | 0.983 |  |
| Flow Rate (vi), pc/h |  | 7787 | 1119 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.83 | 0.59 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area (D) | ), pc/mi/ln | 33.5 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ds) |  | 0.594 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1881 |
| Distance to Downstream Ramp (Lown), ft | - | Off-Ramp Influence Area Speed ( | R), mi/h | 51.3 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.436 | Outer Lanes Freeway Speed (So), | mi/h | 67.9 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4026 | Ramp Junction Speed (S), mi/h |  | 58.2 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | - | Average Density (D), pc/mi/ln |  | 33.4 |
| Level of Service (LOS) | D |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Existing Conditions - Diverge Analysis - PM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 30.0 |
| Segment Length (L) / Deceleration Length (LD), ft | 860 | 600 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume (Vi), veh/h |  | 8800 | 1200 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.70 | 1.70 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.983 | 0.983 |  |
| Flow Rate (vi), pc/h |  | 8952 | 1221 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.95 | 0.64 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 38.3 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ds) |  | 0.603 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2180 |
| Distance to Downstream Ramp (Loown), ft | - | Off-Ramp Influence Area Speed (SR), mi/h |  | 51.1 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 66.7 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4592 | Ramp Junction Speed (S), mi/h |  | 57.7 |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | - | Average Density (D), pc/mi/ln |  | 38.8 |
| Level of Service (LOS) | E |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1 - I-95 NB - Existing Conditions - Merge Analysis - AM |  |  |
| Geometric Data | Freeway | Ramp |  |
|  | 4 | 1 |  |
| Number of Lanes (N) | 65.0 | 25.0 |  |
| Free-Flow Speed (FFS), mi/h | 860 | 620 |  |
| Segment Length (L) / Acceleration Length (LA), ft | Level | Level |  |
| Terrain Type | - | - |  |
| Percent Grade, \% | Freeway | Right |  |
| Segment Type / Ramp Side |  |  |  |
| Adjustment Factors |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 6100 | 1500 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 2.50 | 1.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f f v ) |  | 0.976 | 0.985 |  |
| Flow Rate (vi), pc/h |  | 6250 | 1523 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.83 | 0.80 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{DR}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 32.3 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | 0.508 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1875 |
| Distance to Downstream Ramp (Loown), ft | - | On-Ramp Influence Area Speed (SR), mi/h |  | 53.3 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.027 | Outer Lanes Freeway Speed (So), mi/h |  | 60.0 |
| Flow in Lanes 1 and 2 (v12), pc/h | 2500 | Ramp Junction Speed (S), mi/h |  | 56.3 |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | 4023 | Average Density (D), pc/mi/ln |  | 34.5 |
| Level of Service (LOS) | D |  |  |  |

## D - 24

HCS7 Freeway Merge Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Existing Conditions - Merge Analysis - PM |  |  |
| Geometric Data | Freeway | Ramp |  |
|  | 4 | 1 |  |
| Number of Lanes (N) | 65.0 | 25.0 |  |
| Free-Flow Speed (FFS), mi/h | 860 | 620 |  |
| Segment Length (L) / Acceleration Length (LA), ft | Level | Level |  |
| Terrain Type | - | - |  |
| Percent Grade, \% | Freeway | Right |  |
| Segment Type / Ramp Side |  |  |  |
| Adjustment Factors |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familia |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Seve | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 8800 | 900 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.70 | 2.00 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.983 | 0.980 |  |
| Flow Rate (vi), pc/h |  | 8952 | 918 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 1.05 | 0.48 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{Dr}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | - |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2686 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R}) \text {, mi/h }}$ |  | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (PFM) | 0.103 | Outer Lanes Freeway Speed (So), mi/h |  | 56.2 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3581 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 4499 | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Existing Conditions - Weaving Analysis - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1720 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), IC | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), IC | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 0.83 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 5000 | 1500 | 0 | 1100 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 2.50 | 1.50 | 0.00 | 1.70 |
| Heavy Vehicle Adjustment Factor (f fv ) | 0.976 | 0.985 | 1.000 | 0.983 |
| Flow Rate ( $\mathrm{v}_{\mathrm{i}}$, $\mathrm{pc} / \mathrm{h}$ | 5123 | 1523 | 0 | 1119 |
| Weaving Flow Rate ( $\mathrm{v}_{\mathrm{w}}$ ), pc/h | 2642 | Freeway Max Capacity (ciFL), pc/h/ln |  | 2350 |
| Non-Weaving Flow Rate (vnw), pc/h | 5123 | Density-Based Capacity (ciwl), pc/h/ln |  | 2021 |
| Total Flow Rate (v), pc/h | 7765 | Demand Flow-Based Capacity (ciw), pc/h |  | 7059 |
| Volume Ratio (VR) | 0.340 | Weaving Segment Capacity (cw), veh/h |  | 6889 |
| Minimum Lane Change Rate (LCmin), Ic/h | 0 | Adjusted Weaving Area Capacity (cwa), veh/h |  | 6889 |
| Maximum Weaving Length (Lmax), ft | 6017 | Volume-to-Capacity Ratio (v/c) |  | 1.10 |

## Speed and Density

| Non-Weaving Vehicle Index (lnw) | - | Average Weaving Speed (Sw), mi/h |  |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | - | Average Non-Weaving Speed (SNw), mi/h |  |
| Weaving Lane Change Rate (LCw), Ic/h | - | Average Speed (S), mi/h |  |
| Total Lane Change Rate (LCAll), Ic/h | - | Density (D), pc/mi/ln |  |
| Weaving Intensity Factor (W) | - | Level of Service (LOS) |  |

Managed Lane Geometric Data

| Number of Managed Lanes, In | 1 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Managed Lane Length, ft | 5280 | Percent Grade, \% | - |

## Managed Lane Adjustment Factors

| Driver Population | All Familiar | Driver Population CAF | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Weather Type CAF | 1.000 |
| Driver Population SAF | 1.000 | Final Speed Adjustment Factor (SAF) | 1.000 |
| Weather Type SAF | 1.000 | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Demand Adjustment Factor (DAF) | 1.000 |  |  |

Managed Lane Demand and Capacity

| Volume (VML), veh/h | 0 | Heavy Vehicle Adjustment Factor (f frv ) | 1.000 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor | 0.94 | Flow Rate (Vp,ML), pc/h/ln | 0 |
| Total Trucks, \% | 0.00 | Capacity (c), pc/h/ln | 1804 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Cpacity (Cadj), pc/h/ln | 1804 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.00 |
| Passenger Car Equivalent (ET) |  |  |  |

Managed Lane Speed and Density

| Breakpoint (ВРмц) | 501 | Indicator Variable | 0 |
| :--- | :--- | :--- | :--- |
| Speed $1\left(\mathrm{~S}_{1}\right), \mathrm{mi} / \mathrm{h}$ | 75.4 | Average Speed (SmL), mi/h | 75.4 |
| Speed 2 (S2), mi/h | 0.0 | Density (DмL), pc/mi/ln | 0.0 |
| Speed 2 (S3), mi/h | 0.0 | Level of Service (LOS) | A |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 1-I-95 NB - Existing Conditions - Weaving Analysis - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1720 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), lc | 0 |
| Interchange Density (ID), int/mi | 0.83 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR |  |
| :--- | :--- | :--- | :--- | :--- |
| Volume (Vi), veh/h | 6700 | 900 | 0 | 1200 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 1.70 | 2.00 | 1.00 |  |
| Heavy Vehicle Adjustment Factor (fнv) | 0.983 | 0.980 | 1.000 | 0.983 |
| Flow Rate (vi), pc/h | 6816 | 918 | 1221 |  |
| Weaving Flow Rate (vw), pc/h | 2139 | Density-Based Capacity (ciwL), pc/h/ln | 2104 |  |
| Non-Weaving Flow Rate (vnw), pc/h | 6816 | Demand Flow-Based Capacity (ciw), pc/h | 10042 |  |
| Total Flow Rate (v), pc/h | Weaving Segment Capacity (cw), veh/h | 9871 |  |  |
| Volume Ratio (VR) | Adjusted Weaving Area Capacity (cwa), veh/h | 9871 |  |  |
| Minimum Lane Change Rate (LCMin), Ic/h | 2139 | Volume-to-Capacity Ratio (v/c) | 2350 |  |
| Maximum Weaving Length (Lmax), ft | 4939 | 0.239 |  | 0.89 |

## Speed and Density

| Non-Weaving Vehicle Index (lnw) | 973 | Average Weaving Speed (Sw), mi/h | 49.5 |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | 1373 | Average Non-Weaving Speed (SNw), mi/h | 41.0 |
| Weaving Lane Change Rate (LCw), Ic/h | 2735 | Average Speed (S), mi/h | 42.8 |
| Total Lane Change Rate (LCAll), Ic/h | 4108 | Density (D), pc/mi/ln | 41.8 |
| Weaving Intensity Factor (W) | 0.449 | Level of Service (LOS) | E |

## HCS7 Freeway Diverge Report

## Project Information

| Analyst |  |  | Date |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | $9 / 1 / 2017$ |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - 2030 No Build - Diverge Analysis - AM |  |  |
| Geometric Data | Freeway | Ramp |  |
|  | 4 | 1 |  |
| Number of Lanes (N) | 65.0 | 30.0 |  |
| Free-Flow Speed (FFS), mi/h | 1500 | 1240 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | Level |  |
| Terrain Type | - | - |  |
| Percent Grade, \% | Freeway | Right |  |
| Segment Type / Ramp Side |  |  |  |
| Adjustmer\| |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familia |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Seve | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7875 | 2205 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 3.40 | 3.40 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.967 | 0.967 |  |
| Flow Rate (vi), pc/h |  | 8144 | 2280 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 1.20 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | - |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1654 |
| Distance to Downstream Ramp (Loown), ft | 10000 | Off-Ramp Influence Area Speed ( | ), mi/h | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.436 | Outer Lanes Freeway Speed (So), |  | 68.8 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4837 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | - | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2-I-93 SB - 2030 No Build - Merge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 35.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1100 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume (Vi), veh/h |  | 7718 | 158 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 3.40 | 10.90 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.967 | 0.902 |  |
| Flow Rate (vi), pc/h |  | 7981 | 175 |  |
| Capacity (c), pc/h |  | 9400 | 2000 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.09 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{R}_{\mathrm{R})}, \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 24.8 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | 0.357 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2395 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R}}$, mi/h |  | 56.8 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.196 | Outer Lanes Freeway Speed (So), mi/h |  | 57.9 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3192 | Ramp Junction Speed (S), mi/h |  | 57.4 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 3367 | Average Density (D), pc/mi/ln |  | 35.5 |
| Level of Service (LOS) | C |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - Alternative 1- Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.2 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 7875 | Heavy Vehicle Adjustment Factor (frv) | 0.967 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1629 |
| Total Trucks, \% | 3.40 | Capacity (c), pc/h/ln | 2322 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2322 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.70 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 62.0 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 26.3 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.2 |  |  |

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## HCS7 Freeway Diverge Report

## Project Information

| Analyst |  |  | Date |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | $9 / 1 / 2017$ |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - Alternative 1 - Diverge Analysis - AM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 6017 |  |  |
| Free-Flow Speed (FFS), mi/h | 65.0 | 1 |  |
| Segment Length (L) / Deceleration Length (LD), ft | 1500 | 30.0 |  |
| Terrain Type | Level | 1500 |  |
| Percent Grade, \% | - | Level |  |
| Segment Type / Ramp Side | Freeway | - |  |
| Adjustment Factors |  | Right |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Sever | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7875 | 2205 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 3.40 | 3.40 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.967 | 0.967 |  |
| Flow Rate (vi), pc/h |  | 8144 | 2280 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 1.20 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LeQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | - |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1654 |
| Distance to Downstream Ramp (Lown), ft | 10000 | Off-Ramp Influence Area Speed | ), mi/h | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.436 | Outer Lanes Freeway Speed (So), |  | 68.8 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4837 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | - | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - Alternative 1- Merge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 35.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adju |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familia |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Seve | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7718 | 158 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 3.40 | 10.90 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.967 | 0.902 |  |
| Flow Rate (vi), pc/h |  | 7981 | 175 |  |
| Capacity (c), pc/h |  | 9400 | 2000 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.09 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area | ), pc/mi/ln | 22.3 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | 0.329 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2395 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( | ), mi/h | 57.4 |
| Prop. Freeway Vehicles in Lane 1 and 2 (PFM) | 0.196 | Outer Lanes Freeway Speed (So), |  | 57.9 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3192 | Ramp Junction Speed (S), mi/h |  | 57.7 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 3367 | Average Density (D), pc/mi/ln |  | 35.3 |
| Level of Service (LOS) | C |  |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - Alternative 3 - Basic Freeway Segment 2 (After 37B) - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.2 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 5880 | Heavy Vehicle Adjustment Factor (fhv) | 0.967 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 2027 |
| Total Trucks, \% | 3.40 | Capacity (c), pc/h/ln | 2322 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2322 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.87 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 57.9 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 35.0 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.2 |  |  |

[^26]
## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - Alternative 3 - Diverge Analysis - AM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 65.0 | 2 |  |
| Free-Flow Speed (FFS), mi/h | 1500 | 30.0 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | 3980 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Right |  |
| Adjustment Factors |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Sever | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7875 | 2205 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 3.40 | 3.40 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.967 | 0.967 |  |
| Flow Rate (vi), pc/h |  | 8144 | 2280 |  |
| Capacity (c), pc/h |  | 9400 | 3800 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.60 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - | Density in Ramp Influence Area (D) | ), pc/mi/ln | 1.2 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | 0.698 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2170 |
| Distance to Downstream Ramp (Loown), ft | 10000 | Off-Ramp Influence Area Speed (Sk), | ), mi/h | 48.9 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.260 | Outer Lanes Freeway Speed (So), | i/h | 66.7 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3805 | Ramp Junction Speed (S), mi/h |  | 57.0 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | - | Average Density (D), pc/mi/ln |  | 35.7 |
| Level of Service (LOS) | A |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - Existing Conditions - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.83 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.2 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 7500 | Heavy Vehicle Adjustment Factor (frv) | 0.967 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1939 |
| Total Trucks, \% | 3.40 | Capacity (c), pc/h/ln | 2322 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2322 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.84 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 59.3 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 32.7 |
| Total Ramp Density Adjustment | 2.8 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.2 |  |  |

[^27]
## HCS7 Freeway Diverge Report

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-93 SB - Existing Conditions - Diverge Analysis - AM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 65.0 | 1 |  |
| Free-Flow Speed (FFS), mi/h | 1500 | 30.0 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | 1240 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Right |  |
| Adjustmer\| |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7500 | 2100 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 3.40 | 3.40 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.967 | 0.967 |  |
| Flow Rate (vi), pc/h |  | 7756 | 2172 |  |
| Capacity (c), pc/h |  | 9400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.83 | 1.14 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - |  |  | - |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | - |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1575 |
| Distance to Downstream Ramp (Lown), ft | 10000 | Off-Ramp Influence Area Speed (SR), mi/h |  | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 69.1 |
| Flow in Lanes 1 and 2 (v12), pc/h | 4607 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | - | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2-I-93 SB - Existing Conditions - Merge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 65.0 | 35.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1100 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familia |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Seve | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7350 | 150 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 3.40 | 10.90 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.967 | 0.902 |  |
| Flow Rate (vi), pc/h |  | 7601 | 166 |  |
| Capacity (c), pc/h |  | 9400 | 2000 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.83 | 0.08 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 23.6 |
| Distance to Upstream Ramp (Lup), ft | 10000 | Speed Index (Ms) |  | 0.340 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 2281 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R})}$, mi/h |  | 57.2 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.197 | Outer Lanes Freeway Speed (So), mi/h |  | 58.6 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3040 | Ramp Junction Speed (S), mi/h |  | 58.0 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 3206 | Average Density (D), pc/mi/ln |  | 33.5 |
| Level of Service (LOS) | C |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $8 / 30 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-95 SB - 2030 No Build - Basic Freeway Segment 2 (Before 36) - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 55.0 | Total Ramp Density (TRD), ramps/mi | 1.17 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 51.3 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 6930 | Heavy Vehicle Adjustment Factor (frv) | 0.992 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1746 |
| Total Trucks, \% | 0.80 | Capacity (c), pc/h/ln | 2213 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2213 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.79 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 51.3 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 34.0 |
| Total Ramp Density Adjustment | 3.7 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 51.3 |  |  |

[^28]
## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2-I-95 SB - 2030 No Build - Diverge Analysis (Commerce) - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 30.0 |
| Segment Length (L) / Deceleration Length (LD), ft | 1500 | 485 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Highway/CD Roadway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 6930 | 630 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 0.80 | 0.80 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f f v ) |  | 0.992 | 0.992 |  |
| Flow Rate (vi), pc/h |  | 6986 | 635 |  |
| Capacity (c), pc/h |  | 8400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.83 | 0.33 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 29.2 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | 0.550 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1791 |
| Distance to Downstream Ramp (Loown), ft | - | Off-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R}}$, mi/h |  | 47.8 |
| Prop. Freeway Vehicles in Lane 1 and 2 (PfD) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 57.3 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3404 | Ramp Junction Speed (S), mi/h |  | 52.2 |
| Flow Entering Ramp-Infl. Area (vr12), pc/h | - | Average Density (D), pc/mi/ln |  | 33.5 |
| Level of Service (LOS) | D |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $8 / 30 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-95 SB - 2030 No Build - Merge Analysis (Commerce) - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 30.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 730 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume (Vi), veh/h |  | 6300 | 1260 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 0.80 | 3.80 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.992 | 0.963 |  |
| Flow Rate (vi), pc/h |  | 6351 | 1308 |  |
| Capacity (c), pc/h |  | 9000 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.85 | 0.69 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 30.4 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ms) |  | 0.460 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1906 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R}}$, mi/h |  | 49.0 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.054 | Outer Lanes Freeway Speed (So), mi/h |  | 49.9 |
| Flow in Lanes 1 and 2 (v12), pc/h | 2540 | Ramp Junction Speed (S), mi/h |  | 49.4 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 3848 | Average Density (D), pc/mi/ln |  | 38.8 |
| Level of Service (LOS) | D |  |  |  |

## Project Information

| Analyst |  | Date | $8 / 30 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2-I-95 SB - 2030 No Build - Merge Analysis (I-93) - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 30.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |

## Adjustment Factors



## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2-I-95 SB - 2030 No Build - Weaving Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1450 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCRR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 1.17 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 4095 | 2205 | 0 | 630 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 0.80 | 0.80 | 0.00 | 0.80 |
| Heavy Vehicle Adjustment Factor (f fv ) | 0.992 | 0.992 | 1.000 | 0.992 |
| Flow Rate (vi), pc/h | 4128 | 2223 | 0 | 635 |
| Weaving Flow Rate ( vw ), pc/h | 2858 | Freeway Max Capacity (CIFL), pc/h/ln |  | 2250 |
| Non-Weaving Flow Rate (vnw), pc/h | 4128 | Density-Based Capacity (ciwl), pc/h/ln |  | 1842 |
| Total Flow Rate (v), pc/h | 6986 | Demand Flow-Based Capacity (ciw), pc/h |  | 5868 |
| Volume Ratio (VR) | 0.409 | Weaving Segment Capacity (cw), veh/h |  | 5821 |
| Minimum Lane Change Rate (LCmin), Ic/h | 0 | Adjusted Weaving Area Capacity ( $\mathrm{Cwa}^{\text {a }}$, veh/h |  | 5821 |
| Maximum Weaving Length (Lmax), ft | 6782 | Volume-to-Capacity Ratio (v/c) |  | 1.19 |

## Speed and Density

| Non-Weaving Vehicle Index (lnw) | - | Average Weaving Speed (Sw), mi/h | - |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | - | Average Non-Weaving Speed (SNw), mi/h | - |
| Weaving Lane Change Rate (LCw), Ic/h | - | Average Speed (S), mi/h | - |
| Total Lane Change Rate (LCAll), Ic/h | - | Density (D), pc/mi/ln | - |
| Weaving Intensity Factor (W) | - | Level of Service (LOS) | F |
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Location 2-I-95 SB-2030 No Build - Weaving Segment - AM.xuf
Appendix D

## D -43

HCS7 Freeway Merge Report

## Project Information

| Analyst |  | Date | 8/30/2017 |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-95 SB - Alternative 2 - Merge Analysis (Commerce) - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 30.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1230 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |
| Adjus |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume (Vi), veh/h |  | 6300 | 1260 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 0.80 | 3.80 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.992 | 0.963 |  |
| Flow Rate (vi), pc/h |  | 6351 | 1308 |  |
| Capacity (c), pc/h |  | 9000 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.85 | 0.69 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{Dr}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 27.2 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ms) |  | 0.430 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1906 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R}}$, mi/h |  | 49.4 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғм) | 0.054 | Outer Lanes Freeway Speed (So), mi/h |  | 49.9 |
| Flow in Lanes 1 and 2 (v12), pc/h | 2540 | Ramp Junction Speed (S), mi/h |  | 49.6 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 3848 | Average Density (D), pc/mi/ln |  | 38.6 |
| Level of Service (LOS) | C |  |  |  |

## Project Information

| Analyst |  | Date | $8 / 30 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-95 SB - Alternative 3 - Basic Freeway Segment 2 (Before 36) - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 55.0 | Total Ramp Density (TRD), ramps/mi | 1.17 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 50.7 |
| Right-Side Lateral Clearance, ft | 0 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 6930 | Heavy Vehicle Adjustment Factor (frv) | 0.992 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1397 |
| Total Trucks, \% | 0.80 | Capacity (c), pc/h/ln | 2207 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2207 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.63 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 50.7 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.6 | Density (D), pc/mi/ln | 27.6 |
| Total Ramp Density Adjustment | 3.7 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 50.7 |  |  |

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Location 2 - I-95 SB - Alternative 3 - Basic Freeway Segment 2 (Before 36) - AM.xuf

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-95 SB - Alternative 3 - Diverge Analysis (Commerce) - AM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 55.0 | 1 |  |
| Free-Flow Speed (FFS), mi/h | 1500 | 30.0 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | 1500 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Highway/CD Roadway | Right |  |
| Segment Type / Ramp Side |  | - |  |
| Adjustment Factors |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familia |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Seve | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7277 | 662 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 0.80 | 0.80 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.992 | 0.992 |  |
| Flow Rate (vi), pc/h |  | 7336 | 667 |  |
| Capacity (c), pc/h |  | 8400 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.87 | 0.35 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area (Dr), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 21.5 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | 0.553 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1881 |
| Distance to Downstream Ramp (Lown), ft | - | Off-Ramp Influence Area Speed (SR), mi/h |  | 47.8 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.436 | Outer Lanes Freeway Speed (So), mi/h |  | 56.9 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3575 | Ramp Junction Speed (S), mi/h |  | 52.1 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | - | Average Density (D), pc/mi/ln |  | 35.2 |
| Level of Service (LOS) | C |  |  |  |
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## Project Information

| Analyst |  | Date | $8 / 30 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-95 SB - Alternative 3 - Merge Analysis (I-93) - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 2 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 30.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 4500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familia |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Seve | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 4725 | 2205 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 0.80 | 0.80 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.992 | 0.992 |  |
| Flow Rate ( $\mathrm{v}_{\mathrm{i}}$, $\mathrm{pc} / \mathrm{h}$ |  | 4763 | 2223 |  |
| Capacity (c), pc/h |  | 9000 | 3800 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.78 | 0.59 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 8.5 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ms) |  | 0.293 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1429 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R}}$, mi/h |  | 51.2 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Рғm) | 0.209 | Outer Lanes Freeway Speed (So), mi/h |  | 51.7 |
| Flow in Lanes 1 and 2 (v12), pc/h | 1905 | Ramp Junction Speed (S), mi/h |  | 51.4 |
| Flow Entering Ramp-Infl. Area (vR12), pc/h | 4128 | Average Density (D), pc/mi/ln |  | 34.0 |
| Level of Service (LOS) | A |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 1 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2-I-95 SB - Alternative 3 - Weaving Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 5 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1450 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 2 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), Ic | 0 |
| Interchange Density (ID), int/mi | 1.17 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$, veh/h | 4095 | 2205 | 0 | 630 |
| Peak Hour Factor (PHF) | 1.00 | 1.00 | 1.00 | 1.00 |
| Total Trucks, \% | 0.80 | 0.80 | 0.00 | 0.80 |
| Heavy Vehicle Adjustment Factor (f fv ) | 0.992 | 0.992 | 1.000 | 0.992 |
| Flow Rate (vi), pc/h | 4128 | 2223 | 0 | 635 |
| Weaving Flow Rate (vw), pc/h | 2858 | Freeway Max Capacity (CIFL), pc/h/ln |  | 2250 |
| Non-Weaving Flow Rate (vnw), pc/h | 4128 | Density-Based Capacity (cıwl), pc/h/ln |  | 1842 |
| Total Flow Rate (v), pc/h | 6986 | Demand Flow-Based Capacity (cıw), pc/h |  | 5868 |
| Volume Ratio (VR) | 0.409 | Weaving Segment Capacity (cw), veh/h |  | 5821 |
| Minimum Lane Change Rate (LCmin), Ic/h | 0 | Adjusted Weaving Area Capacity (cwa), veh/h |  | 5821 |
| Maximum Weaving Length (Lmax), ft | 6782 | Volume-to-Capacity Ratio (v/c) |  | 1.19 |

## Speed and Density



Appendix D

## Project Information

| Analyst |  | Date | $8 / 30 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 2 - I-95 SB - Existing Conditions - Merge Analysis (I-93) - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 30.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Right |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 4500 | 2100 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 0.80 | 0.80 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.992 | 0.992 |  |
| Flow Rate (vi), pc/h |  | 4536 | 2117 |  |
| Capacity (c), pc/h |  | 9000 | 1900 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.74 | 1.11 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LeQ), ft | - | Density in Ramp Influence Area ( $\mathrm{DR}^{\text {) , }} \mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ms) |  | - |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1361 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed (SR), mi/h |  | - |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfm) | 0.000 | Outer Lanes Freeway Speed (So), mi/h |  | 51.9 |
| Flow in Lanes 1 and 2 (v12), pc/h | 1814 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | 3931 | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 11 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3 - I-93 SB - 2030 No Build - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | Percent Grade, \% | - |  |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 55.0 | Total Ramp Density (TRD), ramps/mi | 1.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 51.8 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 7245 | Heavy Vehicle Adjustment Factor (fнv) | 0.982 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1844 |
| Total Trucks, \% | 1.80 | Capacity (c), pc/h/ln | 2218 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (cadj), pc/h/ln | 2218 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.83 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 51.8 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 35.6 |
| Total Ramp Density Adjustment | 3.2 | Level of Service (LOS) | E |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 51.8 |  |  |

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## Project Information

| Analyst |  | Date | $9 / 11 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3 - I-93 SB - 2030 No Build - Merge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 1 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 50.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 1500 | 1000 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Left |

## Adjustment Factors



## Project Information

| Analyst |  | Date | $9 / 11 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3 - I-93 SB - Alternative 3 - Merge Analysis - AM |  |  |

Geometric Data

|  | Freeway | Ramp |
| :--- | :--- | :--- |
| Number of Lanes (N) | 4 | 2 |
| Free-Flow Speed (FFS), mi/h | 55.0 | 50.0 |
| Segment Length (L) / Acceleration Length (LA), ft | 3000 | 3500 |
| Terrain Type | Level | Level |
| Percent Grade, \% | - | - |
| Segment Type / Ramp Side | Freeway | Left |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume (Vi), veh/h |  | 4830 | 2415 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.80 | 5.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.982 | 0.948 |  |
| Flow Rate (vi), pc/h |  | 4919 | 2547 |  |
| Capacity (c), pc/h |  | 9000 | 4200 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.83 | 0.61 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 17.6 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ms) |  | 0.327 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1476 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R}}$, mi/h |  | 50.7 |
| Prop. Freeway Vehicles in Lane 3 and 4 (PFM) | 0.209 | Outer Lanes Freeway Speed (So), mi/h |  | 51.5 |
| Flow in Lanes 3 and 4 (V34), pc/h | 1968 | Ramp Junction Speed (S), mi/h |  | 51.0 |
| Flow Entering Ramp-Infl. Area (VR34), pc/h | 4515 | Average Density (D), pc/mi/ln |  | 36.6 |
| Level of Service (LOS) | B |  |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst |  | Date | $9 / 11 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3 - I-93 SB - Existing Conditions - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 55.0 | Total Ramp Density (TRD), ramps/mi | 1.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 51.8 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 6900 | Heavy Vehicle Adjustment Factor (fhv) | 0.982 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1756 |
| Total Trucks, \% | 1.80 | Capacity (c), pc/h/ln | 2218 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2218 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.79 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 51.8 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 33.9 |
| Total Ramp Density Adjustment | 3.2 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 51.8 |  |  |

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HCS7 ${ }^{\text {TM }}$ Freeways Version 7.3

## Project Information

| Analyst |  | Date | $9 / 11 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3-I-93 SB - Existing Conditions - Merge Analysis - AM |  |  |
| Geometric Data | Freeway | Ramp |  |
|  | 4 | 1 |  |
| Number of Lanes (N) | 55.0 | 50.0 |  |
| Free-Flow Speed (FFS), mi/h | 1500 | 1500 |  |
| Segment Length (L) / Acceleration Length (LA), ft | Level | Level |  |
| Terrain Type | - | - |  |
| Percent Grade, \% | Freeway | Left |  |
| Segment Type / Ramp Side |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 4600 | 2300 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.80 | 5.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.982 | 0.948 |  |
| Flow Rate (vi), pc/h |  | 4684 | 2426 |  |
| Capacity (c), pc/h |  | 9000 | 2100 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.79 | 1.16 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | - |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ms) |  | - |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1405 |
| Distance to Downstream Ramp (Lown), ft | - | On-Ramp Influence Area Speed (SR), mi/h |  | - |
| Prop. Freeway Vehicles in Lane 3 and 4 (Рғм) | 0.000 | Outer Lanes Freeway Speed (So), mi/h |  | 51.7 |
| Flow in Lanes 3 and 4 (v34), pc/h | 1874 | Ramp Junction Speed (S), mi/h |  | - |
| Flow Entering Ramp-Infl. Area (vR34), pc/h | 4300 | Average Density (D), pc/mi/ln |  | - |
| Level of Service (LOS) | F |  |  |  |
|  |  |  |  |  |

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3 - Route 24 NB - 2030 No Build - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.67 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.7 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 4830 | Heavy Vehicle Adjustment Factor (frv) | 0.948 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1698 |
| Total Trucks, \% | 5.50 | Capacity (c), pc/h/ln | 2327 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2327 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.73 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 62.0 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 27.4 |
| Total Ramp Density Adjustment | 2.3 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.7 |  |  |

[^29]
## HCS7 Basic Freeway Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3 - Route 24 NB - Alternative 1 \& 2 - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.67 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 61.5 |
| Right-Side Lateral Clearance, ft | 0 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 4830 | Heavy Vehicle Adjustment Factor (fhv) | 0.948 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1274 |
| Total Trucks, \% | 5.50 | Capacity (c), pc/h/ln | 2315 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2315 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.55 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 61.5 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 1.2 | Density (D), pc/mi/ln | 20.7 |
| Total Ramp Density Adjustment | 2.3 | Level of Service (LOS) | C |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 61.5 |  |  |

[^30]HCS7 ${ }^{\text {TM }}$ Freeways Version 7.3
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## HCS7 Basic Freeway Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 3 - Route 24 NB - Existing Conditions - Basic Freeway Segment - AM |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.67 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.7 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 4600 | Heavy Vehicle Adjustment Factor (frv) | 0.948 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1617 |
| Total Trucks, \% | 5.50 | Capacity (c), pc/h/ln | 2327 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2327 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.70 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 62.5 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 25.9 |
| Total Ramp Density Adjustment | 2.3 | Level of Service (LOS) | C |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.7 |  |  |

[^31]
## HCS7 Freeway Diverge Report

## Project Information

| Analyst |  | Date | $9 / 13 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 4 - I-93 NB - Existing Conditions - Diverge Analysis - PM |  |  |
| Geometric Data | Freeway | Ramp |  |
|  | 4 | 2 |  |
| Number of Lanes (N) | 55.0 | 50.0 |  |
| Free-Flow Speed (FFS), mi/h | 1500 | 2500 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | Level |  |
| Terrain Type | - | - |  |
| Percent Grade, \% | Freeway | Right |  |
| Segment Type / Ramp Side |  |  |  |
| Adjustmer\| |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familia |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Seve | Weather |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 6600 | 2700 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 4.20 | 0.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (f fv ) |  | 0.960 | 0.995 |  |
| Flow Rate (vi), pc/h |  | 6875 | 2714 |  |
| Capacity (c), pc/h |  | 9000 | 4200 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.76 | 0.65 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (LEQ), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{r}}$ ), $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 14.4 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | 0.477 |
| Downstream Equilibrium Distance (Leq), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1540 |
| Distance to Downstream Ramp (Lown), ft | - | Off-Ramp Influence Area Speed (SR), mi/h |  | 48.8 |
| Prop. Freeway Vehicles in Lane 1 and 2 (Pfd) | 0.260 | Outer Lanes Freeway Speed (So), mi/h |  | 58.2 |
| Flow in Lanes 1 and 2 (v12), pc/h | 3796 | Ramp Junction Speed (S), mi/h |  | 52.6 |
| Flow Entering Ramp-Infl. Area (VR12), pc/h | - | Average Density (D), pc/mi/ln |  | 32.7 |
| Level of Service (LOS) | B |  |  |  |

HCS7 Freeway Diverge Report

## Project Information

| Analyst |  |  | Date |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | $9 / 13 / 2017$ |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 4 - I-93 SB - Existing Conditions - Diverge Analysis - PM |  |  |
| Geometric Data | Freeway |  |  |
|  | 4 | Ramp |  |
| Number of Lanes (N) | 55.0 | 2 |  |
| Free-Flow Speed (FFS), mi/h | 1500 | 50.0 |  |
| Segment Length (L) / Deceleration Length (LD), ft | Level | 2500 |  |
| Terrain Type | - | Level |  |
| Percent Grade, \% | Freeway | - |  |
| Segment Type / Ramp Side |  | Left |  |
| Adjustmer\| |  |  |  |

## Adjustment Factors

| Driver Population |  | All Familiar | All Familiar |  |
| :---: | :---: | :---: | :---: | :---: |
| Weather Type |  | Non-Severe Weather | Non-Severe Weather |  |
| Incident Type |  | No Incident | - |  |
| Final Speed Adjustment Factor (SAF) |  | 1.000 | 1.000 |  |
| Final Capacity Adjustment Factor (CAF) |  | 1.000 | 1.000 |  |
| Demand Adjustment Factor (DAF) |  | 1.000 | 1.000 |  |
| Demand and Capacity |  |  |  |  |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h |  | 7800 | 2600 |  |
| Peak Hour Factor (PHF) |  | 1.00 | 1.00 |  |
| Total Trucks, \% |  | 1.80 | 0.50 |  |
| Single-Unit Trucks (SUT), \% |  | - | - |  |
| Tractor-Trailers (TT), \% |  | - | - |  |
| Heavy Vehicle Adjustment Factor (fhv) |  | 0.982 | 0.995 |  |
| Flow Rate (vi), pc/h |  | 7943 | 2613 |  |
| Capacity (c), pc/h |  | 9000 | 4200 |  |
| Volume-to-Capacity Ratio (v/c) |  | 0.88 | 0.62 |  |
| Speed and Density |  |  |  |  |
| Upstream Equilibrium Distance (Leq), ft | - | Density in Ramp Influence Area ( $\mathrm{D}_{\mathrm{R}}$, $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ |  | 19.6 |
| Distance to Upstream Ramp (Lup), ft | - | Speed Index (Ds) |  | 0.468 |
| Downstream Equilibrium Distance (LEQ), ft | - | Flow Outer Lanes (voa), pc/h/ln |  | 1772 |
| Distance to Downstream Ramp (Lown), ft | - | Off-Ramp Influence Area Speed ( $\mathrm{S}_{\mathrm{R})}$, mi/h |  | 48.9 |
| Prop. Freeway Vehicles in Lane 3 and 4 (PfD) | 0.260 | Outer Lanes Freeway Speed (So), mi/h |  | 57.3 |
| Flow in Lanes 3 and 4 (v34), pc/h | 4399 | Ramp Junction Speed (S), mi/h |  | 52.3 |
| Flow Entering Ramp-Infl. Area (VR34), pc/h | - | Average Density (D), pc/mi/ln |  | 38.0 |
| Level of Service (LOS) | B |  |  |  |
|  |  |  |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 4 - Route 24 SB - 2030 No Build - Basic Freeway Segment - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.67 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.7 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 5565 | Heavy Vehicle Adjustment Factor (fuv) | 0.997 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1861 |
| Total Trucks, \% | 0.30 | Capacity (c), pc/h/ln | 2327 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (cadj), pc/h/ln | 2327 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.80 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 60.6 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 30.7 |
| Total Ramp Density Adjustment | 2.3 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.7 |  |  |

[^32]
## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 4 - Route 24 SB - Alternative 1- Basic Freeway Segment - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 4 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.67 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 61.5 |
| Right-Side Lateral Clearance, ft | 0 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 5565 | Heavy Vehicle Adjustment Factor (fuv) | 0.997 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1396 |
| Total Trucks, \% | 0.30 | Capacity (c), pc/h/ln | 2315 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (cadj), pc/h/ln | 2315 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.60 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 61.5 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 1.2 | Density (D), pc/mi/ln | 22.7 |
| Total Ramp Density Adjustment | 2.3 | Level of Service (LOS) | C |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 61.5 |  |  |

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## HCS7 Basic Freeway Report

## Project Information

| Analyst |  | Date | $9 / 6 / 2017$ |
| :--- | :--- | :--- | :--- |
| Agency |  | Analysis Year | 2017 |
| Jurisdiction |  | Time Period Analyzed |  |
| Project Description | Location 4 - Route 24 SB - Existing Conditions - Basic Freeway Segment - PM |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 65.0 | Total Ramp Density (TRD), ramps/mi | 0.67 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 62.7 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 5300 | Heavy Vehicle Adjustment Factor (fuv) | 0.997 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 1.00 | Flow Rate (vp), pc/h/ln | 1772 |
| Total Trucks, \% | 0.30 | Capacity (c), pc/h/ln | 2327 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (cadj), pc/h/ln | 2327 |
| Tractor-Trailers (TT), \% | - | Volume-to-Capacity Ratio (v/c) | 0.76 |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 61.5 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (fRLC) | 0.0 | Density (D), pc/mi/ln | 28.8 |
| Total Ramp Density Adjustment | 2.3 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 62.7 |  |  |

[^33]
[^0]:    ${ }^{1}$ Federal Highway Administration, Recurring Traffic Bottlenecks: A Primer: Focus on Low-Cost Operations Improvements, US Department of Transportation, Federal Highway Administration, June 2009, p. 1.

[^1]:    ${ }^{2}$ Seth Asante, MPO staff, memorandum to the Transportation Planning and Programming Committee of the Boston Region MPO, "Low-Cost Improvements to Bottleneck Locations, Phase I," June 2, 2011.
    ${ }^{3}$ Chen-Yuan Wang, MPO staff, memorandum to the Transportation Planning and Programming Committee of the Boston Region MPO, "Low-Cost Improvements to Bottleneck Locations, Phase II," March 12, 2012.
    ${ }^{4}$ Seth Asante, MPO staff, memorandum to the Transportation Planning and Programming Committee of the Boston Region MPO, "Low-Cost Improvements to Express-Highway Bottleneck Locations," December 3, 2015.

[^2]:    ${ }^{5}$ Seth Asante, MPO staff, memorandum to the Boston Region MPO, "Low-Cost Improvements to Express-Highway Bottleneck Locations: Selection of Study Locations," April 2, 2015.

[^3]:    ${ }^{6}$ Highway Capacity Manual 2010, Transportation Research Board of the National Academies, Washington, DC, December 2010.
    ${ }^{7}$ Highway Capacity Software 7, Version 7.3, McTrans Center, PO Box 116585, Gainesville, Florida, 2017.

[^4]:    ${ }^{8}$ The AM peak period is 6:00 AM to 10:00 AM, and the PM peak period is 3:00 PM to 7:00 PM. Source: Central Transportation Planning Staff.
    ${ }^{9}$ Acceleration and deceleration lanes are measured from the point where the lane reaches 12 feet wide to the first controlling curve. Source: A Policy on Geometric Design of Highways and Streets, AASHTO, 2004. Chapter 10 Grade Separations and Interchanges.

[^5]:    ${ }^{10}$ Highway Capacity Software 7, Version 7.3, McTrans Center, PO Box 116585, Gainesville, Florida, 2017.

[^6]:    ${ }^{11}$ American Association of State Highway and Transportation Officials. Highway Safety Manual. Washington, DC, 2010.
    ${ }^{12}$ Crash Modification Factors Clearinghouse, www.cmfclearinghouse.org/index.cfm.

[^7]:    ${ }^{13}$ The AM peak period is 6:00 AM to 10:00 AM, and the PM peak period is 3:00 PM to 7:00 PM. Source: Central Transportation Planning Staff.

[^8]:    ${ }^{14}$ Acceleration and deceleration lanes are measured from the point where the lane reaches 12 feet wide to the first controlling curve. Source: A Policy on Geometric Design of Highways and Streets, AASHTO, 2004. Chapter 10 Grade Separations and Interchanges.

[^9]:    ${ }^{15} 200$ vehicles per hour estimate uses a one-mile queue of vehicles spaced with 25 -foot headways.

[^10]:    ${ }^{16}$ Highway Capacity Software 7, Version 7.3, McTrans Center, PO Box 116585, Gainesville, Florida, 2017.

[^11]:    ${ }^{\text {a }}$ Uses an acceleration lane of 1,500 feet as an approximation for a full auxiliary lane in the Alternative 1 and Alternative 3 merge and diverge models.
    ${ }^{\mathrm{b}} \mathrm{HCM}$ does not provide density and speed data for scenarios that result in LOS F.
    ${ }^{\text {c }}$ Uses a diverge segment of four through lanes for Alternative 3; therefore, limiting factor is diverge capacity and not mainline capacity. (HCM analysis assumes lanes are never dropped after diverge.)
    ${ }^{\mathrm{d}}$ Uses a weaving segment of five lanes; therefore, limiting factor is weaving behavior and not mainline capacity. (HCM weaving analysis assumes a lane drop after the merge.)
    HCM = Highway Capacity Manual; LOS = level of service; $\mathrm{mph}=$ miles per hour; pc/lane mile = passenger cars per lane mile; V/C = volume-to-capacity

[^12]:    ${ }^{17}$ 1-93/I-95 Interchange Transportation Study, produced by the Massachusetts Executive Office of Transportation Office of Transportation Planning, June 2007.

[^13]:    ${ }^{18}$ The AM peak period is 6:00 AM to 10:00 AM, and the PM peak period is 3:00 PM to 7:00 PM. Source: Central Transportation Planning Staff.

[^14]:    ${ }^{19}$ I-93 and I-95 Transportation Improvement Project. This project, which is currently under construction, added a lane in each direction to I-93 and I-95 from Randolph to Wellesley.

[^15]:    ${ }^{20} 700$ vehicles per hour estimate uses a five-mile queue of vehicles spaced with 25 -foot headways, spread over 1.5 lanes, and dispersed over the course of two hours.
    ${ }^{21}$ Highway Capacity Manual 2010, Transportation Research Board of the National Academies, Washington, DC, December 2010. 13-18.

[^16]:    ${ }^{22}$ Seth Asante, MPO staff, memorandum to the Transportation Planning and Programming Committee of the Boston Region MPO, "Safety and Operational Improvements for the I93/Route 24 Interchange," September 2007.

[^17]:    ${ }^{23}$ Highway Capacity Software 7, Version 7.3, McTrans Center, PO Box 116585, Gainesville, Florida, 2017.

[^18]:    ${ }^{24}$ American Association of State Highway and Transportation Officials. Highway Safety Manual. Washington, DC, 2010.
    ${ }^{25}$ Crash Modification Factors Clearinghouse, www.cmfclearinghouse.org/index.cfm
    ${ }^{26}$ American Association of State Highway and Transportation Officials. Highway Safety Manual. Washington, DC, 2010.
    ${ }^{27}$ Crash Modification Factors Clearinghouse, www.cmfclearinghouse.org/index.cfm

[^19]:    ${ }^{28}$ Safety and Operational Improvements for the I-93/Route 24 Interchange, produced by the Central Transportation Planning Staff of the Boston Region MPO, September 2007.

[^20]:    ${ }^{29}$ The AM peak period is 6:00 AM to 10:00 AM, and the PM peak period is 3:00 PM to 7:00 PM. Source: Central Transportation Planning Staff.

[^21]:    ${ }^{30}$ Highway Capacity Software 7, Version 7.3, McTrans Center, PO Box 116585, Gainesville, Florida, 2017.
    ${ }^{31}$ Highway Capacity Manual 2010, Transportation Research Board of the National Academies, Washington, DC, December 2010. 13-18.

[^22]:    Connie

[^23]:    ${ }^{1}$ Karl H Quackenbush, CTPS Executive Director, work program to the Boston Region Metropolitan Organization, "Low-Cost Improvements to Express-Highway Bottleneck Locations: FFY 2017," December 15, 2016.
    ${ }^{2}$ Federal Highway Administration, Recurring Traffic Bottlenecks: A Primer: Focus on Low-Cost Operations Improvements, US Department of Transportation, Federal Highway Administration, June 2009, p. 1.
    ${ }^{3}$ Seth Asante, MPO staff, memorandum to the Transportation Planning and Programing Committee of the Boston Region Metropolitan Planning Organization, "Low-Cost Improvements to Bottleneck Locations, Phase I," June 2, 2011.
    ${ }^{4}$ Chen-Yuan Wang, MPO staff, memorandum to the Transportation Planning and Programing Committee of the Boston Region Metropolitan Planning Organization, "Low-Cost Improvements to Bottleneck Locations, Phase II," dated March 12, 2012.
    ${ }^{5}$ Seth Asante, Seth Asante, MPO staff, memorandum to the Transportation Planning and Programing Committee of the Boston Region Metropolitan Planning Organization, "Low-Cost Improvements to Express-Highway Bottleneck Locations," December 3, 2015.

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